

# Final Noise Technical Report 

ODOT | K19786 I-205: Stafford Rd to OR 213
Corridor Widening \& Abernethy Bridge Seismic
Retrofit / Widening
ODOT EA: C6035200
HDR Project \#10063137
Clackamas County, Oregon
December 4, 2018

## Professional Engineer's Stamp



Signature:


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## Acronyms and Initialisms

| Consultant | HDR Engineering, Inc. and subconsultant partners |
| :--- | :--- |
| County | Clackamas County, Oregon |
| dB | Decibel |
| dB(A) | A-weighted decibels |
| DD | doubling of distance |
| FHWA | Federal Highway Administration |
| I-205 | Interstate 205 |
| Leq | equivalent sound level |
| Leq(h) | hourly equivalent sound level |
| LT- | Long-term measurement location |
| mph | miles per hour |
| NAC | noise abatement criteria |
| NAAC | Noise Abatement Approach Criteria |
| NB | Northbound |
| NCHRP | National Cooperative Highway Research Program |
| NEPA | National Environmental Policy Act |
| ODOT | Oregon Department of Transportation |
| OR | Oregon Route |
| OSMRE | Office of Surface Mining Reclamation and Enforcement |
| Project | I-205: Stafford Road to OR 99E Corridor Widening \& Abernethy Bridge |
| SB | Seismic Retrofit / Widening |
| ST- | Southbound |
| TNM | Short-term measurement location |
|  | Traffic Noise Model |

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## Executive Summary

The Interstate 205 (I-205): Stafford Road to Oregon Route (OR) 213 (Project) proposes to widen I-205 from the Stafford Road interchange to just north of the Abernethy Bridge crossing and tie into the existing roadway near the OR 213 interchange. Two new travel lanes would be added, generally to the middle of the facility where a grass median currently exists. Where there is no grass median, such as where the facility approaches the Abernethy Bridge from the west, the roadways would be widened to the south where a rock cut and blasting would be required. North of the Abernethy Bridge only, an auxiliary lane will be added to the facility. The Project also proposes to retrofit several structures including the Abernethy Bridge to accommodate the additional travel lanes.

Noise and vibration levels associated with the construction and operation of the Project Build Alternative (2045) were calculated and where appropriate compared to the Existing Conditions (2017). The No Build Alternative (2045) was also analyzed for the environmental assessment being prepared for the Project pursuant to the National Environmental Policy Act (NEPA).

Existing Condition (2017) noise levels range from 43 A-weighted decibels ( $\mathrm{dB}(\mathrm{A})$ ) hourly equivalent sound level (Leq) to $74 \mathrm{~dB}(\mathrm{~A}) \mathrm{L}_{\text {eq }}$ and exceed the Oregon Department of Transportation (ODOT) noise abatement approach criteria (NAAC) at 238 residences, the South Lake Church/Pre-School/Daycare, Jon Storm Park, and the Atlas Immersion Academy School.

No Build Alternative (2045) noise levels would range from $45 \mathrm{~dB}(\mathrm{~A}) \mathrm{L}_{\text {eq }}$ to $74 \mathrm{~dB}(\mathrm{~A})$ $L_{\text {eq }}$ and are predicted to exceed the NAAC at 281 residences, the South Lake Church/Pre-School/Daycare, Jon Storm Park, and the Atlas Immersion Academy School. No Build Alternative noise levels are predicted to increase on average by 1 decibel ( dB ) over the Existing Conditions and would be due to increases in traffic volumes. Build Alternative (2045) noise levels would range from $45 \mathrm{~dB}(\mathrm{~A}) \mathrm{L}_{\text {eq }}$ to 75 $\mathrm{dB}(\mathrm{A}) \mathrm{L}_{\text {eq }}$ and impacts would occur at 351 residences, the South Lake Church/PreSchool/Daycare, a pool at the Jamestown Apartments, Jon Storm Park, and the Atlas Immersion Academy School. Changes in noise levels predicted under the Build Alternative when compared to the Existing Condition would increase up to $5 \mathrm{~dB}(\mathrm{~A})$ due to increased traffic and reduced setback distances to the widened roadway.

The Build Alternative noise impacts are predicted throughout the study area and noise abatement measures in the form of noise walls were evaluated in 13 locations for feasibleness and reasonableness. Three of the 13 noise walls (Noise Walls 5, 8, and 9 ) cannot feasibly reduce noise levels per ODOT policy and five of the 13 noise walls (Noise Walls 1, 3, 6b, and 11) could feasibly reduce noise levels but are unreasonably expensive per ODOT policy. The remaining noise walls (Noise Walls 2, $4,6 a, 7$, and 12) are feasible and reasonable per ODOT policy and are recommended for further consideration and inclusion in the Project, specifically:

- Noise Wall 2: North of Blankenship Road located parallel to the southbound (SB) I-205 lanes.
- Noise Wall 4: South of Blankenship Road located parallel to the SB I-205 lanes.
- Noise Wall 6a: 3,697 feet south of the $10^{\text {th }}$ Street interchange and located on a ridge at the SB I-205 right-of-way.
- Noise Wall 7: North of the Sunset Avenue overcrossing and west of the I-205 SB lanes.
- Noise Wall 12: North of the I-205 SB lanes near the Main Street overcrossing in Oregon City.

These noise walls would provide sufficient noise reduction to be classified as "benefitted" (i.e., 5 dB reduction or greater) per ODOT noise regulations at 136 impacted residences. An additional 100 residences would also benefit from the noise abatement that would not be impacted by the project. Preliminary costs for the noise walls would total $\$ 2,854,020^{1}$. Noise impacts are unavoidable at the remaining 223 impacted receptors.

The distance to the $65 \mathrm{~dB}(\mathrm{~A})$ noise abatement approach criteria (NAAC) on undeveloped lands in the vicinity of I-205 ranges from 420 feet in the western portion of the Project to 480 feet in the eastern portion of the Project. The distance to the 70 dB(A) NAAC would range from 150 feet in the western portion of the Project to 170 feet in the eastern portion of the Project.

The findings of this report will be shared with local governments, such as the cities of West Linn and Oregon City as well as Clackamas County, for their consideration of these sound levels in approving residential land use development in the future.

[^0]
## 1 Introduction

This Noise and Vibration Technical Report has been prepared as a part of the environmental review for the I-205: Stafford Road to Oregon Route 213 (OR 213) (the Project). The section of I-205 from Stafford Road to OR 99E is the last remaining bottleneck on the l-205 corridor and also does not meet seismic resiliency goals. With just two through lanes in each direction, this section of the I-205 freeway currently experiences significant traffic delay. Regional growth is expected to expand the congested peak periods, further reducing the hours that vehicles can move on the system without major delays. The purpose of the project is to reduce congestion in the I-205 corridor by adding additional through-lanes in the northbound (NB) and southbound (SB) directions between Stafford Road and OR 99E, as well as to ensure seismic resiliency of the entire corridor. The Project is also considering an auxiliary lane on I-205 northbound from OR 99E to OR 213. The Project is anticipated to improve mobility and travel time reliability within the corridor, with corridor peak hour travel speeds estimated to increase up to 25 percent over today's speeds.

## 2 Project Description

The Project area consists of an urban freeway segment that generally includes two travel lanes in each direction with auxiliary lanes at the Abernethy Bridge. The existing third general purpose lane stops at the north end of the Project at the OR 99E interchange area. The Project would add a third through-travel lane in each direction and would minimally adjust affected interchanges to conform to the third lane. It is not the Project's intent to significantly reconfigure any interchange. The Project would also widen and seismically upgrade twelve structures, reconstruct four structures, and remove one structure. Details of the Project are listed below:

- Adding a third through-lane in each direction form Stafford Road to OR 99E.
- Adding a NB auxiliary lane from OR 99E to OR 213.
- Widening with seismic upgrades to the following bridges:
o I-205 SB over Borland Road
o I-205 NB over Borland Road
o I-205 SB over 10th Street (West Linn)
o I-205 NB over 10th Street (West Linn)
o I-205 over Willamette River (Abernethy)
o I-205 SB Connection \#2 to Highway 3 (West Linn interchanges)


## o I-205 over Main Street (Oregon City)

- Removal and reconstruction of the following bridges:
o Sunset Avenue (West Linn) over I-205
o West A Street (West Linn) over I-205
o Tualatin River, I-205 SB
o Tualatin River, I-205 NB
o I-205 SB over Woodbine Road (removal and reconstruction)
o I-205 NB over Woodbine Road (removal and reconstruction)
o I-205 SB over Blankenship Road (removal and reconstruction)
o I-205 NB over Blankenship Road (removal and reconstruction)
- Removal of the following bridges:
o Broadway (West Linn) over I-205 \& OR 43
o I-205 NB Connection \#1 to OR 99E (Oregon City interchange)


## 3 Methodology

This section describes the methodology used in the Project's noise and vibration analysis to identify impact conditions consistent with federal, state, and local regulations.

### 3.1 Noise Standards and Criteria

The noise impact of the Project was assessed in accordance with Federal Highway Administration (FHWA) and ODOT noise assessment regulations and guidelines. The FHWA regulations are set forth in 23 CFR Part 772. ${ }^{2}$ On July 13, 2010, FHWA published revised noise regulations that became effective on July 13, 2011. ODOT prepared revisions to its noise policy in accordance with FHWA's requirements and revised policy which became effective July 13, 20113.

[^1]
### 3.1.1 Noise Abatement Criteria

To assess the degree of traffic noise impact on human activity, the FHWA established a noise abatement criteria (NAC) for different categories of land use (see Table 1). Per the aforementioned FHWA regulations, these levels "represent the upper limit of acceptable traffic noise conditions" and the NAC "represent a balancing of that which may be desirable with that which may be achievable." According to ODOT regulations, traffic noise impact occurs when the predicted traffic noise levels approach or exceed the NAC, or when the predicted traffic noise levels substantially exceed the existing noise levels. ODOT defines the word "approach" in "approach or exceed" as 2 decibels (dB) less than the FHWA NAC and defines this as the Noise Abatement Approach Criteria (NAAC) and identifies a substantial increase as having occurred if the increase is 10 dB or greater above existing conditions. The regulations further state that noise impact should be assessed for the loudest traffic conditions, which are either the peak vehicular hour or the peak truck hour for the design year. The peak truck hour is used in this analysis because the project corridor operates below posted speed limits during peak hour, therefore lower noise levels persist during the peak hour when compared to the peak truck hour. This approach was agreed to with ODOT noise staff during a project meeting held in October of 2017. (ODOT 2017)

The NAAC are expressed in terms of the hourly equivalent A-weighted sound levels. The A-weighted sound level, designated $\mathrm{dB}(\mathrm{A})$, is a measure of sound intensity with weighted frequency characteristics that corresponds to human subjective response to noise. Most environmental noise (and the A-weighted sound level) fluctuates from moment to moment, and it is common practice to characterize the fluctuating level by a single number called the equivalent sound level ( $\mathrm{L}_{\text {eq }}$ ). The $\mathrm{L}_{\text {eq }}$ is the value or level of a steady, non-fluctuating sound that represents the same sound energy as the actual time-varying sound evaluated over the same time period. For traffic noise assessment, $L_{\text {eq }}$ is typically evaluated over a one-hour period, and may be denoted as $L_{\text {eq }}(h)$.

This study evaluated residential (Category B), park/school/recreation areas (Category C), one interior use only retirement home (Category D), and a hotel outdoor use areas (Category E). For Categories B and C, noise impact is assumed to occur when predicted exterior noise levels, due to the Project, approach or exceed $67 \mathrm{~dB}(\mathrm{~A}) \mathrm{L}_{\mathrm{eq}}(\mathrm{h})$ during the loudest hour of the day. Therefore, the ODOT-defined threshold for noise impact is where exterior noise levels would be 2 dB less than 67 $d B(A) L_{e q}(h)$, or $65 d B(A) L_{e q}(h)$ for NAAC $B$ and $C$ uses. For commercial properties, noise impact is assumed to occur when predicted exterior noise levels, due to the Project, would approach or exceed $72 \mathrm{~dB}(\mathrm{~A}) \mathrm{L}_{\text {eq }}(\mathrm{h})$ during the loudest hour of the day. Therefore, the threshold for noise impact is where exterior noise levels would be 2 dB less than $72 \mathrm{~dB}(\mathrm{~A}) \mathrm{L}_{\mathrm{eq}}(\mathrm{h})$, or $70 \mathrm{~dB}(\mathrm{~A}) \mathrm{L}_{\mathrm{eq}}(\mathrm{h})$. Noise impact also would occur wherever Project noise causes a substantial increase over existing noise levels. ODOT defines a substantial increase as an increase of 10 dB or more above existing noise levels.

Table 1. FHWA Noise Abatement Criteria and ODOT Approach Criteria

| Activity Category | NAC Leq(h) ${ }^{1}$ | ODOT NAAC $\mathrm{L}_{\text {eq }}(\mathrm{h})^{1}$ | Description of Activity Category |
| :---: | :---: | :---: | :---: |
| A | 57 (Exterior) | 55 (Exterior) | Lands on which serenity and quiet are of extraordinary significance and serve an important public need and where the preservation of those qualities is essential if the area is to continue to serve its intended purpose |
| $B^{2}$ | 67 (Exterior) | 65 (Exterior) | Residential |
| $\mathrm{C}^{2}$ | 67 (Exterior) | 65 (Exterior) | Active sport areas, amphitheaters, auditoriums, campgrounds, cemeteries, day care centers, hospitals, libraries, medical facilities, parks, picnic areas, places of worship, playgrounds, public meeting rooms, public or nonprofit institutional structures, radio studios, recording studios, recreation areas, Section 4(f) sites, schools, television studios, trails, and trail crossings |
| D | 52 (Interior) | 50 (Interior) | Auditoriums, day care centers, hospitals, libraries, medical facilities, places of worship, public meeting rooms, public or nonprofit institutional structures, radio studios, recording studios, schools, and television studios |
| $\mathrm{E}^{2}$ | 72 (Exterior) | 70 (Exterior) | Hotels, motels, offices, restaurants/bars, and other developed lands, properties or activities not included in A-D or F |
| F | - | - | Agriculture, airports, bus yards, emergency services, industrial, logging, maintenance facilities, manufacturing, mining, rail yards, retail facilities, shipyards, utilities (water resources, water treatment, electrical), and warehousing |
| G | - | - | Undeveloped lands that are not permitted (without building permits) |
| ${ }^{1}$ Hourly Equivalent A-weighted Sound Level (dB(A)) <br> ${ }^{2}$ Includes undeveloped lands permitted for this activity category Source: 23 CFR Part 772. |  |  |  |

When the predicted design-year Build case noise levels would approach or exceed the NAC during the loudest hour of the day or would cause a substantial increase in existing noise, consideration of traffic noise reduction measures is necessary. If it is found that such mitigation measures would cause adverse social, economic or environmental effects outweighing the benefits received, they may be dismissed from consideration. For this study, noise levels throughout the study area were estimated for Existing (2017) conditions and for the 2045 No Build and Build alternatives.

### 3.1.2 Local Noise Regulations

Portions of the Project are within the three local jurisdictions of Clackamas County, West Linn, and Oregon City.

### 3.1.2.1 Clackamas County

Clackamas County prescribes noise regulations via Title 6-10 of the County Code (Clackamas County, 2000). The applicable portions include those relating to construction noise, which the County restricts to daytime hours. Specifically, construction noise is restricted to the hours from 6:00 a.m. to 10:00 p.m. Construction noise associated with blasting is restricted to the hours from 9:00 a.m. to 10:00 p.m., excluding the weekends. Nighttime construction requires a noise variance from the County.

### 3.1.2.2 West Linn

West Linn prescribes noise regulations via Title 5, section 5.487 of the Municipal Code (City of West Linn, 2004). As with the County, the applicable portions include those relating to construction noise. Construction noise is exempted from the City's noise level limits from 7:00 a.m. to 7:00 p.m. during weekdays and from 9:00 a.m. to 5:00 p.m. on Saturdays. Construction noise may occur outside of these hours provided that it complies with the City's noise level limits which are provided in Table 2. If compliance is not possible, a noise variance is required. Noise-sensitive land uses are defined by the City as "Any use which is adversely affected by ambient sound or noise, as in the use of real property for residential occupancy, schools, churches, public libraries, or hospitals. This definition includes any place where people normally sleep. Impulse sounds include air overpressure associated with blasting." Examples of impulse sounds include noise from pile driving as well as blasting.

Table 2. West Linn Noise-Sensitive Use Property Line Sound Level Limits

| Type of Sound | 7:00 a.m. to 7:00 p.m. | 7:00 p.m. to 7:00 a.m. |
| :---: | :---: | :---: |
| Steady Sound ${ }^{1}$ | $\mathrm{L}_{50}=55 \mathrm{~dB}(\mathrm{~A})$ | $\mathrm{L}_{50}=45 \mathrm{~dB}(\mathrm{~A})$ |
|  | $\mathrm{L}_{10}=60 \mathrm{~dB}(\mathrm{~A})$ | $\mathrm{L}_{10}=50 \mathrm{~dB}(\mathrm{~A})$ |
|  | $\mathrm{L}_{1}=70 \mathrm{~dB}(\mathrm{~A})$ | $\mathrm{L}_{1}=55 \mathrm{~dB}(\mathrm{~A})$ |
| Impulse Sound ${ }^{2}$ | 95 dB | 80 dB |
| ${ }^{1}$ Statistical sound levels represent the percentage of time a sound level is exceeded. For example, the $L_{50}$ is the sound level exceeded 50 percent of the time and the $L_{10}$ is the sound level exceeded $10 \%$ of the time. <br> ${ }^{2}$ Impulse sound is typically evaluated in linear decibels (dB). <br> Source: West Linn Municipal Code, 2004. |  |  |

### 3.1.2.3 Oregon City

Oregon City's Public Works Department has published nighttime construction noise restrictions on their website (City of Oregon City, 2018). Specifically, construction is restricted to daytime from 7:00 a.m. to 6:00 p.m. weekdays and from 9:00 a.m. to 6:00 p.m. Saturdays. Construction outside of these time periods requires a variance.

### 3.2 Noise Prediction Model

HDR partnered with HMMH who used the latest version of the FHWA's Traffic Noise Model (TNM), Version 2.5 , to compute existing and future Build case loudest-hour noise levels and develop the preliminary heights, lengths and locations for all potential noise barriers along the project corridor. TNM incorporates state-of-the-art sound emissions and sound propagation algorithms, based on well-established theory or on accepted international standards. The acoustical algorithms contained
within the FHWA TNM have been validated with respect to carefully conducted noise measurement programs, and show agreement in most cases for sites with and without noise barriers (Federal Highway Administration, 1998, and US Department of Transportation, 2004).

Available aerial photography from Metro, topographic information from the Project survey effort, tree zones identified visually, and geographic information system (GIS) building information from Metro were used to create a three-dimensional model in the TNM of the geometry of the existing and future roadway configurations and the surrounding terrain and buildings. It should be noted there is considerable topographical change in the Project area, such as where I-205 approaches the Willamette River crossing from the south. These topographic effects and others were included in the modeling to increase the accuracy of TNM's predictions. The noise modeling also accounts for such factors as propagation over different types of ground (acoustically soft and hard ground), elevated roadway sections, shielding effects from local terrain and structures, distance from the road, traffic speed, and hourly traffic volumes including the distribution of roadway traffic in terms of automobiles, medium and heavy trucks, motorcycles, and buses. In some areas, local roadways were included in the models without traffic to help account for topographic and ground effects (i.e., acoustically reflective). To fully characterize existing and future noise levels at all noise-sensitive land uses in the study area, 731 noise prediction receivers were included in the modeling. There is one instance of a receiver representing two noise sensitive properties/sites.

At approximately 11 miles, the Project corridor is relatively long for TNM prediction efforts. Therefore, the project was divided roughly at its midpoint, where there are no noise-sensitive land uses within 500 feet, to improve run times. The modelling was divided up in such a manner to ensure sufficient overlap, which is achieved by extending roadways with traffic on them approximately 1,000 to 2,000 feet beyond where noise-sensitive receptors of interest are located. Noise abatement modelling was also divided up to analyze each individual noise wall. Where noise abatement measures were analyzed in detail the reported noise levels, both abated and unabated, are obtained from those noise models.

Information on noise-sensitive residential land use in the study area (NAAC B, C, D, and E ) includes the number of dwelling units, outdoor uses, and interior uses (where applicable) identified from existing mapping and field verification.

### 3.2.1 Abernethy Bridge Structure-Borne Noise

The Abernethy Bridge spans the Willamette River connecting the Oregon City side of the river to the east with the West Linn side of the river to the west. Clusters of noisesensitive receptors are located in these areas consisting of mainly residential uses on the West Linn side and a park on the Oregon City side of the river.

TNM does not directly account for noise emanating from aerial structures, such as noise from vehicle vibrations through the bridge's deck. Methodologies developed and documented in the National Cooperative Highway Research Program (NCHRP)

Report 791 were implemented to account for the structure-borne noise from the bridge. The process involved obtaining measurement data at the drip edge of the structure and simultaneously at distances further away from the structure to identify how much structure-borne noise influences sound levels in a given area of sensitive receptors. Studies have shown that structure-borne noise measured under free flow and relatively constant traffic conditions, such as what occurred during the measurement effort, does not vary greatly with increased traffic volumes. For this reason, the measured traffic noise level at drip edge, and as documented in the measurement section of this report, are applied to each of the conditions analyzed (e.g., Existing Conditions, No Build alternative, and Build alternative). Section 5 provides additional detail on these measurements and structure-borne noise.

### 3.3 Traffic Data for Noise Prediction

The traffic data used in the noise analysis is representative of the loudest hour of the day, which ODOT noise policy identifies as being the louder of either the peak vehicular hour or peak truck hour. Traffic modeling data for the project were derived using ODOT-provided counts combined with traffic predictions made by HDR for the 2016 Existing Conditions and the 2045 No Build and Build Alternatives. Existing traffic was counted on May 3, 2017 to obtain existing volumes (HDR 2017). Hourly volumes, truck percentages and posted speeds were provided for other major intersecting roadways in the local network.

HMMH worked with HDR to compare the peak vehicular hour against the peak truck hour to identify which case yields the higher traffic noise levels. While the peak vehicular hour has higher overall volumes of traffic on the analysis area roadways, traffic under these conditions are traveling well below posted speeds, at 25 miles per hour (mph) or less, along many portions of I-205. Lower traffic speeds, characteristic of the peak vehicular hour, produce considerably lower noise levels than under free flow conditions. Conversely, the peak truck hour conditions occur in the middle of the day, where volumes are lower, but traffic is moving under free flow conditions. Additionally, heavy trucks account for higher single passby noise levels in comparison to automobiles or light trucks. Therefore, the combination of vehicular traffic moving at free flow conditions and the highest percentage of heavy truck traffic on area roadways makes the peak truck hour the worst case traffic noise hour for the project area. This approach was agreed to during a conference call between ODOT noise staff and the HDR/HMMH consulting team. (ODOT 2017)

## 4 Existing Conditions

Existing noise levels were established using a combination of noise monitoring and modeling efforts. Additionally, existing structure-borne noise from the Abernethy Bridge was measured to identify the amount of structure-related noise that currently exists in areas near the bridge. Existing noise levels were identified at noise sensitive land uses in the analysis area.

### 4.1 Land Use

The study area, i.e., the area of potential impact, of noise-sensitive land uses for this report extends approximately 500 feet from Project improvements. The southwestern end of the study area from the Stafford Road interchange to the intersection of Johnson Road and Grapevine Road includes lower density development and could be considered more rural than the portion of the study area to the northeast. From approximately 2,000 feet west of the intersection of Johnson Road and Blankenship Road near I-205 to the eastern terminus of the Project at OR 213, the study area has higher density development and would be characterized as being more urban.

Table 3 provides the quantities of land uses by NAAC. Figure 1 and Figure 2, in Section 11 of this report, are zoning and comprehensive plan designation maps, respectively, for the areas analyzed. No noise-sensitive receptors would be displaced as part of the Project. Research was conducted to identify new developments in the noise study area that could be impacted by the Project. The only such development, the Grand Cove Project multi-family complex, is currently under construction in Oregon City. According to the Grand Cove Project Land Use Application with the City of Oregon City (Oregon City, 2015) it will be constructed over a number of years in multiple phases and will comply with all federal, state, and local noise regulations. The first phase of this new development includes 132 multifamily residences and outdoor pool.

The McLean House, and other historic resources on Willamette Drive, are included in the analysis as a NAAC B uses and are located near the West Linn landing of the Abernethy Bridge.

Table 3. Existing Land Uses

| Noise Abatement Activity Category and Land Use | Total Number of Uses |
| :---: | :---: |
| B (65) | $\mathbf{7 1 3}$ |
| Multi-Family Residential | $294^{1}$ |
| Single-Family Residential | 419 |
| C (65) | $\mathbf{1 0}$ |
| Church, Daycare, School | 1 |
| Jon Storm Park | 5 |
| Play Structure at Apts. | 1 |
| Pool at Apts. | 2 |
| School (Atlas Immersion Academy) | 1 |
| D (50) |  |
| Retirement Home (no outdoor use) | $\mathbf{7 1}$ |
| E (70) | 71 |
| Best Western | 120 |
| Best Western (Outdoor Seating) | $118^{3}$ |
|  | 1 |


| Noise Abatement Activity Category and Land Use | Total Number of Uses |
| :--- | :---: |
| Best Western (Pool) | 1 |
| Notes: |  |
| 1. | Includes Grand Cove Project future sensitive receptors. |
| 2. |  |
| 3. an interior noise level limit. | The hotel has 118 rooms. |

### 4.2 Measurements

A noise measurement program, consisting of long-term (LT) and short-term (ST) measurements, was conducted to document existing ambient sound levels and to assist in validating the modeling results Photographs were collected of each measurement location and each measurement was completed with a sound level meter that is classified as an American National Standards Institute (ANSI) Type 1 (precision) sound level meter. The monitoring locations are shown in the figures in Section 11 of this report. Appendix A provides the noise measurement data sheets and photographs for each measurement location. The monitoring equipment was laboratory calibrated within the previous year. Appendix B provides the laboratory calibration sheets for the equipment used in this monitoring effort. Traffic data used in all of the prediction efforts, including the validation efforts, are provided in Appendix C.

The LT and ST measurements are described in the following subsections.

### 4.2.1 Long-Term (24-hour) Measurements

Two long-term (24-hour) measurements were conducted during weekdays to document existing conditions and diurnal variation. Long-term measurement location 1 (LT-1) was located at a place of worship (South Lake Foursquare Church) and preschool approximately 140 feet south of the I-205 SB lanes and approximately 650 feet east of the crossover of I-205 and SW Borland Road. LT-1 was situated approximately 100 feet east of the play structure at the same perpendicular distance from the highway as the play structure. During deployment of the LT-1 monitoring equipment field engineers anecdotally noted that traffic noise at this location dominated the noise of children on the play structure. Sound levels at LT-1 were measured from 12:19 p.m. on August 29, 2017 to 1:16 p.m. on August 30, 2017.

LT-2 was located at a duplex at 4329 Imperial Drive. This residential structure is located approximately 215 feet north of the I-205 NB lanes and is on top of a bluff with the highway approximately 25 to 35 feet below. Sound levels were measured at LT-2 from 2:14 p.m. on August 30, 2017 to 2:45 p.m. on August 31, 2017. Table 4 provides a summary of the long-term measurement results.

Table 4. Long-Term 24-Hour Measurement Results

| Monitoring Location | $\begin{aligned} & \mathrm{Leq}^{1} \\ & \mathrm{~dB}(\mathrm{~A}) \\ & \text { (day) } \end{aligned}$ |  | $L_{\text {dn }}{ }^{1}$ $\mathrm{~dB}(\mathrm{~A})$ | $L_{\text {min }}$ $d B(A)$ | $L_{\text {max }}$ $\mathrm{dB}(\mathrm{A})$ | $\mathrm{L}_{10}$ <br> $d B(A)$ | $\begin{gathered} L_{50} \\ d B(A) \end{gathered}$ | L90 <br> $d B(A)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LT-1 | 71.6 | 68.9 | 75.6 | 42.8 | 88.2 | 73.0 | 68.6 | 63.0 |
| LT-2 | 59.7 | 58.8 | 65.2 | 48.8 | 81.2 | 60.4 | 58.4 | 56.4 |

${ }^{1} \mathrm{~L}_{\text {eq }}$ (day) represents the energy averaged sound level for the hours of 7:00 a.m. to 10:00 p.m., $\mathrm{L}_{\text {eq }}$ (night) is the energy averaged sound level for the hours of 10:00 p.m. to 7:00 a.m., and the $L_{d n}$ is the Day-Night Average Sound Level which is the energy averaged sound level for the 24 -hour monitoring period with 10 dB added to nighttime sound levels. .

### 4.2.2 Short-term Validation Measurements

The short-term measurements were used to validate the TNM results for the existing conditions scenario. Section 6.3 of the ODOT Noise Manual states a traffic noise model is considered a valid predictor of traffic noise if measured and modeled noise levels agree within $\pm 3 \mathrm{~dB}(\mathrm{~A})$. The short-term measurements were at least 15 minutes in duration at each of 13 locations throughout the study area. Also, vehicle traffic classification counts were conducted for 10-minutes during each measurement and speeds documented concurrent with each of the short-term noise measurements as shown in Appendix C. Two of these measurements were conducted at the same location as long-term measurements, specifically Short-Term measurement location 1 (ST-1) was collected at the same location as LT-1 and ST-10 was collected at LT2. Speeds at ST-10 were slower than posted speeds during the validation effort due to unknown causes ${ }^{4}$. Speeds were also slower than posted speeds on l-205 during the ST-7, ST-8, ST-9, and ST-13 validation measurements for unknown reasons. Observed traffic speeds were used in the model validation effort. The remaining short-term validation measurements were completed at the following locations:

- ST-2: This measurement was conducted in the yard of a residence on the side closest to I-205 at 22400 Johnson Road. The measurement was approximately 240 feet south of I-205 SB lanes and 165 feet east of SW Johnson Road.
- ST-3: This measurement was conducted in the yard of a residence on the side closest to I-205 at 22601 Grapevine Road. The measurement was approximately 233 feet northeast of I-205 NB lanes and 80 feet west of S Grapevine Road.
- ST-4: This measurement site was in the yard of a residence on the side closest to I-205 at 23400 Johnson Road. The measurement was approximately 180 feet west of I-205 SB lanes and 525 feet east of Johnson Road.
- ST-5a: This measurement was conducted in the yard of a residence on the side closest to I-205 at 2384 Margery Street. The measurement was approximately 140 feet east of I-205 NB lanes and 84 feet west of Margery Street. This measurement was representative of front row residences in that neighborhood.

[^2]- ST-5b: This measurement was conducted at the second row of residences in the same neighborhood as ST-5a and in the yard of a residence on the side closest to I-205 at 2383 Margery Street. The measurement was approximately 275 feet east of I-205 NB lanes and 40 feet east of Margery Street. This measurement was representative of front row residences in that neighborhood.
- ST-6: This measurement site was at the portion of a play structure/swing at the Willamette Terrace Apartments closest to I-205 at 1709 Blankenship Rd. The measurement was approximately 260 feet northeast of I-205 SB lanes and 240 feet south of Blankenship Road.
- ST-7: This measurement was conducted in the yard of a residence on the side closest to I-205 at 1788 Jamie Circle. The measurement was approximately 260 feet southwest of I-205 NB lanes and 100 feet northeast of Jamie Circle.
- ST-8: This measurement site was in the yard of a residence on the side closest to $\mathrm{I}-205$ at $23188^{\text {th }}$ Street. The measurement was approximately 455 feet south of the I-205 NB onramp from $10^{\text {th }}$ Street and 90 feet south of Willamette Falls Drive. At this location, noise from I-205 is dominant; however, when traffic is present on Willamette Falls Drive it is audible over the more consistent noise source from l-205.
- ST-9: This measurement was conducted in the yard of a residence on the side closest to I-205 at 4701 Imperial Drive. The measurement was approximately 315 feet north of the I-205 SB lanes and 110 feet south of Imperial Drive.
- ST-11: This measurement site was in the yard of a residence on the side closest to I-205 at 4835 Willamette Falls Drive. The measurement was approximately 380 feet south of the I-205 NB lanes and 70 feet south of Willamette Falls Drive. Due to topography, l-205 is about 35 feet higher in elevation than where the measurement was completed and Willamette Falls Drive is about 10 feet higher in elevation. As a result, line of sight to traffic on I-205 is mostly blocked, its noise is lower in intensity than traffic noise from Willamette Falls Drive.
- ST-12: This measurement was conducted in the yard of a residence on the side closest to I-205 at 5345 Grove Street. The measurement was approximately 90 feet north of the I-205 SB lanes and 90 feet south of Grove Street. I-205 is on structure in this part of the project area at the south end of the Abernethy Bridge crossing of the Willamette River. The main lanes and the exit ramp to OR 43 are both approximately 40 feet above the neighborhood and where the measurement was conducted.
- ST-13: This measurement site was at a picnic table in Jon Storm Park at 1801 Clackamette Drive. The measurement was approximately 118 feet north of the I-205 SB lanes and 260 feet west of highway 99E. I-205 is on-structure in this part of the project area at the north end of the Abernethy Bridge crossing of the Willamette River. The main lanes and the exit ramp to 99E are both approximately 40 feet above where the measurement was conducted.

Observed traffic volumes during each of the short-term measurements were scaled to be hourly equivalents and applied to the roadways in the modeling and run for each measurement location. These traffic volumes are provided in Appendix C.

As Table 5 demonstrates, the measured and modeled noise levels agree within 3 $\mathrm{dB}(\mathrm{A})$; therefore, the TNM (and its data inputs) are valid predictors of traffic noise for the Project.

The validation included shielding effects from topographic features, large tree stands, buildings and rows of houses, and reflective surfaces such as water bodies (i.e., the Willamette River).

Upon completion of the validation effort, the TNM implementation of the study area was expanded to include all of the identified noise-sensitive land uses in the study area. This area extended out from the I-205 corridor widening project by about 500 feet, and included all of the noise-sensitive land uses listed in Table 3. The measurement locations are provided on Figures 1 through 32 in Section 11.

Table 5. Short-Term Measurement Validation Results

| Monitoring Location | Date/Time of Measurement | Distance to Edge of Roadway (feet) | $\begin{gathered} \text { Measured } \\ \text { Leq }_{\text {eq }} \\ \mathrm{dB}(\mathrm{~A}) \end{gathered}$ | $\begin{gathered} \text { Modeled } \\ \text { Leq } \\ \operatorname{dB}(A) \end{gathered}$ | Difference <br> (Modeled minus <br> Measured) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| ST-01 | 8/29/2017 12:35-12:50 | 140 | 72.6 | 70.1 | -2.5 |
| ST-02 | 8/29/2017 13:24-13:52 | 240 | 64.5 | 63.5 | -1.0 |
| ST-03 | 8/30/2017 9:38-9:53 | 233 | 63.1 | 65.9 | 2.8 |
| ST-04 | 8/30/2017 10:16-10:31 | 180 | 63.9 | 66.6 | 2.7 |
| ST-05a | 8/30/2017 10:49-11:04 | 140 | 69.4 | 72.2 | 2.8 |
| ST-05b | 8/30/2017 11:06-11:21 | 275 | 64.9 | 65.4 | 0.5 |
| ST-06 | 8/30/2017 12:36-13:01 | 240 | 58.0 | 60.2 | 2.2 |
| ST-07 | 8/30/2017 15:06-15:21 | 260 | 58.1 | 60.9 | 2.8 |
| ST-08 | 8/31/2017 9:38-9:57 | 455 | 63.2 | 62.6 | -0.6 |
| ST-09 | 8/31/2017 10:25-10:40 | 315 | 56.0 | 58.0 | 2.0 |
| ST-10 | 8/30/2017 14:35-14:50 | 215 | 57.4 | 58.3 | 0.9 |
| ST-11 | 8/31/2017 13:07-13:22 | 380 | 57.6 | 57.2 | -0.4 |
| ST-12 | 8/31/2017 13:39-14:00 | 90 | 59.9 | 57.0 | -2.9 |
| ST-13 | 8/31/2017 14:14-14:32 | 118 | 63.4 | 62.8 | -0.6 |

Note: Traffic counts and speeds for each measurement are provided in Appendix C.

### 4.2.3 Abernethy Bridge Structure-Borne Noise Measurements

Structure-born noise was measured using the same type of equipment as was used for the long-term measurements. TNM does not calculate structure-borne noise. For this reason, quantifying the structure-borne noise is necessary to properly analyze potential noise mitigation (i.e., a noise wall) that could be needed on the bridge. Specifically, short-term monitoring near the bridge validated within the tolerance of TNM per the ODOT noise manual; however, these measurements were completed at locations away from the structure where noise from vehicular traffic on the bridge alone currently dominates structure-borne noise. If the vehicular traffic noise source
was blocked by a noise wall, structure-borne noise would remain and the noise wall would not be as effective as TNM predicts. To identify the contribution of structureborne noise from the Abernethy Bridge, structure-borne noise measurements were completed implementing the procedures documented in NCHRP Report 791 (NCHRP 2014), specifically Chapter 2 and Appendix A of that report.. The general measurement process and application of the resulting structure-borne noise levels for the project was as follows:

1. Noise measurements were completed at the drip edge of the structure and at least two other locations further away from the structure.
2. Traffic volumes of vehicles using the structure were collected.
3. Drop-off rates of structure-borne noise were calculated using the worksheet provided in Appendix A of the NCHRP 791 report with noise reducing by 3 dB per doubling of distance (dB/DD), $4.5 \mathrm{~dB} / D \mathrm{D}$, and $6 \mathrm{~dB} / D \mathrm{D}$.
4. The sound level at the two measurement locations that are not the drip edge measurement were calculated using TNM.
5. The calculated sound levels obtained via steps \#3 and \#4 were logarithmically added.
6. Results of Step \#5 was compared to the measured sound levels collected in step \#1 to identify what drop-off rate was most appropriate to apply to the structureborne noise from the structure being analyzed.
7. Using the measured drip edge sound level and the identified drop-off rate, the structure-borne noise level occurring at the noise sensitive receptors of interest was identified by adjusting for distance and using the worksheet from NCHRP 791 (See Table 6 and Appendix A).
8. The resultant levels from step \#7 were logarithmically added to the TNM predictions for the existing conditions, No Build Alternative, and Build Alternative.

Amounts of structure-borne noise is present at all receptors near (i.e., within approximately 500 feet) the Abernethy Bridge analyzed as part of the Project. The amount of structure-borne noise varies with distance from the structure with those closest to the structure experiencing higher structure-borne noise than those further away. For example, for receptors along OR 43, noise from OR 43 dominates, but there is also some structure radiated noise. For these receptors the noise from OR 43 is of such significance that the structure-radiated noise only has a negligible effect (less than 1 dB ). For receptors closer to the river that are also close to the bridge, such as those on River Street, structure-radiated noise is more significant.

The measurement effort involved three sound level meters. The locations of the measurements are shown on Figure 33. Structure-borne sound levels were measured on the Oregon City side of the crossing in John Storm Park and near the McLean House on River Street on the West Linn side of the crossing. For the Oregon City measurements, one sound level meter was set up at the drip edge of the structure and two other sound level meters were set up at 50 feet and 100 feet,
respectively. The Oregon City measurements were completed on June 13, 2018 and the West Linn measurements were completed on June 13, 2018 and June 19, 2018. On the West Linn side of the crossing, two sets of measurements were completed on different days to obtain a second data set under a different traffic condition. The West Linn measurements were completed at the drip edge and at varying distances from the structure, specifically 50 feet, 85 feet, and 120 feet. Traffic conditions (i.e., vehicle counts and speeds) on I-205 were simultaneously collected during each of the measurements and are contained in Appendix C. Traffic volumes were entered into the validated existing conditions TNM run and the differences between measured and modeled sound levels tabulated.

As mentioned earlier in this section, three drop-off rates were analyzed to identify which drop-off rate was most appropriate for a given structure, specifically $3 \mathrm{~dB} / D \mathrm{D}$, 4.5 dB/DD, and 6 dB/DD. Equations are provided in NCHRP Report 791 to accomplish these calculations and spreadsheets were used to complete these calculations. Specifically, the following equation was employed for $4.5 \mathrm{~dB} / \mathrm{DD}$ calculations:
$L_{A x}=\operatorname{Lde}-15 \times \log _{10}\left(D_{A P} / D_{R e f}\right)$, where

- $L_{D E}=$ measured $L_{\text {eq }}$ in $d B(A)$ at 5 feet above the ground under the structure drip edge
- $L_{A x}=$ Calculated structure-related noise level at analysis point $A_{x}$, located $x$ feet from the drip edge, in $\mathrm{dB}(\mathrm{A})$
- $D_{A P}=$ Distance from point $S$ to the analysis point $A_{x}$, in feet
- $\quad D_{\text {Ref }}=$ Distance from point $S$ to point $A_{\text {ref }}$, in feet
o 56 feet on the Oregon City side
o 82 feet on the West Linn side
- $S$ = Length to the midpoint of the structure, or the width divided in half, in feet.
o 50 feet on the Oregon City side
o 70 feet on the West Linn side
See Table 6 for an example of the calculation worksheet where these values were implemented for the Oregon City side of the crossing. Figure 34 provides a schematic drawing of how these variables are used to assess structure related noise.

Table 6. Structure Related Noise Calculation Worksheet for Oregon City

| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Oregon City Side of Crossing |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck, in feet |  |  |  | 50 |
| Aref: Center point between ground and underside of structure (h/2), in feet |  |  |  | 25 |
| w: Width of Structure (feet) |  |  |  | 100 |
| Mw: Midpoint of structure (w/2) in feet. The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 50 |
| Dref: Reference distance - from S to Aref, in feet |  |  |  | 55.9 |
| Measured Noise Level at Drip Edge, $\mathrm{dB}(\mathrm{A})$ |  |  |  | 72.3 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from Drip Edge (feet) | Distance from Analysis Point (feet) | Measured <br> Noise <br> Level at <br> Drip Edge <br> Leq in <br> $\mathrm{dB}(\mathrm{A})$ | Calculated <br> Noise <br> Level with <br> Drop-off <br> Rate $=3.0$ <br> dB/DD |
| Aref | 0 | 55.9 | 72.3 | n/a |
| A50 | 50 | 105.9 | n/a | 70 |
| A100 | 100 | 155.9 | n/a | 68 |
| Analysis Point | Distance from Drip Edge (feet) | Distance from Analysis Point (feet) | Measured <br> Noise <br> Level at <br> Drip Edge <br> Leq in <br> $\mathrm{dB}(\mathrm{A})$ | Calculated <br> Noise <br> Level with <br> Drop-off <br> Rate $=4.5$ <br> dB/DD |
| Aref | 0 | 55.9 | 72.3 | n/a |
| A50 | 50 | 105.9 | n/a | 68.1 |
| A100 | 100 | 155.9 | n/a | 65.6 |
| Analysis Point | Distance from Drip Edge (feet) | Distance from Analysis Point (feet) | Measured <br> Noise <br> Level at <br> Drip Edge <br> Leq in <br> $\mathrm{dB}(\mathrm{A})$ | Calculated <br> Noise <br> Level with <br> Drop-off <br> Rate $=6.0$ <br> dB/DD |
| Aref | 0 | 55.9 | 72.3 | n/a |
| A50 | 50 | 105.9 | n/a | 67 |
| A100 | 100 | 155.9 | n/a | 63 |

Source: NCHRP 2014, HMMH 2018

Table 7 presents the results of the structure-borne measurement and analysis effort and demonstrates that structure-borne noise most closely aligns with a drop-off rate of $4.5 \mathrm{~dB} / \mathrm{DD}$. Figure 35 is a chart that shows how these sound levels drop off with distance and how they relate to the corresponding measured noise levels. The structure-borne noise levels identified are applied to noise-sensitive land uses near the Abernethy Bridge to properly account for the structure-related noise.

As an example, measurement ST-12, on Figure 14, was conducted in the backyard of a residence 90 feet from the edge of the Abernethy Bridge with a level of 59.9 $d B(A)$ Leq. The TNM-modeled sound level for validation purposes with no adjustments made for structure-borne noise was $57.0 \mathrm{~dB}(\mathrm{~A})$ Leq, a sound level 2.9 dB less than what was measured. Based on the structure-borne noise analysis, the noise emanating from the structure deck for this location was $60.2 \mathrm{~dB}(A) L_{\text {eq }}$. Therefore, adding the structure-borne noise to the TNM-modeled level results in an adjusted sound level of $61.9 \mathrm{~dB}(\mathrm{~A})$, a level 2 dB higher than what was measured. This is a level that would be considered "valid" for prediction purposes and shows better agreement with the original validation measurement.

Ultimately, the reason why it is necessary to include structure-borne noise in this analysis is because it affects how well potential noise mitigation is estimated to perform on the bridge, as documented in Section 6 of this report. Specifically, if a noise wall is installed on the Abernethy Bridge, the sound emanating from vehicular traffic on the roadway would be blocked; however, the sound from vehicles causing structure-born noise to radiate from below the structure would remain. Accounting for the amount of structure-borne noise that cannot be abated affects how well noise abatement measures perform per ODOT policy. Appendix A provides the measurement results and NCHRP Report 791 analysis sheets.

Table 7. Structure-Borne Noise Measurement and Analysis Results

| Measurement Location | Measurement Period |  | Location of Measurem ent in Relation to Drip Edge (feet) | Measured <br> Leq Noise Level [dB(A)] | FHWA TNM Modeled Leq(h) Noise Level [dB(A)] due to Highway Traffic Only | Assumed Effect of Structure -Related Noise (dB) | Modeled Leq(h) Noise Level [dB(A)] Assuming Spreadsheet Value <br> Adjustment for StructureRelated Noise and Assuming Drop-Off Rate of: |  |  | Measured Minus Modeled Leq Noise Level [dB(A)] Assuming Drop-Off Rate of: |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | From | To |  |  |  |  | $3 \mathrm{~dB} / \mathrm{DD}$ | $\begin{gathered} 4.5 \\ \mathrm{~dB} / \mathrm{DD} \end{gathered}$ | $\begin{gathered} 6 \\ \text { dB/DD } \end{gathered}$ | $\stackrel{3}{\mathrm{~dB} / \mathrm{DD}}$ | $\begin{gathered} 4.5 \\ \mathrm{~dB} / \mathrm{DD} \end{gathered}$ | $\begin{gathered} 6 \\ \mathrm{~dB} / \mathrm{DD} \end{gathered}$ |
| Oregon City Side of Crossing | $\begin{gathered} 6 / 13 / 2 \\ 018 \\ 11: 00 \end{gathered}$ | $\begin{gathered} 6 / 13 / 2 \\ 018 \\ 12: 23 \end{gathered}$ | Drip Edge | 72.3 | 62.2 | 10.1 | N/A | N/A | N/A | N/A | N/A | N/A |
| (Jon Storm Park |  |  | 50 | 69 | 63.7 | 4.8 | 70.5 | 69.5 | 68.5 | 2.0 | 1.0 | 0.0 |
| Park/Near SB <br> Lanes) |  |  | 100 | 68 | 62.6 | 5.7 | 69.0 | 67.4 | 66.0 | 0.7 | -0.9 | -2.3 |
| West Linn Side of Crossing (SB Side of Structure) | $\begin{gathered} 6 / 13 / 2 \\ 018 \\ 14: 14 \end{gathered}$ | $\begin{gathered} 6 / 13 / 2 \\ 018 \\ 14: 51 \end{gathered}$ | Drip Edge | 67.1 | 57.4 | 9.7 | N/A | N/A | N/A | N/A | N/A | N/A |
|  |  |  | 50 | 65.2 | 56.8 | 8.4 | 65.6 | 64.8 | 63.9 | 0.4 | -0.4 | -1.3 |
|  |  |  | 85 | 62.5 | 58.2 | 4.3 | 65.0 | 63.8 | 62.8 | 2.5 | 1.3 | 0.3 |
| West Linn Side of Crossing (SB Side of Structure) | $\begin{gathered} \text { 6/19/2 } \\ 018 \\ 11: 52 \end{gathered}$ | $\begin{gathered} 6 / 19 / 2 \\ 018 \\ 12: 11 \end{gathered}$ | Drip Edge | 66.0 | 57.4 | 8.6 | N/A | N/A | N/A | N/A | N/A | N/A |
|  |  |  | 50 | 63.7 | 57.1 | 6.6 | 64.8 | 63.9 | 63.1 | 1.1 | 0.3 | -0.5 |
|  |  |  | 120 | 61.7 | 59 | 2.7 | 63.8 | 62.6 | 61.6 | 2.1 | 0.9 | -0.1 |

### 4.3 Existing Conditions (2017)

Existing 2017 peak truck hour traffic data were entered into the Existing Conditions modeled scenario to enable loudest-hour prediction of noise levels at all noisesensitive land uses. Under the existing 2017 conditions, traffic noise levels range from $43 \mathrm{~dB}(A) L_{e q}$ to $74 \mathrm{~dB}(A) L_{e q}$ and exceed the NAAC at 238 residences (NAAC B), the South Lake Church/Pre-School/Daycare (NAAC C), Jon Storm Park (NAAC C), and the Atlas Immersion Academy School (NAAC C). Exterior sound levels at the retirement home (NAAC D) are predicted to be $70 \mathrm{~dB}(\mathrm{~A}) \mathrm{L}_{\text {eq }}$ at the façade closest to I-205. Visual inspections of the building identified that the building window type are what FHWA classifies as "storm windows" which result in an interior sound level 25 dB lower (FHWA 2011a), the interior sound level at the retirement home is predicted to be $45 \mathrm{~dB}(\mathrm{~A}) \mathrm{L}_{\text {eq }}$ and is therefore not impacted. Traffic noise levels are highest for outdoor use areas located closest to the I-205 facility. Table 8 provides the summary of exceedances for the Existing Conditions, Table 9 provides a tabular list of existing traffic noise levels for the receptors analyzed, and Figures 3 through 17 show the location of each receptor listed in the table.

## 5 Future Noise Levels

Traffic noise levels were predicted for two future (2045) alternatives: the No Build Alternative and the Build Alternative (Table 10).

### 5.1 No Build Alternative (2045)

No Build Alternative 2045 traffic noise levels are provided in Table 11 and Figures 3 through 17 in Section 11 show the location of each receptor listed in the table. Under the No Build Alternative 2045 conditions, predicted traffic noise levels would range from $45 \mathrm{~dB}(A) L_{\text {eq }}$ to $74 \mathrm{~dB}(A) L_{\text {eq }}$ and would exceed the NAAC at 281 residences (NAAC B), the South Lake Church/Pre-School/Daycare (NAAC C), Jon Storm Park (NAAC C), and the Atlas Immersion Academy School (NAAC C). Traffic noise levels are predicted to increase up to 4 dB under the No Build Alternative due to increased traffic volumes on area roadways. On average, traffic noise would increase by 1 dB over existing conditions. Exterior sound levels at the retirement home (NAAC D) are predicted to be $70 \mathrm{~dB}(\mathrm{~A}) \mathrm{L}_{\text {eq }}$ at the façade closest to $\mathrm{l}-205$. Visual inspections of the building identified that the building window type are what FHWA classifies as "storm windows" which result in an interior sound level $25 \mathrm{~dB}(\mathrm{~A})$ lower; therefore, the interior sound level at the retirement home is predicted to be $45 \mathrm{~dB}(\mathrm{~A}) \mathrm{L}_{\text {eq }}$ and therefore would not be impacted. As with the existing conditions, traffic noise levels would be highest for outdoor use areas located closest to the I-205 facility.

### 5.2 Build Alternative (2045)

Build Alternative 2045 traffic noise levels are provided in Table 11 and Figures 18 to 32 (Build alt) in Section 11 show the location of each receptor listed in the table.

Under the Build Alternative 2045 conditions, predicted traffic noise levels would range from $45 \mathrm{~dB}(A) L_{\text {eq }}$ to $75 \mathrm{~dB}(A) \mathrm{L}_{\text {eq }}$. Traffic noise impacts would occur at 351 residences (NAAC B), the South Lake Church/Pre-School/Daycare (NAAC C), a pool at the Jamestown Plaza Apartments (NAAC C), Jon Storm Park (NAAC C), and at the Atlas Immersion Academy School (NAAC C). No substantial increases in noise would result from the Build Alternative. Exterior sound levels at the retirement home (NAAC D) are predicted to be $70 \mathrm{~dB}(\mathrm{~A}) \mathrm{L}_{\text {eq }}$ at the façade closest to $\mathrm{I}-205$. Visual inspections of the building identified that the building window type are what FHWA classifies as "storm windows" which result in an interior sound level $25 \mathrm{~dB}(\mathrm{~A})$ lower (FHWA, 2011); therefore, the interior sound level at the retirement home is predicted to be $45 \mathrm{~dB}(\mathrm{~A}) \mathrm{L}_{\mathrm{eq}}$ at the closest point to the highway and would not be impacted. Compared to the existing conditions, traffic noise levels are predicted to increase by up to $5 \mathrm{~dB}(\mathrm{~A})$, depending on the proximity of a receptor to the widened roadway. There are nine receptors where sound levels would be one to three dB lower under the Build Alternative 2045 conditions, specifically R183, R185, R349 to R350, R439, R444, and R445. The reductions in sound levels would occur because of changes in horizontal and/or vertical alignment resulting in increased shielding in some of these locations. Traffic noise levels would be highest for outdoor use areas located closest to the proposed l-205 facility. Traffic noise abatement measures were evaluated for each of the impacts and the results of this analysis are provided in Section 7 of this report.

Each receptor is shown in Figures 18 to 32 with a color-coded dot that indicates the status of each receptor according to its 2045 Build noise level, both with and without a noise barrier, if one is shown opposite the receptor. The color code and corresponding receptor status are as follows:

- Light blue - impacted (without noise barrier) and 5 or $6 \mathrm{~dB}(\mathrm{~A})$ of insertion loss (with noise barrier);
- Dark blue - impacted (without noise barrier) and $7 \mathrm{~dB}(\mathrm{~A})$ or more of insertion loss (with noise barrier);
- Red - impacted (without noise barrier) and not benefited, i.e. less than $5 \mathrm{~dB}(\mathrm{~A})$ of insertion loss (with noise barrier);
- Green - not impacted (without noise barrier) and benefited (with noise barrier); and
- Yellow - not impacted (without noise barrier) or benefited (with noise barrier).

A summary of exceedance conditions for the conditions/alternatives analyzed are provided in Table 8.

Table 8. Summary of Exceedance Conditions for the Existing Conditions and No Build and Build Alternatives

|  |  | Land Use and NAAC |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{array}{c}\text { Impact } \\ \text { Residential } \\ \text { Exterior }\end{array}$ | $\begin{array}{c}\text { Recreational } \\ \text { Exterior (C)* }\end{array}$ | $\begin{array}{c}\text { Institutional } \\ \text { Interior (D) }\end{array}$ | $\begin{array}{c}\text { Commercial } \\ \text { Exterior (E) }\end{array}$ |  |
| Condition/Alternative | Type | NAAC | 238 | 7 | 0 |$] 0$

Notes: *Exceedances at NAAC C uses under the Existing and No Build Alternative include the South Lake Church/Pre-School/Daycare, five outdoor uses at Jon Storm Park, and at the Atlas Immersion Academy School and under the Build Alternative include the same uses in addition to a pool at the Jamestown Plaza Apartments.

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | $\begin{aligned} & \text { ODOT } \\ & \text { Criteria } \\ & \text { NAAC } \end{aligned}$ |  | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing 2017 TNM + StructureBorne Leq dB(A) | No Build 2040 <br> Alternative Leq dB(A) | No Build 2040 TNM + <br> StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM + StructureBorne Leq dB(A) | Build 2040 <br> Increase over Existing Noise Level dB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LT-1/ST-1 | Church, Daycare, School | C (65) | 1 | N/A | 69 | 69 | 70 | 70 | 1 | 69 | 69 | 0 |
| ST-2 | Residence | B (65) | 1 | N/A | 63 | 63 | 63 | 63 | 0 | 66 | 66 | 3 |
| ST-3 | Residence | B (65) | 1 | N/A | 67 | 67 | 68 | 68 | 1 | 70 | 70 | 3 |
| ST-4 | Residence | B (65) | 1 | N/A | 67 | 67 | 68 | 68 | 1 | 69 | 69 | 2 |
| ST-5a | Residence | B (65) | 1 | N/A | 72 | 72 | 73 | 73 | 1 | 73 | 73 | 1 |
| ST-5b | Residence | B (65) | 1 | N/A | 66 | 66 | 66 | 66 | 0 | 68 | 68 | 2 |
| ST-6 | Play Structure at Apts. | C (65) | 1 | N/A | 60 | 60 | 61 | 61 | 1 | 63 | 63 | 3 |
| ST-7 | Residence | B (65) | 1 | N/A | 64 | 64 | 64 | 64 | 0 | 65 | 65 | 1 |
| ST-8 | Residence | B (65) | 1 | N/A | 63 | 63 | 63 | 63 | 0 | 65 | 65 | 2 |
| ST-9 | Residence | B (65) | 1 | N/A | 60 | 60 | 61 | 61 | 1 | 65 | 65 | 5 |
| $\begin{gathered} \hline \text { LT-2/ST- } \\ 10 \\ \hline \end{gathered}$ | Residence | B (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 64 | 64 | 1 |
| ST-11 | Residence | B (65) | 1 | N/A | 57 | 57 | 58 | 58 | 1 | 58 | 58 | 1 |
| ST-12 | Residence | B (65) | 1 | 60 | 59 | 63 | 59 | 63 | 0 | 60 | 63 | 0 |
| ST-13 | Jon Storm Park | C (65) | 1 | 64 | 66 | 68 | 66 | 68 | 0 | 66 | 68 | 0 |
| R1 | Residence | B (65) | 1 | N/A | 70 | 70 | 71 | 71 | 1 | 70 | 70 | 0 |
| R2 | Residence | B (65) | 1 | N/A | 64 | 64 | 64 | 64 | 0 | 65 | 65 | 1 |
| R3 | Residence | B (65) | 2 | N/A | 60 | 60 | 61 | 61 | 1 | 62 | 62 | 2 |
| R4 | Residence | B (65) | 1 | N/A | 60 | 60 | 61 | 61 | 1 | 61 | 61 | 1 |
| R5 | Residence | B (65) | 1 | N/A | 70 | 70 | 71 | 71 | 1 | 71 | 71 | 1 |
| R6 | Residence | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 66 | 66 | 2 |
| R7 | Residence | B (65) | 1 | N/A | 65 | 65 | 65 | 65 | 0 | 66 | 66 | 1 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | ODOT Criteria NAAC | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing <br> 2017 TNM <br> + <br> StructureBorne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + <br> StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM + StructureBorne Leq dB(A) | $\begin{gathered} \text { Build } \\ 2040 \\ \text { Increase } \\ \text { over } \\ \text { Existing } \\ \text { Noise } \\ \text { Level } \\ \text { dB } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R8 | Residence | B (65) | 1 | N/A | 55 | 55 | 56 | 56 | 1 | 57 | 57 | 2 |
| R9 | Residence | B (65) | 1 | N/A | 58 | 58 | 58 | 58 | 0 | 61 | 61 | 3 |
| R10 | Residence | B (65) | 1 | N/A | 57 | 57 | 57 | 57 | 0 | 61 | 61 | 4 |
| R11 | Residence | B (65) | 1 | N/A | 58 | 58 | 59 | 59 | 1 | 62 | 62 | 4 |
| R12 | Residence | B (65) | 1 | N/A | 70 | 70 | 70 | 70 | 0 | 72 | 72 | 2 |
| R13 | Residence | B (65) | 1 | N/A | 67 | 67 | 67 | 67 | 0 | 68 | 68 | 1 |
| R14 | Residence | B (65) | 1 | N/A | 66 | 66 | 66 | 66 | 0 | 66 | 66 | 0 |
| R15 | Residence | B (65) | 1 | N/A | 71 | 71 | 71 | 71 | 0 | 72 | 72 | 1 |
| R16 | Residence | B (65) | 1 | N/A | 67 | 67 | 68 | 68 | 1 | 69 | 69 | 2 |
| R17 | Residence | B (65) | 1 | N/A | 54 | 54 | 54 | 54 | 0 | 55 | 55 | 1 |
| R18 | Residence | B (65) | 1 | N/A | 58 | 58 | 58 | 58 | 0 | 60 | 60 | 2 |
| R19 | Residence | B (65) | 1 | N/A | 62 | 62 | 62 | 62 | 0 | 64 | 64 | 2 |
| R20 | Residence | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 67 | 67 | 3 |
| R21 | Residence | B (65) | 1 | N/A | 70 | 70 | 71 | 71 | 1 | 72 | 72 | 2 |
| R22 | Residence | B (65) | 1 | N/A | 72 | 72 | 72 | 72 | 0 | 74 | 74 | 2 |
| R23 | Residence | B (65) | 1 | N/A | 72 | 72 | 72 | 72 | 0 | 73 | 73 | 1 |
| R24 | Residence | B (65) | 1 | N/A | 72 | 72 | 73 | 73 | 1 | 74 | 74 | 2 |
| R25 | Residence | B (65) | 1 | N/A | 73 | 73 | 73 | 73 | 0 | 74 | 74 | 1 |
| R26 | Residence | B (65) | 1 | N/A | 73 | 73 | 73 | 73 | 0 | 74 | 74 | 1 |
| R27 | Residence | B (65) | 1 | N/A | 73 | 73 | 73 | 73 | 0 | 74 | 74 | 1 |
| R28 | Residence | B (65) | 1 | N/A | 72 | 72 | 73 | 73 | 1 | 74 | 74 | 2 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | $\begin{aligned} & \text { ODOT } \\ & \text { Criteria } \\ & \text { NAAC } \end{aligned}$ | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing 2017 TNM + StructureBorne Leq dB(A) | No Build 2040 <br> Alternative Leq dB(A) | No Build 2040 TNM + <br> StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM + StructureBorne Leq dB(A) | Build 2040 <br> Increase over Existing Noise Level dB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R29 | Residence | B (65) | 1 | N/A | 73 | 73 | 74 | 74 | 1 | 75 | 75 | 2 |
| R30 | Residence | B (65) | 1 | N/A | 72 | 72 | 72 | 72 | 0 | 73 | 73 | 1 |
| R31 | Residence | B (65) | 1 | N/A | 73 | 73 | 73 | 73 | 0 | 74 | 74 | 1 |
| R32 | Residence | B (65) | 1 | N/A | 73 | 73 | 73 | 73 | 0 | 74 | 74 | 1 |
| R33 | Residence | B (65) | 1 | N/A | 74 | 74 | 74 | 74 | 0 | 75 | 75 | 1 |
| R34 | Residence | B (65) | 1 | N/A | 67 | 67 | 68 | 68 | 1 | 69 | 69 | 2 |
| R35 | Residence | B (65) | 1 | N/A | 67 | 67 | 67 | 67 | 0 | 69 | 69 | 2 |
| R36 | Residence | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 68 | 68 | 3 |
| R37 | Residence | B (65) | 1 | N/A | 65 | 65 | 65 | 65 | 0 | 67 | 67 | 2 |
| R38 | Residence | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 67 | 67 | 2 |
| R39 | Residence | B (65) | 1 | N/A | 65 | 65 | 65 | 65 | 0 | 67 | 67 | 2 |
| R40 | Residence | B (65) | 1 | N/A | 65 | 65 | 65 | 65 | 0 | 67 | 67 | 2 |
| R41 | Residence | B (65) | 1 | N/A | 63 | 63 | 63 | 63 | 0 | 66 | 66 | 3 |
| R42 | Residence | B (65) | 1 | N/A | 61 | 61 | 61 | 61 | 0 | 64 | 64 | 3 |
| R43 | Residence | B (65) | 1 | N/A | 62 | 62 | 62 | 62 | 0 | 64 | 64 | 2 |
| R44 | Residence | B (65) | 1 | N/A | 62 | 62 | 62 | 62 | 0 | 64 | 64 | 2 |
| R45 | Residence | B (65) | 1 | N/A | 62 | 62 | 62 | 62 | 0 | 64 | 64 | 2 |
| R46 | Residence | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 64 | 64 | 3 |
| R47 | Residence | B (65) | 1 | N/A | 62 | 62 | 62 | 62 | 0 | 64 | 64 | 2 |
| R48 | Residence | B (65) | 1 | N/A | 63 | 63 | 63 | 63 | 0 | 64 | 64 | 1 |
| R49 | Residence | B (65) | 1 | N/A | 65 | 65 | 65 | 65 | 0 | 66 | 66 | 1 |

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ODOT | K19786 I-205: Stafford Rd to OR 213 Corridor Widening \& Abernethy Bridge Seismic Retrofit / Widening

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | $\begin{aligned} & \text { ODOT } \\ & \text { Criteria } \\ & \text { NAAC } \end{aligned}$ | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing <br> 2017 TNM <br> + <br> StructureBorne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + <br> StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM $+$ StructureBorne Leq dB(A) | Build <br> 2040 <br> Increase over Existing Noise Level dB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R50 | Residence | B (65) | 1 | N/A | 73 | 73 | 74 | 74 | 1 | 74 | 74 | 1 |
| R51 | Residence | B (65) | 1 | N/A | 70 | 70 | 70 | 70 | 0 | 70 | 70 | 0 |
| R52 | Residence | B (65) | 1 | N/A | 67 | 67 | 68 | 68 | 1 | 69 | 69 | 2 |
| R53 | Residence | B (65) | 1 | N/A | 66 | 66 | 67 | 67 | 1 | 67 | 67 | 1 |
| R54 | Residence | B (65) | 1 | N/A | 62 | 62 | 62 | 62 | 0 | 63 | 63 | 1 |
| R55 | Residence | B (65) | 1 | N/A | 66 | 66 | 67 | 67 | 1 | 67 | 67 | 1 |
| R56 | Residence | B (65) | 1 | N/A | 67 | 67 | 67 | 67 | 0 | 67 | 67 | 0 |
| R57 | Residence | B (65) | 1 | N/A | 67 | 67 | 67 | 67 | 0 | 67 | 67 | 0 |
| R58 | Residence | B (65) | 1 | N/A | 66 | 66 | 67 | 67 | 1 | 67 | 67 | 1 |
| R59 | Residence | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 65 | 65 | 1 |
| R60 | Residence | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 66 | 66 | 1 |
| R61 | Residence | B (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 64 | 64 | 1 |
| R62 | Residence | B (65) | 1 | N/A | 65 | 65 | 65 | 65 | 0 | 66 | 66 | 1 |
| R63 | Residence | B (65) | 1 | N/A | 71 | 71 | 71 | 71 | 0 | 72 | 72 | 1 |
| R64 | Residence | B (65) | 1 | N/A | 72 | 72 | 72 | 72 | 0 | 73 | 73 | 1 |
| R65 | Residence | B (65) | 1 | N/A | 72 | 72 | 73 | 73 | 1 | 74 | 74 | 2 |
| R66 | Residence | B (65) | 1 | N/A | 70 | 70 | 70 | 70 | 0 | 72 | 72 | 2 |
| R67 | Residence | B (65) | 1 | N/A | 66 | 66 | 66 | 66 | 0 | 68 | 68 | 2 |
| R68 | Residence | B (65) | 1 | N/A | 65 | 65 | 65 | 65 | 0 | 67 | 67 | 2 |
| R69 | Residence | B (65) | 1 | N/A | 63 | 63 | 63 | 63 | 0 | 64 | 64 | 1 |
| R70 | Residence | B (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 65 | 65 | 2 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | ODOT <br> Criteria NAAC | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing 2017 TNM + Structure- Borne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + <br> StructureBorne Leq dB(A) | No <br> Build <br> 2040 <br> Increase <br> over <br> Existing <br> Noise <br> Level <br> dB | Build Alternative Leq dB(A) | Build 2040 TNM + StructureBorne Leq dB(A) | $\begin{gathered} \text { Build } \\ 2040 \\ \text { Increase } \\ \text { over } \\ \text { Existing } \\ \text { Noise } \\ \text { Level } \\ \text { dB } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R71 | Residence | B (65) | 1 | N/A | 65 | 65 | 65 | 65 | 0 | 66 | 66 | 1 |
| R72 | Residence | B (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 65 | 65 | 2 |
| R73 | Residence | B (65) | 1 | N/A | 65 | 65 | 65 | 65 | 0 | 67 | 67 | 2 |
| R74 | Residence | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 66 | 66 | 2 |
| R75 | Residence | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 67 | 67 | 2 |
| R76 | Retirement Home (no outdoor use) | D (50)* | 1 | N/A | 45 | 45 | 45 | 45 | 0 | 45 | 45 | 0 |
| R77 | Pool at Apts. | C (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 66 | 66 | 3 |
| R78 | Multi-Family | B (65) | 1 | N/A | 65 | 65 | 65 | 65 | 0 | 66 | 66 | 1 |
| R79 | Multi-Family | B (65) | 1 | N/A | 64 | 64 | 64 | 64 | 0 | 65 | 65 | 1 |
| R80 | Multi-Family | B (65) | 1 | N/A | 68 | 68 | 69 | 69 | 1 | 70 | 70 | 2 |
| R81 | Multi-Family | B (65) | 1 | N/A | 68 | 68 | 68 | 68 | 0 | 69 | 69 | 1 |
| R82 | Multi-Family | B (65) | 1 | N/A | 57 | 57 | 57 | 57 | 0 | 59 | 59 | 2 |
| R83 | Multi-Family | B (65) | 1 | N/A | 57 | 57 | 57 | 57 | 0 | 58 | 58 | 1 |
| R84 | Multi-Family | B (65) | 1 | N/A | 61 | 61 | 61 | 61 | 0 | 62 | 62 | 1 |
| R85 | Multi-Family | B (65) | 1 | N/A | 60 | 60 | 61 | 61 | 1 | 61 | 61 | 1 |
| R86 | Multi-Family | B (65) | 1 | N/A | 50 | 50 | 50 | 50 | 0 | 53 | 53 | 3 |
| R87 | Multi-Family | B (65) | 1 | N/A | 53 | 53 | 53 | 53 | 0 | 55 | 55 | 2 |
| R88 | Multi-Family | B (65) | 1 | N/A | 53 | 53 | 54 | 54 | 1 | 55 | 55 | 2 |
| R89 | Multi-Family | B (65) | 1 | N/A | 56 | 56 | 56 | 56 | 0 | 57 | 57 | 1 |
| R90 | Multi-Family | B (65) | 1 | N/A | 53 | 53 | 53 | 53 | 0 | 54 | 54 | 1 |
| R91 | Multi-Family | B (65) | 1 | N/A | 52 | 52 | 53 | 53 | 1 | 54 | 54 | 2 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | $\begin{aligned} & \text { ODOT } \\ & \text { Criteria } \\ & \text { NAAC } \end{aligned}$ | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing <br> 2017 TNM + <br> StructureBorne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + StructureBorne Leq dB(A) | No <br> Build <br> 2040 <br> Increase <br> over <br> Existing <br> Noise <br> Level <br> dB | Build Alternative Leq dB(A) | Build 2040 TNM + StructureBorne Leq dB(A) | Build <br> 2040 <br> Increase over Existing Noise Level dB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R92 | Multi-Family | B (65) | 1 | N/A | 55 | 55 | 56 | 56 | 1 | 56 | 56 | 1 |
| R93 | Multi-Family | B (65) | 1 | N/A | 55 | 55 | 55 | 55 | 0 | 56 | 56 | 1 |
| R94 | Multi-Family | B (65) | 1 | N/A | 60 | 60 | 60 | 60 | 0 | 63 | 63 | 3 |
| R95 | Multi-Family | B (65) | 1 | N/A | 60 | 60 | 60 | 60 | 0 | 63 | 63 | 3 |
| R96 | Multi-Family | B (65) | 1 | N/A | 64 | 64 | 64 | 64 | 0 | 65 | 65 | 1 |
| R97 | Multi-Family | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 65 | 65 | 1 |
| R98 | Multi-Family | B (65) | 1 | N/A | 63 | 63 | 63 | 63 | 0 | 65 | 65 | 2 |
| R99 | Multi-Family | B (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 65 | 65 | 2 |
| R100 | Multi-Family | B (65) | 1 | N/A | 68 | 68 | 69 | 69 | 1 | 69 | 69 | 1 |
| R101 | Multi-Family | B (65) | 1 | N/A | 68 | 68 | 68 | 68 | 0 | 69 | 69 | 1 |
| R102 | Multi-Family | B (65) | 1 | N/A | 57 | 57 | 58 | 58 | 1 | 60 | 60 | 3 |
| R103 | Multi-Family | B (65) | 1 | N/A | 57 | 57 | 58 | 58 | 1 | 61 | 61 | 4 |
| R104 | Multi-Family | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 63 | 63 | 1 |
| R105 | Multi-Family | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 63 | 63 | 1 |
| R106 | Multi-Family | B (65) | 1 | N/A | 47 | 47 | 47 | 47 | 0 | 52 | 52 | 5 |
| R107 | Multi-Family | B (65) | 1 | N/A | 47 | 47 | 47 | 47 | 0 | 51 | 51 | 4 |
| R108 | Multi-Family | B (65) | 1 | N/A | 50 | 50 | 50 | 50 | 0 | 54 | 54 | 4 |
| R109 | Multi-Family | B (65) | 1 | N/A | 49 | 49 | 50 | 50 | 1 | 54 | 54 | 5 |
| R110 | Multi-Family | B (65) | 1 | N/A | 52 | 52 | 52 | 52 | 0 | 55 | 55 | 3 |
| R111 | Multi-Family | B (65) | 1 | N/A | 48 | 48 | 49 | 49 | 1 | 51 | 51 | 3 |
| R112 | Multi-Family | B (65) | 1 | N/A | 55 | 55 | 56 | 56 | 1 | 57 | 57 | 2 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | ODOT Criteria NAAC | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing 2017 TNM + <br> StructureBorne <br> Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + <br> StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM + <br> StructureBorne Leq dB(A) | Build <br> 2040 <br> Increase over Existing Noise Level dB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R113 | Multi-Family | B (65) | 1 | N/A | 51 | 51 | 51 | 51 | 0 | 53 | 53 | 2 |
| R114 | Residence | B (65) | 1 | N/A | 64 | 64 | 64 | 64 | 0 | 65 | 65 | 1 |
| R115 | Residence | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 66 | 66 | 1 |
| R116 | Residence | B (65) | 1 | N/A | 66 | 66 | 67 | 67 | 1 | 67 | 67 | 1 |
| R117 | Residence | B (65) | 1 | N/A | 67 | 67 | 68 | 68 | 1 | 69 | 69 | 2 |
| R118 | Residence | B (65) | 1 | N/A | 69 | 69 | 69 | 69 | 0 | 70 | 70 | 1 |
| R119 | Residence | B (65) | 1 | N/A | 68 | 68 | 69 | 69 | 1 | 70 | 70 | 2 |
| R120 | Residence | B (65) | 1 | N/A | 68 | 68 | 68 | 68 | 0 | 69 | 69 | 1 |
| R121 | Residence | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 67 | 67 | 2 |
| R122 | Residence | B (65) | 1 | N/A | 67 | 67 | 68 | 68 | 1 | 68 | 68 | 1 |
| R123 | Residence | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 66 | 66 | 1 |
| R124 | Residence | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 66 | 66 | 2 |
| R125 | Residence | B (65) | 1 | N/A | 63 | 63 | 63 | 63 | 0 | 64 | 64 | 1 |
| R126 | Residence | B (65) | 1 | N/A | 66 | 66 | 66 | 66 | 0 | 68 | 68 | 2 |
| R127 | Residence | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 66 | 66 | 2 |
| R128 | Residence | B (65) | 1 | N/A | 66 | 66 | 66 | 66 | 0 | 68 | 68 | 2 |
| R129 | Residence | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 66 | 66 | 2 |
| R130 | Residence | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 65 | 65 | 1 |
| R131 | Residence | B (65) | 1 | N/A | 64 | 64 | 64 | 64 | 0 | 65 | 65 | 1 |
| R132 | Residence | B (65) | 1 | N/A | 60 | 60 | 61 | 61 | 1 | 61 | 61 | 1 |
| R133 | Residence | B (65) | 1 | N/A | 65 | 65 | 65 | 65 | 0 | 67 | 67 | 2 |

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Table 9. Predicted Noise Levels

| Receptor ID | Land Use | ODOT <br> Criteria NAAC | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | $\begin{gathered} \text { Existing } \\ 2017 \text { TNM } \\ + \\ \text { Structure- } \\ \text { Borne } \\ \text { Leq dB(A) } \end{gathered}$ | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + <br> StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM + StructureBorne Leq dB(A) | Build <br> 2040 <br> Increase over Existing Noise Level dB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R134 | Residence | B (65) | 1 | N/A | 66 | 66 | 66 | 66 | 0 | 67 | 67 | 1 |
| R135 | Residence | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 67 | 67 | 2 |
| R136 | Residence | B (65) | 1 | N/A | 66 | 66 | 67 | 67 | 1 | 68 | 68 | 2 |
| R137 | Residence | B (65) | 1 | N/A | 67 | 67 | 68 | 68 | 1 | 69 | 69 | 2 |
| R138 | Residence | B (65) | 1 | N/A | 66 | 66 | 66 | 66 | 0 | 68 | 68 | 2 |
| R139 | Residence | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 68 | 68 | 3 |
| R140 | Residence | B (65) | 1 | N/A | 66 | 66 | 67 | 67 | 1 | 69 | 69 | 3 |
| R141 | Residence | B (65) | 1 | N/A | 67 | 67 | 67 | 67 | 0 | 68 | 68 | 1 |
| R142 | Residence | B (65) | 1 | N/A | 66 | 66 | 67 | 67 | 1 | 68 | 68 | 2 |
| R143 | Residence | B (65) | 1 | N/A | 67 | 67 | 68 | 68 | 1 | 69 | 69 | 2 |
| R144 | Residence | B (65) | 1 | N/A | 68 | 68 | 68 | 68 | 0 | 70 | 70 | 2 |
| R145 | Residence | B (65) | 1 | N/A | 67 | 67 | 67 | 67 | 0 | 68 | 68 | 1 |
| R146 | Residence | B (65) | 1 | N/A | 68 | 68 | 68 | 68 | 0 | 69 | 69 | 1 |
| R147 | Residence | B (65) | 1 | N/A | 66 | 66 | 66 | 66 | 0 | 68 | 68 | 2 |
| R148 | Residence | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 68 | 68 | 3 |
| R149 | Residence | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 68 | 68 | 3 |
| R150 | Residence | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 66 | 66 | 2 |
| R151 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 64 | 64 | 2 |
| R152 | Residence | B (65) | 1 | N/A | 63 | 63 | 63 | 63 | 0 | 65 | 65 | 2 |
| R153 | Residence | B (65) | 1 | N/A | 63 | 63 | 63 | 63 | 0 | 65 | 65 | 2 |
| R154 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 64 | 64 | 2 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | ODOT Criteria NAAC | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing 2017 TNM $+$ <br> StructureBorne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM + StructureBorne Leq dB(A) | $\begin{gathered} \text { Build } \\ 2040 \\ \text { Increase } \\ \text { over } \\ \text { Existing } \\ \text { Noise } \\ \text { Level } \\ \text { dB } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R155 | Residence | B (65) | 1 | N/A | 64 | 64 | 64 | 64 | 0 | 66 | 66 | 2 |
| R156 | Residence | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 67 | 67 | 2 |
| R157 | Residence | B (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 65 | 65 | 2 |
| R158 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 64 | 64 | 2 |
| R159 | Residence | B (65) | 1 | N/A | 59 | 59 | 60 | 60 | 1 | 61 | 61 | 2 |
| R160 | Residence | B (65) | 1 | N/A | 63 | 63 | 63 | 63 | 0 | 64 | 64 | 1 |
| R161 | Residence | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 63 | 63 | 2 |
| R162 | Residence | B (65) | 1 | N/A | 60 | 60 | 61 | 61 | 1 | 63 | 63 | 3 |
| R163 | Residence | B (65) | 1 | N/A | 61 | 61 | 61 | 61 | 0 | 63 | 63 | 2 |
| R164 | Residence | B (65) | 1 | N/A | 60 | 60 | 61 | 61 | 1 | 62 | 62 | 2 |
| R165 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 64 | 64 | 2 |
| R166 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 64 | 64 | 2 |
| R167 | Residence | B (65) | 1 | N/A | 62 | 62 | 62 | 62 | 0 | 64 | 64 | 2 |
| R168 | Multi-Family | B (65) | 1 | N/A | 65 | 65 | 65 | 65 | 0 | 68 | 68 | 3 |
| R169 | Multi-Family | B (65) | 1 | N/A | 65 | 65 | 65 | 65 | 0 | 68 | 68 | 3 |
| R170 | Multi-Family | B (65) | 1 | N/A | 59 | 59 | 60 | 60 | 1 | 60 | 60 | 1 |
| R171 | Multi-Family | B (65) | 1 | N/A | 64 | 64 | 64 | 64 | 0 | 65 | 65 | 1 |
| R172 | Multi-Family | B (65) | 1 | N/A | 70 | 70 | 71 | 71 | 1 | 71 | 71 | 1 |
| R173 | Multi-Family | B (65) | 1 | N/A | 59 | 59 | 59 | 59 | 0 | 60 | 60 | 1 |
| R174 | Multi-Family | B (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 65 | 65 | 2 |
| R175 | Multi-Family | B (65) | 1 | N/A | 69 | 69 | 70 | 70 | 1 | 71 | 71 | 2 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | $\begin{aligned} & \text { ODOT } \\ & \text { Criteria } \\ & \text { NAAC } \end{aligned}$ | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing <br> 2017 TNM + <br> StructureBorne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM + StructureBorne Leq dB(A) | Build <br> 2040 <br> Increase over Existing Noise Level dB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R176 | Multi-Family | B (65) | 1 | N/A | 59 | 59 | 60 | 60 | 1 | 60 | 60 | 1 |
| R177 | Multi-Family | B (65) | 1 | N/A | 65 | 65 | 65 | 65 | 0 | 65 | 65 | 0 |
| R178 | Multi-Family | B (65) | 1 | N/A | 70 | 70 | 70 | 70 | 0 | 71 | 71 | 1 |
| R179 | Multi-Family | B (65) | 1 | N/A | 59 | 59 | 59 | 59 | 0 | 60 | 60 | 1 |
| R180 | Multi-Family | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 65 | 65 | 1 |
| R181 | Multi-Family | B (65) | 1 | N/A | 69 | 69 | 70 | 70 | 1 | 71 | 71 | 2 |
| R182 | Multi-Family | B (65) | 1 | N/A | 57 | 57 | 57 | 57 | 0 | 59 | 59 | 2 |
| R183 | Multi-Family | B (65) | 1 | N/A | 63 | 63 | 63 | 63 | 0 | 62 | 62 | -1 |
| R184 | Multi-Family | B (65) | 1 | N/A | 57 | 57 | 58 | 58 | 1 | 59 | 59 | 2 |
| R185 | Multi-Family | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 63 | 63 | -1 |
| R186 | Multi-Family | B (65) | 1 | N/A | 61 | 61 | 61 | 61 | 0 | 63 | 63 | 2 |
| R187 | Multi-Family | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 67 | 67 | 2 |
| R188 | Multi-Family | B (65) | 1 | N/A | 61 | 61 | 61 | 61 | 0 | 63 | 63 | 2 |
| R189 | Multi-Family | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 67 | 67 | 2 |
| R190 | Multi-Family | B (65) | 1 | N/A | 60 | 60 | 61 | 61 | 1 | 63 | 63 | 3 |
| R191 | Multi-Family | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 67 | 67 | 2 |
| R192 | Multi-Family | B (65) | 1 | N/A | 60 | 60 | 60 | 60 | 0 | 63 | 63 | 3 |
| R193 | Multi-Family | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 67 | 67 | 2 |
| R194 | Multi-Family | B (65) | 1 | N/A | 59 | 59 | 60 | 60 | 1 | 61 | 61 | 2 |
| R195 | Multi-Family | B (65) | 1 | N/A | 65 | 65 | 65 | 65 | 0 | 67 | 67 | 2 |
| R196 | Multi-Family | B (65) | 1 | N/A | 59 | 59 | 60 | 60 | 1 | 61 | 61 | 2 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | $\begin{aligned} & \text { ODOT } \\ & \text { Criteria } \\ & \text { NAAC } \end{aligned}$ | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing 2017 TNM + StructureBorne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM + StructureBorne Leq dB(A) | Build <br> 2040 <br> Increase over Existing Noise Level dB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R197 | Multi-Family | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 67 | 67 | 3 |
| R198 | Multi-Family | B (65) | 1 | N/A | 59 | 59 | 59 | 59 | 0 | 60 | 60 | 1 |
| R199 | Multi-Family | B (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 66 | 66 | 3 |
| R200 | Multi-Family | B (65) | 1 | N/A | 58 | 58 | 59 | 59 | 1 | 60 | 60 | 2 |
| R201 | Multi-Family | B (65) | 1 | N/A | 63 | 63 | 63 | 63 | 0 | 65 | 65 | 2 |
| R202 | Multi-Family | B (65) | 1 | N/A | 58 | 58 | 59 | 59 | 1 | 60 | 60 | 2 |
| R203 | Multi-Family | B (65) | 1 | N/A | 63 | 63 | 63 | 63 | 0 | 65 | 65 | 2 |
| R204 | Multi-Family | B (65) | 1 | N/A | 57 | 57 | 58 | 58 | 1 | 59 | 59 | 2 |
| R205 | Multi-Family | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 64 | 64 | 3 |
| R206 | Multi-Family | B (65) | 1 | N/A | 58 | 58 | 59 | 59 | 1 | 60 | 60 | 2 |
| R207 | Multi-Family | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 65 | 65 | 3 |
| R208 | Multi-Family | B (65) | 1 | N/A | 58 | 58 | 59 | 59 | 1 | 60 | 60 | 2 |
| R209 | Multi-Family | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 65 | 65 | 3 |
| R210 | Multi-Family | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 67 | 67 | 3 |
| R211 | Multi-Family | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 67 | 67 | 3 |
| R212 | Multi-Family | B (65) | 1 | N/A | 58 | 58 | 58 | 58 | 0 | 60 | 60 | 2 |
| R213 | Multi-Family | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 65 | 65 | 3 |
| R214 | Multi-Family | B (65) | 1 | N/A | 58 | 58 | 58 | 58 | 0 | 60 | 60 | 2 |
| R215 | Multi-Family | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 65 | 65 | 3 |
| R216 | Multi-Family | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 66 | 66 | 2 |
| R217 | Multi-Family | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 67 | 67 | 3 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | $\begin{aligned} & \text { ODOT } \\ & \text { Criteria } \\ & \text { NAAC } \end{aligned}$ | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing <br> 2017 TNM + <br> StructureBorne Leq dB(A) | No Build 2040 <br> Alternative Leq dB(A) | No Build 2040 TNM + StructureBorne Leq dB(A) | No <br> Build <br> 2040 <br> Increase <br> over <br> Existing <br> Noise <br> Level <br> dB | Build Alternative Leq dB(A) | Build 2040 TNM + <br> StructureBorne Leq dB(A) | Build <br> 2040 <br> Increase over Existing Noise Level dB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R218 | Multi-Family | B (65) | 1 | N/A | 58 | 58 | 58 | 58 | 0 | 60 | 60 | 2 |
| R219 | Multi-Family | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 64 | 64 | 2 |
| R220 | Multi-Family | B (65) | 1 | N/A | 58 | 58 | 58 | 58 | 0 | 60 | 60 | 2 |
| R221 | Multi-Family | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 65 | 65 | 3 |
| R222 | Multi-Family | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 66 | 66 | 2 |
| R223 | Multi-Family | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 66 | 66 | 2 |
| R224 | Multi-Family | B (65) | 1 | N/A | 57 | 57 | 57 | 57 | 0 | 59 | 59 | 2 |
| R225 | Multi-Family | B (65) | 1 | N/A | 62 | 62 | 62 | 62 | 0 | 64 | 64 | 2 |
| R226 | Multi-Family | B (65) | 1 | N/A | 70 | 70 | 70 | 70 | 0 | 71 | 71 | 1 |
| R227 | Multi-Family | B (65) | 1 | N/A | 58 | 58 | 58 | 58 | 0 | 59 | 59 | 1 |
| R228 | Multi-Family | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 64 | 64 | 3 |
| R229 | Multi-Family | B (65) | 1 | N/A | 69 | 69 | 69 | 69 | 0 | 71 | 71 | 2 |
| R230 | Multi-Family | B (65) | 1 | N/A | 57 | 57 | 58 | 58 | 1 | 59 | 59 | 2 |
| R231 | Multi-Family | B (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 64 | 64 | 1 |
| R232 | Multi-Family | B (65) | 1 | N/A | 70 | 70 | 71 | 71 | 1 | 71 | 71 | 1 |
| R233 | Multi-Family | B (65) | 1 | N/A | 58 | 58 | 59 | 59 | 1 | 60 | 60 | 2 |
| R234 | Multi-Family | B (65) | 1 | N/A | 63 | 63 | 63 | 63 | 0 | 64 | 64 | 1 |
| R235 | Multi-Family | B (65) | 1 | N/A | 69 | 69 | 70 | 70 | 1 | 70 | 70 | 1 |
| R236 | Multi-Family | B (65) | 1 | N/A | 57 | 57 | 57 | 57 | 0 | 59 | 59 | 2 |
| R237 | Multi-Family | B (65) | 1 | N/A | 60 | 60 | 61 | 61 | 1 | 62 | 62 | 2 |
| R238 | Multi-Family | B (65) | 1 | N/A | 56 | 56 | 57 | 57 | 1 | 58 | 58 | 2 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | ODOT Criteria NAAC | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing 2017 TNM $+$ StructureBorne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + <br> StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM + StructureBorne Leq dB(A) | $\begin{gathered} \text { Build } \\ 2040 \\ \text { Increase } \\ \text { over } \\ \text { Existing } \\ \text { Noise } \\ \text { Level } \\ \text { dB } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R239 | Multi-Family | B (65) | 1 | N/A | 60 | 60 | 60 | 60 | 0 | 62 | 62 | 2 |
| R240 | Multi-Family | B (65) | 1 | N/A | 57 | 57 | 57 | 57 | 0 | 58 | 58 | 1 |
| R241 | Multi-Family | B (65) | 1 | N/A | 61 | 61 | 61 | 61 | 0 | 63 | 63 | 2 |
| R242 | Multi-Family | B (65) | 1 | N/A | 56 | 56 | 57 | 57 | 1 | 58 | 58 | 2 |
| R243 | Multi-Family | B (65) | 1 | N/A | 60 | 60 | 61 | 61 | 1 | 63 | 63 | 3 |
| R244 | Residence | B (65) | 1 | N/A | 60 | 60 | 60 | 60 | 0 | 61 | 61 | 1 |
| R245 | Residence | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 63 | 63 | 2 |
| R246 | Residence | B (65) | 1 | N/A | 61 | 61 | 61 | 61 | 0 | 62 | 62 | 1 |
| R247 | Residence | B (65) | 1 | N/A | 60 | 60 | 60 | 60 | 0 | 62 | 62 | 2 |
| R248 | Residence | B (65) | 1 | N/A | 60 | 60 | 60 | 60 | 0 | 62 | 62 | 2 |
| R249 | Residence | B (65) | 1 | N/A | 59 | 59 | 59 | 59 | 0 | 61 | 61 | 2 |
| R250 | Residence | B (65) | 1 | N/A | 57 | 57 | 57 | 57 | 0 | 60 | 60 | 3 |
| R251 | Residence | B (65) | 1 | N/A | 57 | 57 | 57 | 57 | 0 | 59 | 59 | 2 |
| R252 | Residence | B (65) | 1 | N/A | 57 | 57 | 57 | 57 | 0 | 59 | 59 | 2 |
| R253 | Residence | B (65) | 1 | N/A | 56 | 56 | 56 | 56 | 0 | 59 | 59 | 3 |
| R254 | Residence | B (65) | 1 | N/A | 56 | 56 | 57 | 57 | 1 | 59 | 59 | 3 |
| R255 | Residence | B (65) | 1 | N/A | 56 | 56 | 57 | 57 | 1 | 59 | 59 | 3 |
| R256 | Residence | B (65) | 1 | N/A | 63 | 63 | 63 | 63 | 0 | 64 | 64 | 1 |
| R257 | Residence | B (65) | 1 | N/A | 62 | 62 | 62 | 62 | 0 | 62 | 62 | 0 |
| R258 | Residence | B (65) | 1 | N/A | 61 | 61 | 61 | 61 | 0 | 61 | 61 | 0 |
| R259 | Residence | B (65) | 1 | N/A | 60 | 60 | 60 | 60 | 0 | 61 | 61 | 1 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | $\begin{aligned} & \text { ODOT } \\ & \text { Criteria } \\ & \text { NAAC } \end{aligned}$ | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing <br> 2017 TNM + <br> StructureBorne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM + StructureBorne Leq dB(A) | Build <br> 2040 <br> Increase over Existing Noise Level dB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R260 | Residence | B (65) | 1 | N/A | 59 | 59 | 59 | 59 | 0 | 60 | 60 | 1 |
| R261 | Residence | B (65) | 1 | N/A | 58 | 58 | 58 | 58 | 0 | 59 | 59 | 1 |
| R262 | Residence | B (65) | 1 | N/A | 58 | 58 | 58 | 58 | 0 | 59 | 59 | 1 |
| R263 | Residence | B (65) | 1 | N/A | 57 | 57 | 57 | 57 | 0 | 59 | 59 | 2 |
| R264 | Residence | B (65) | 1 | N/A | 58 | 58 | 58 | 58 | 0 | 61 | 61 | 3 |
| R265 | Residence | B (65) | 1 | N/A | 58 | 58 | 58 | 58 | 0 | 61 | 61 | 3 |
| R266 | Residence | B (65) | 1 | N/A | 55 | 55 | 55 | 55 | 0 | 58 | 58 | 3 |
| R267 | Residence | B (65) | 1 | N/A | 57 | 57 | 57 | 57 | 0 | 59 | 59 | 2 |
| R268 | Residence | B (65) | 1 | N/A | 59 | 59 | 60 | 60 | 1 | 62 | 62 | 3 |
| R269 | Residence | B (65) | 1 | N/A | 61 | 61 | 61 | 61 | 0 | 63 | 63 | 2 |
| R270 | Residence | B (65) | 1 | N/A | 61 | 61 | 61 | 61 | 0 | 63 | 63 | 2 |
| R271 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 65 | 65 | 3 |
| R272 | Residence | B (65) | 1 | N/A | 64 | 64 | 64 | 64 | 0 | 66 | 66 | 2 |
| R273 | Residence | B (65) | 1 | N/A | 66 | 66 | 66 | 66 | 0 | 67 | 67 | 1 |
| R274 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 65 | 65 | 3 |
| R275 | Residence | B (65) | 1 | N/A | 63 | 63 | 63 | 63 | 0 | 65 | 65 | 2 |
| R276 | Residence | B (65) | 1 | N/A | 63 | 63 | 63 | 63 | 0 | 65 | 65 | 2 |
| R277 | Residence | B (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 65 | 65 | 2 |
| R278 | Residence | B (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 65 | 65 | 2 |
| R279 | Residence | B (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 65 | 65 | 2 |
| R280 | Residence | B (65) | 1 | N/A | 63 | 63 | 63 | 63 | 0 | 65 | 65 | 2 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | ODOT <br> Criteria NAAC | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | $\begin{gathered} \text { Existing } \\ 2017 \text { TNM } \\ + \\ \text { Structure- } \\ \text { Borne } \\ \text { Leq dB(A) } \end{gathered}$ | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + <br> StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM + <br> StructureBorne Leq dB(A) | Build <br> 2040 <br> Increase over Existing Noise Level dB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R281 | Residence | B (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 66 | 66 | 3 |
| R282 | Residence | B (65) | 1 | N/A | 64 | 64 | 64 | 64 | 0 | 66 | 66 | 2 |
| R283 | Residence | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 67 | 67 | 3 |
| R284 | Residence | B (65) | 1 | N/A | 64 | 64 | 64 | 64 | 0 | 67 | 67 | 3 |
| R285 | Residence | B (65) | 1 | N/A | 64 | 64 | 64 | 64 | 0 | 67 | 67 | 3 |
| R286 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 64 | 64 | 2 |
| R287 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 64 | 64 | 2 |
| R288 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 65 | 65 | 3 |
| R289 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 64 | 64 | 2 |
| R290 | Residence | B (65) | 1 | N/A | 63 | 63 | 63 | 63 | 0 | 65 | 65 | 2 |
| R291 | Residence | B (65) | 1 | N/A | 63 | 63 | 63 | 63 | 0 | 65 | 65 | 2 |
| R292 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 64 | 64 | 2 |
| R293 | Residence | B (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 65 | 65 | 2 |
| R294 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 64 | 64 | 2 |
| R295 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 65 | 65 | 3 |
| R296 | Residence | B (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 66 | 66 | 3 |
| R297 | Residence | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 69 | 69 | 4 |
| R298 | Residence | B (65) | 1 | N/A | 68 | 68 | 69 | 69 | 1 | 71 | 71 | 3 |
| R299 | Residence | B (65) | 1 | N/A | 68 | 68 | 69 | 69 | 1 | 71 | 71 | 3 |
| R300 | Residence | B (65) | 1 | N/A | 68 | 68 | 68 | 68 | 0 | 70 | 70 | 2 |
| R301 | Residence | B (65) | 1 | N/A | 66 | 66 | 67 | 67 | 1 | 69 | 69 | 3 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | ODOT <br> Criteria <br> NAAC | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing 2017 TNM + StructureBorne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM + StructureBorne Leq dB(A) | Build <br> 2040 <br> Increase over Existing Noise Level dB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R302 | Residence | B (65) | 1 | N/A | 68 | 68 | 68 | 68 | 0 | 70 | 70 | 2 |
| R303 | Residence | B (65) | 1 | N/A | 66 | 66 | 67 | 67 | 1 | 69 | 69 | 3 |
| R304 | Residence | B (65) | 1 | N/A | 66 | 66 | 67 | 67 | 1 | 69 | 69 | 3 |
| R305 | Residence | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 68 | 68 | 3 |
| R306 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 65 | 65 | 3 |
| R307 | Residence | B (65) | 1 | N/A | 62 | 62 | 62 | 62 | 0 | 64 | 64 | 2 |
| R308 | Residence | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 64 | 64 | 3 |
| R309 | Residence | B (65) | 1 | N/A | 62 | 62 | 62 | 62 | 0 | 64 | 64 | 2 |
| R310 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 65 | 65 | 3 |
| R311 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 65 | 65 | 3 |
| R312 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 64 | 64 | 2 |
| R313 | Residence | B (65) | 1 | N/A | 62 | 62 | 62 | 62 | 0 | 64 | 64 | 2 |
| R314 | Residence | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 63 | 63 | 2 |
| R315 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 64 | 64 | 2 |
| R316 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 64 | 64 | 2 |
| R317 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 64 | 64 | 2 |
| R318 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 64 | 64 | 2 |
| R319 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 64 | 64 | 2 |
| R320 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 64 | 64 | 2 |
| R321 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 64 | 64 | 2 |
| R322 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 65 | 65 | 3 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | ODOT <br> Criteria NAAC |  | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing <br> 2017 TNM + <br> StructureBorne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + <br> StructureBorne Leq dB(A) | No <br> Build <br> 2040 <br> Increase <br> over <br> Existing <br> Noise <br> Level <br> dB | Build Alternative Leq dB(A) | Build 2040 TNM + <br> StructureBorne Leq dB(A) | Build <br> 2040 <br> Increase over Existing Noise Level dB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R323 | Residence | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 68 | 68 | 4 |
| R324 | Residence | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 68 | 68 | 4 |
| R325 | Residence | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 67 | 67 | 3 |
| R326 | Residence | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 67 | 67 | 3 |
| R327 | Residence | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 68 | 68 | 4 |
| R328 | Residence | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 68 | 68 | 4 |
| R329 | Residence | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 68 | 68 | 3 |
| R330 | Residence | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 68 | 68 | 3 |
| R331 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 64 | 64 | 2 |
| R332 | Residence | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 64 | 64 | 3 |
| R333 | Residence | B (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 65 | 65 | 2 |
| R334 | Residence | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 64 | 64 | 3 |
| R335 | Residence | B (65) | 1 | N/A | 60 | 60 | 61 | 61 | 1 | 63 | 63 | 3 |
| R336 | Residence | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 64 | 64 | 3 |
| R337 | Residence | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 67 | 67 | 2 |
| R338 | Residence | B (65) | 1 | N/A | 65 | 65 | 65 | 65 | 0 | 67 | 67 | 2 |
| R339 | Residence | B (65) | 1 | N/A | 65 | 65 | 65 | 65 | 0 | 66 | 66 | 1 |
| R340 | Residence | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 67 | 67 | 2 |
| R341 | Residence | B (65) | 1 | N/A | 64 | 64 | 64 | 64 | 0 | 67 | 67 | 3 |
| R342 | Residence | B (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 67 | 67 | 4 |
| R343 | Residence | B (65) | 1 | N/A | 66 | 66 | 66 | 66 | 0 | 69 | 69 | 3 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | $\begin{aligned} & \text { ODOT } \\ & \text { Criteria } \\ & \text { NAAC } \end{aligned}$ | No. of <br> Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing 2017 TNM + <br> StructureBorne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + <br> StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build <br> 2040 TNM $+$ <br> StructureBorne Leq dB(A) | Build <br> 2040 <br> Increase over Existing Noise Level dB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R344 | Residence | B (65) | 1 | N/A | 67 | 67 | 68 | 68 | 1 | 70 | 70 | 3 |
| R345 | Residence | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 68 | 68 | 3 |
| R346 | Residence | B (65) | 1 | N/A | 66 | 66 | 67 | 67 | 1 | 67 | 67 | 1 |
| R347 | Residence | B (65) | 1 | N/A | 67 | 67 | 68 | 68 | 1 | 67 | 67 | 0 |
| R348 | Residence | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 66 | 66 | 1 |
| R349 | Residence | B (65) | 1 | N/A | 67 | 67 | 68 | 68 | 1 | 66 | 66 | -1 |
| R350 | Residence | B (65) | 1 | N/A | 68 | 68 | 69 | 69 | 1 | 67 | 67 | -1 |
| R351 | Residence | B (65) | 1 | N/A | 68 | 68 | 69 | 69 | 1 | 67 | 67 | -1 |
| R352 | Residence | B (65) | 1 | N/A | 68 | 68 | 69 | 69 | 1 | 67 | 67 | -1 |
| R353 | Residence | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 64 | 64 | 3 |
| R354 | Residence | B (65) | 1 | N/A | 56 | 56 | 57 | 57 | 1 | 59 | 59 | 3 |
| R355 | Residence | B (65) | 1 | N/A | 59 | 59 | 60 | 60 | 1 | 62 | 62 | 3 |
| R356 | Residence | B (65) | 1 | N/A | 58 | 58 | 59 | 59 | 1 | 61 | 61 | 3 |
| R357 | Residence | B (65) | 1 | N/A | 55 | 55 | 56 | 56 | 1 | 57 | 57 | 2 |
| R358 | Residence | B (65) | 1 | N/A | 57 | 57 | 58 | 58 | 1 | 59 | 59 | 2 |
| R359 | Residence | B (65) | 1 | N/A | 57 | 57 | 58 | 58 | 1 | 58 | 58 | 1 |
| R360 | Residence | B (65) | 1 | N/A | 67 | 67 | 68 | 68 | 1 | 67 | 67 | 0 |
| R361 | Residence | B (65) | 1 | N/A | 66 | 66 | 67 | 67 | 1 | 67 | 67 | 1 |
| R362 | Residence | B (65) | 1 | N/A | 66 | 66 | 67 | 67 | 1 | 67 | 67 | 1 |
| R363 | Residence | B (65) | 1 | N/A | 66 | 66 | 67 | 67 | 1 | 66 | 66 | 0 |
| R364 | Residence | B (65) | 1 | N/A | 66 | 66 | 67 | 67 | 1 | 66 | 66 | 0 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | ODOT <br> Criteria NAAC |  | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing <br> 2017 TNM + <br> StructureBorne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + <br> StructureBorne Leq dB(A) | No <br> Build <br> 2040 <br> Increase <br> over <br> Existing <br> Noise <br> Level <br> dB | Build Alternative Leq dB(A) | Build 2040 TNM + <br> StructureBorne Leq dB(A) | Build <br> 2040 <br> Increase over Existing Noise Level dB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R365 | Residence | B (65) | 1 | N/A | 55 | 55 | 56 | 56 | 1 | 57 | 57 | 2 |
| R366 | Residence | B (65) | 1 | N/A | 55 | 55 | 55 | 55 | 0 | 57 | 57 | 2 |
| R367 | Residence | B (65) | 1 | N/A | 55 | 55 | 56 | 56 | 1 | 55 | 55 | 0 |
| R368 | Residence | B (65) | 1 | N/A | 51 | 51 | 51 | 51 | 0 | 54 | 54 | 3 |
| R369 | Residence | B (65) | 1 | N/A | 50 | 50 | 51 | 51 | 1 | 52 | 52 | 2 |
| R370 | Residence | B (65) | 1 | N/A | 51 | 51 | 52 | 52 | 1 | 53 | 53 | 2 |
| R371 | Residence | B (65) | 1 | N/A | 66 | 66 | 67 | 67 | 1 | 66 | 66 | 0 |
| R372 | Residence | B (65) | 1 | N/A | 66 | 66 | 67 | 67 | 1 | 66 | 66 | 0 |
| R373 | Residence | B (65) | 1 | N/A | 69 | 69 | 70 | 70 | 1 | 71 | 71 | 2 |
| R374 | Residence | B (65) | 1 | N/A | 70 | 70 | 71 | 71 | 1 | 72 | 72 | 2 |
| R375 | Residence | B (65) | 1 | N/A | 70 | 70 | 71 | 71 | 1 | 72 | 72 | 2 |
| R376 | Residence | B (65) | 1 | N/A | 70 | 70 | 71 | 71 | 1 | 72 | 72 | 2 |
| R377 | Residence | B (65) | 1 | N/A | 69 | 69 | 70 | 70 | 1 | 71 | 71 | 2 |
| R378 | Residence | B (65) | 1 | N/A | 71 | 71 | 71 | 71 | 0 | 72 | 72 | 1 |
| R379 | Residence | B (65) | 1 | N/A | 68 | 68 | 69 | 69 | 1 | 71 | 71 | 3 |
| R380 | Residence | B (65) | 1 | N/A | 70 | 70 | 71 | 71 | 1 | 72 | 72 | 2 |
| R381 | Residence | B (65) | 1 | N/A | 67 | 67 | 68 | 68 | 1 | 70 | 70 | 3 |
| R382 | Residence | B (65) | 1 | N/A | 66 | 66 | 67 | 67 | 1 | 69 | 69 | 3 |
| R383 | Residence | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 67 | 67 | 2 |
| R384 | Residence | B (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 66 | 66 | 3 |
| R385 | Residence | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 66 | 66 | 2 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | $\begin{aligned} & \text { ODOT } \\ & \text { Criteria } \\ & \text { NAAC } \end{aligned}$ | No. of <br> Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing <br> 2017 TNM $+$ <br> StructureBorne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM + StructureBorne Leq dB(A) | Build <br> 2040 <br> Increase over Existing Noise Level dB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R386 | Residence | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 68 | 68 | 3 |
| R387 | Residence | B (65) | 1 | N/A | 59 | 59 | 60 | 60 | 1 | 62 | 62 | 3 |
| R388 | Multi-Family | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 63 | 63 | 2 |
| R389 | Multi-Family | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 64 | 64 | 3 |
| R390 | Multi-Family | B (65) | 1 | N/A | 59 | 59 | 59 | 59 | 0 | 61 | 61 | 2 |
| R391 | Multi-Family | B (65) | 1 | N/A | 58 | 58 | 58 | 58 | 0 | 60 | 60 | 2 |
| R392 | Multi-Family | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 64 | 64 | 3 |
| R393 | Multi-Family | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 64 | 64 | 2 |
| R394 | Multi-Family | B (65) | 1 | N/A | 60 | 60 | 61 | 61 | 1 | 63 | 63 | 3 |
| R395 | Multi-Family | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 65 | 65 | 3 |
| R396 | Multi-Family | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 63 | 63 | 2 |
| R397 | Multi-Family | B (65) | 1 | N/A | 61 | 61 | 61 | 61 | 0 | 63 | 63 | 2 |
| R398 | Multi-Family | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 64 | 64 | 2 |
| R399 | Multi-Family | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 64 | 64 | 2 |
| R400 | Residence | B (65) | 1 | N/A | 58 | 58 | 59 | 59 | 1 | 61 | 61 | 3 |
| R401 | Residence | B (65) | 1 | N/A | 57 | 57 | 58 | 58 | 1 | 60 | 60 | 3 |
| R402 | Residence | B (65) | 1 | N/A | 56 | 56 | 57 | 57 | 1 | 58 | 58 | 2 |
| R403 | Residence | B (65) | 1 | N/A | 57 | 57 | 58 | 58 | 1 | 60 | 60 | 3 |
| R404 | Residence | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 68 | 68 | 3 |
| R405 | Residence | B (65) | 1 | N/A | 72 | 72 | 72 | 72 | 0 | 73 | 73 | 1 |
| R406 | Residence | B (65) | 1 | N/A | 52 | 52 | 53 | 53 | 1 | 53 | 53 | 1 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | $\begin{aligned} & \text { ODOT } \\ & \text { Criteria } \\ & \text { NAAC } \end{aligned}$ |  | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing <br> 2017 TNM <br> + <br> StructureBorne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + <br> StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM + StructureBorne Leq dB(A) | $\begin{gathered} \text { Build } \\ 2040 \\ \text { Increase } \\ \text { over } \\ \text { Existing } \\ \text { Noise } \\ \text { Level } \\ \text { dB } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R407 | Residence | B (65) | 1 | N/A | 52 | 52 | 53 | 53 | 1 | 53 | 53 | 1 |
| R408 | Residence | B (65) | 1 | N/A | 52 | 52 | 53 | 53 | 1 | 53 | 53 | 1 |
| R409 | Residence | B (65) | 1 | N/A | 53 | 53 | 53 | 53 | 0 | 54 | 54 | 1 |
| R410 | Residence | B (65) | 1 | N/A | 54 | 54 | 55 | 55 | 1 | 56 | 56 | 2 |
| R411 | Residence | B (65) | 1 | N/A | 54 | 54 | 55 | 55 | 1 | 55 | 55 | 1 |
| R412 | Residence | B (65) | 1 | N/A | 54 | 54 | 55 | 55 | 1 | 56 | 56 | 2 |
| R413 | Residence | B (65) | 1 | N/A | 55 | 55 | 56 | 56 | 1 | 57 | 57 | 2 |
| R414 | Residence | B (65) | 1 | N/A | 54 | 54 | 54 | 54 | 0 | 57 | 57 | 3 |
| R415 | Residence | B (65) | 1 | N/A | 54 | 54 | 55 | 55 | 1 | 58 | 58 | 4 |
| R416 | Residence | B (65) | 1 | N/A | 57 | 57 | 58 | 58 | 1 | 61 | 61 | 4 |
| R417 | Residence | B (65) | 1 | N/A | 53 | 53 | 54 | 54 | 1 | 56 | 56 | 3 |
| R418 | Residence | B (65) | 1 | N/A | 53 | 53 | 54 | 54 | 1 | 56 | 56 | 3 |
| R419 | Residence | B (65) | 1 | N/A | 53 | 53 | 54 | 54 | 1 | 56 | 56 | 3 |
| R420 | Residence | B (65) | 1 | N/A | 53 | 53 | 54 | 54 | 1 | 56 | 56 | 3 |
| R421 | Residence | B (65) | 1 | N/A | 55 | 55 | 56 | 56 | 1 | 59 | 59 | 4 |
| R422 | Residence | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 64 | 64 | 3 |
| R423 | Residence | B (65) | 1 | N/A | 62 | 62 | 62 | 62 | 0 | 65 | 65 | 3 |
| R424 | Residence | B (65) | 1 | N/A | 59 | 59 | 60 | 60 | 1 | 63 | 63 | 4 |
| R425 | Residence | B (65) | 1 | N/A | 59 | 59 | 60 | 60 | 1 | 63 | 63 | 4 |
| R426 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 65 | 65 | 3 |
| R427 | Residence | B (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 66 | 66 | 3 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | $\begin{aligned} & \text { ODOT } \\ & \text { Criteria } \\ & \text { NAAC } \end{aligned}$ | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing 2017 TNM + StructureBorne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM + StructureBorne Leq dB(A) | Build <br> 2040 <br> Increase over Existing Noise Level dB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R428 | Residence | B (65) | 1 | N/A | 58 | 58 | 59 | 59 | 1 | 62 | 62 | 4 |
| R429 | Residence | B (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 65 | 65 | 2 |
| R430 | Residence | B (65) | 1 | N/A | 56 | 56 | 57 | 57 | 1 | 59 | 59 | 3 |
| R431 | Residence | B (65) | 1 | N/A | 57 | 57 | 58 | 58 | 1 | 60 | 60 | 3 |
| R432 | Residence | B (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 66 | 66 | 3 |
| R433 | Residence | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 64 | 64 | 3 |
| R434 | Residence | B (65) | 1 | N/A | 54 | 54 | 55 | 55 | 1 | 57 | 57 | 3 |
| R435 | Residence | B (65) | 1 | N/A | 53 | 53 | 54 | 54 | 1 | 54 | 54 | 1 |
| R436 | Residence | B (65) | 1 | N/A | 60 | 60 | 61 | 61 | 1 | 62 | 62 | 2 |
| R437 | Residence | B (65) | 1 | N/A | 53 | 53 | 54 | 54 | 1 | 54 | 54 | 1 |
| R438 | Residence | B (65) | 1 | N/A | 53 | 53 | 54 | 54 | 1 | 53 | 53 | 0 |
| R439 | Residence | B (65) | 1 | N/A | 54 | 54 | 54 | 54 | 0 | 53 | 53 | -1 |
| R440 | Residence | B (65) | 1 | N/A | 69 | 69 | 70 | 70 | 1 | 70 | 70 | 1 |
| R441 | Residence | B (65) | 1 | N/A | 59 | 59 | 60 | 60 | 1 | 63 | 63 | 4 |
| R442 | Multi-Family | B (65) | 1 | N/A | 68 | 68 | 69 | 69 | 1 | 69 | 69 | 1 |
| R443 | Multi-Family | B (65) | 1 | N/A | 69 | 69 | 70 | 70 | 1 | 69 | 69 | 0 |
| R444 | Multi-Family | B (65) | 1 | N/A | 69 | 69 | 70 | 70 | 1 | 67 | 67 | -2 |
| R445 | Multi-Family | B (65) | 1 | N/A | 69 | 69 | 70 | 70 | 1 | 66 | 66 | -3 |
| R446 | Multi-Family | B (65) | 1 | N/A | 71 | 71 | 72 | 72 | 1 | 72 | 72 | 1 |
| R447 | Multi-Family | B (65) | 1 | N/A | 72 | 72 | 73 | 73 | 1 | 73 | 73 | 1 |
| R448 | Multi-Family | B (65) | 1 | N/A | 72 | 72 | 73 | 73 | 1 | 73 | 73 | 1 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | ODOT <br> Criteria <br> NAAC | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing <br> 2017 TNM + <br> StructureBorne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + <br> StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM + StructureBorne Leq dB(A) | $\begin{gathered} \text { Build } \\ 2040 \\ \text { Increase } \\ \text { over } \\ \text { Existing } \\ \text { Noise } \\ \text { Level } \\ \text { dB } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R449 | Multi-Family | B (65) | 1 | N/A | 72 | 72 | 73 | 73 | 1 | 73 | 73 | 1 |
| R450 | Multi-Family | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 63 | 63 | 1 |
| R451 | Multi-Family | B (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 64 | 64 | 1 |
| R452 | Multi-Family | B (65) | 1 | N/A | 67 | 67 | 67 | 67 | 0 | 67 | 67 | 0 |
| R453 | Multi-Family | B (65) | 1 | N/A | 69 | 69 | 70 | 70 | 1 | 69 | 69 | 0 |
| R454 | Multi-Family | B (65) | 1 | N/A | 58 | 58 | 59 | 59 | 1 | 60 | 60 | 2 |
| R455 | Multi-Family | B (65) | 1 | N/A | 58 | 58 | 59 | 59 | 1 | 60 | 60 | 2 |
| R456 | Multi-Family | B (65) | 1 | N/A | 58 | 58 | 59 | 59 | 1 | 60 | 60 | 2 |
| R457 | Multi-Family | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 63 | 63 | 2 |
| R458 | Multi-Family | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 63 | 63 | 2 |
| R459 | Multi-Family | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 63 | 63 | 2 |
| R460 | Residence | B (65) | 1 | N/A | 55 | 55 | 56 | 56 | 1 | 56 | 56 | 1 |
| R461 | Residence | B (65) | 1 | N/A | 56 | 56 | 58 | 58 | 2 | 58 | 58 | 2 |
| R462 | Residence | B (65) | 1 | N/A | 55 | 55 | 56 | 56 | 1 | 57 | 57 | 2 |
| R463 | Residence | B (65) | 1 | N/A | 56 | 56 | 57 | 57 | 1 | 57 | 57 | 1 |
| R464 | Residence | B (65) | 1 | N/A | 57 | 57 | 58 | 58 | 1 | 58 | 58 | 1 |
| R465 | Residence | B (65) | 1 | N/A | 57 | 57 | 58 | 58 | 1 | 59 | 59 | 2 |
| R466 | $\qquad$ | C (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 66 | 66 | 1 |
| R467 | Multi-Family | B (65) | 1 | N/A | 67 | 67 | 69 | 69 | 2 | 70 | 70 | 3 |
| R468 | Multi-Family | B (65) | 1 | N/A | 68 | 68 | 70 | 70 | 2 | 71 | 71 | 3 |
| R469 | Multi-Family | B (65) | 1 | N/A | 66 | 66 | 67 | 67 | 1 | 69 | 69 | 3 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | ODOT Criteria NAAC | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing 2017 TNM $+$ StructureBorne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + <br> StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM + StructureBorne Leq dB(A) | Build <br> 2040 <br> Increase over Existing Noise Level dB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R470 | Multi-Family | B (65) | 1 | N/A | 67 | 67 | 68 | 68 | 1 | 70 | 70 | 3 |
| R471 | Multi-Family | B (65) | 1 | N/A | 68 | 68 | 69 | 69 | 1 | 70 | 70 | 2 |
| R472 | Multi-Family | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 68 | 68 | 3 |
| R473 | Multi-Family | B (65) | 1 | N/A | 66 | 66 | 67 | 67 | 1 | 69 | 69 | 3 |
| R474 | Multi-Family | B (65) | 1 | N/A | 67 | 67 | 68 | 68 | 1 | 70 | 70 | 3 |
| R475 | Multi-Family | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 67 | 67 | 3 |
| R476 | Multi-Family | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 68 | 68 | 3 |
| R477 | Multi-Family | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 68 | 68 | 3 |
| R478 | Multi-Family | B (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 66 | 66 | 3 |
| R479 | Multi-Family | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 67 | 67 | 3 |
| R480 | Multi-Family | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 67 | 67 | 3 |
| R481 | Multi-Family | B (65) | 1 | N/A | 62 | 62 | 64 | 64 | 2 | 65 | 65 | 3 |
| R482 | Multi-Family | B (65) | 1 | N/A | 63 | 63 | 65 | 65 | 2 | 66 | 66 | 3 |
| R483 | Multi-Family | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 66 | 66 | 2 |
| R484 | Residence | B (65) | 1 | N/A | 56 | 56 | 57 | 57 | 1 | 61 | 61 | 5 |
| R485 | Residence | B (65) | 1 | N/A | 55 | 55 | 56 | 56 | 1 | 60 | 60 | 5 |
| R486 | Residence | B (65) | 1 | N/A | 54 | 54 | 55 | 55 | 1 | 58 | 58 | 4 |
| R487 | Residence | B (65) | 1 | N/A | 54 | 54 | 55 | 55 | 1 | 58 | 58 | 4 |
| R488 | Residence | B (65) | 1 | N/A | 54 | 54 | 55 | 55 | 1 | 57 | 57 | 3 |
| R489 | Residence | B (65) | 1 | N/A | 72 | 72 | 73 | 73 | 1 | 74 | 74 | 2 |
| R490 | Residence | B (65) | 1 | N/A | 72 | 72 | 73 | 73 | 1 | 74 | 74 | 2 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | ODOT <br> Criteria NAAC | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | $\begin{gathered} \text { Existing } \\ 2017 \text { TNM } \\ + \\ \text { Structure- } \\ \text { Borne } \\ \text { Leq dB(A) } \end{gathered}$ | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + <br> StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM + <br> StructureBorne Leq dB(A) | Build <br> 2040 <br> Increase over Existing Noise Level dB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R491 | Residence | B (65) | 1 | N/A | 69 | 69 | 70 | 70 | 1 | 71 | 71 | 2 |
| R492 | Residence | B (65) | 1 | N/A | 67 | 67 | 68 | 68 | 1 | 69 | 69 | 2 |
| R493 | Residence | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 66 | 66 | 2 |
| R494 | Residence | B (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 65 | 65 | 2 |
| R495 | Residence | B (65) | 1 | N/A | 62 | 62 | 62 | 62 | 0 | 64 | 64 | 2 |
| R496 | Residence | B (65) | 1 | N/A | 68 | 68 | 69 | 69 | 1 | 70 | 70 | 2 |
| R497 | Residence | B (65) | 1 | N/A | 67 | 67 | 68 | 68 | 1 | 69 | 69 | 2 |
| R498 | Residence | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 66 | 66 | 2 |
| R499 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 65 | 65 | 3 |
| R500 | Residence | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 63 | 63 | 2 |
| R501 | Residence | B (65) | 1 | N/A | 70 | 70 | 71 | 71 | 1 | 72 | 72 | 2 |
| R502 | Residence | B (65) | 1 | N/A | 69 | 69 | 70 | 70 | 1 | 71 | 71 | 2 |
| R503 | Residence | B (65) | 1 | N/A | 69 | 69 | 70 | 70 | 1 | 71 | 71 | 2 |
| R504 | Residence | B (65) | 1 | N/A | 70 | 70 | 71 | 71 | 1 | 72 | 72 | 2 |
| R505 | Residence | B (65) | 1 | N/A | 70 | 70 | 70 | 70 | 0 | 72 | 72 | 2 |
| R506 | Residence | B (65) | 1 | N/A | 69 | 69 | 70 | 70 | 1 | 72 | 72 | 3 |
| R507 | Residence | B (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 65 | 65 | 2 |
| R508 | Residence | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 63 | 63 | 2 |
| R509 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 65 | 65 | 3 |
| R510 | Residence | B (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 65 | 65 | 2 |
| R511 | Residence | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 64 | 64 | 2 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | ODOT <br> Criteria <br> NAAC | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing 2017 TNM + StructureBorne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + <br> StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM + StructureBorne Leq dB(A) | Build <br> 2040 <br> Increase over Existing Noise Level dB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R512 | Residence | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 64 | 64 | 3 |
| R513 | Residence | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 63 | 63 | 2 |
| R514 | Residence | B (65) | 1 | N/A | 60 | 60 | 61 | 61 | 1 | 62 | 62 | 2 |
| R515 | Residence | B (65) | 1 | N/A | 58 | 58 | 59 | 59 | 1 | 60 | 60 | 2 |
| R516 | Residence | B (65) | 1 | N/A | 58 | 58 | 59 | 59 | 1 | 60 | 60 | 2 |
| R517 | Residence | B (65) | 1 | N/A | 57 | 57 | 58 | 58 | 1 | 59 | 59 | 2 |
| R518 | Residence | B (65) | 1 | N/A | 60 | 60 | 60 | 60 | 0 | 61 | 61 | 1 |
| R519 | Residence | B (65) | 1 | N/A | 54 | 54 | 55 | 55 | 1 | 56 | 56 | 2 |
| R520 | Residence | B (65) | 1 | N/A | 53 | 53 | 54 | 54 | 1 | 55 | 55 | 2 |
| R521 | Residence | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 67 | 67 | 2 |
| R522 | Residence | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 67 | 67 | 2 |
| R523 | Residence | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 66 | 66 | 2 |
| R524 | Residence | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 66 | 66 | 2 |
| R525 | Residence | B (65) | 1 | N/A | 63 | 63 | 65 | 65 | 2 | 65 | 65 | 2 |
| R526 | Residence | B (65) | 1 | N/A | 59 | 59 | 60 | 60 | 1 | 61 | 61 | 2 |
| R527 | Multi-Family | B (65) | 1 | N/A | 69 | 69 | 70 | 70 | 1 | 72 | 72 | 3 |
| R528 | Multi-Family | B (65) | 1 | N/A | 68 | 68 | 69 | 69 | 1 | 71 | 71 | 3 |
| R529 | Multi-Family | B (65) | 1 | N/A | 67 | 67 | 68 | 68 | 1 | 69 | 69 | 2 |
| R530 | Multi-Family | B (65) | 1 | N/A | 70 | 70 | 70 | 70 | 0 | 73 | 73 | 3 |
| R531 | Multi-Family | B (65) | 1 | N/A | 69 | 69 | 70 | 70 | 1 | 71 | 71 | 2 |
| R532 | Multi-Family | B (65) | 1 | N/A | 68 | 68 | 68 | 68 | 0 | 70 | 70 | 2 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | $\begin{aligned} & \text { ODOT } \\ & \text { Criteria } \\ & \text { NAAC } \end{aligned}$ | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing <br> 2017 TNM <br> + <br> StructureBorne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + <br> StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM + StructureBorne Leq dB(A) | $\begin{gathered} \text { Build } \\ 2040 \\ \text { Increase } \\ \text { over } \\ \text { Existing } \\ \text { Noise } \\ \text { Level } \\ \text { dB } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R533 | Multi-Family | B (65) | 1 | N/A | 54 | 54 | 57 | 57 | 3 | 56 | 56 | 2 |
| R534 | Multi-Family | B (65) | 1 | N/A | 60 | 60 | 61 | 61 | 1 | 62 | 62 | 2 |
| R535 | Multi-Family | B (65) | 1 | N/A | 53 | 53 | 56 | 56 | 3 | 55 | 55 | 2 |
| R536 | Residence | B (65) | 1 | N/A | 62 | 62 | 64 | 64 | 2 | 64 | 64 | 2 |
| R537 | Residence | B (65) | 1 | 54 | 63 | 64 | 63 | 63 | -1 | 64 | 64 | 0 |
| R538 | Residence | B (65) | 1 | 53 | 61 | 62 | 66 | 66 | 4 | 62 | 62 | 0 |
| R539 | Residence | B (65) | 1 | 52 | 59 | 60 | 61 | 62 | 2 | 60 | 61 | 1 |
| R540 | Residence | B (65) | 1 | 52 | 59 | 60 | 60 | 61 | 1 | 60 | 61 | 1 |
| R541 | Residence | B (65) | 1 | 53 | 59 | 60 | 60 | 61 | 1 | 60 | 61 | 1 |
| R542 | Residence | B (65) | 1 | 53 | 59 | 60 | 60 | 61 | 1 | 60 | 61 | 1 |
| R543 | Residence | B (65) | 1 | 53 | 59 | 60 | 60 | 61 | 1 | 60 | 61 | 1 |
| R544 | Residence | B (65) | 1 | 53 | 59 | 60 | 59 | 60 | 0 | 60 | 61 | 1 |
| R545 | Residence | B (65) | 1 | 53 | 59 | 60 | 60 | 61 | 1 | 61 | 62 | 2 |
| R546 | Residence | B (65) | 1 | 53 | 61 | 62 | 62 | 62 | 0 | 63 | 63 | 1 |
| R547 | Residence | B (65) | 1 | 53 | 60 | 61 | 61 | 62 | 1 | 62 | 63 | 2 |
| R548 | Residence | B (65) | 1 | 54 | 61 | 62 | 61 | 62 | 0 | 62 | 63 | 1 |
| R549 | Residence | B (65) | 1 | 54 | 61 | 61 | 61 | 62 | 1 | 62 | 63 | 2 |
| R550 | Residence | B (65) | 1 | 55 | 60 | 61 | 61 | 62 | 1 | 62 | 63 | 2 |
| R551 | Residence | B (65) | 1 | 56 | 61 | 62 | 62 | 63 | 1 | 63 | 64 | 2 |
| R552 | Residence | B (65) | 1 | 56 | 62 | 63 | 63 | 64 | 1 | 64 | 65 | 2 |
| R553 | Residence | B (65) | 1 | 57 | 63 | 64 | 64 | 65 | 1 | 65 | 66 | 2 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | $\begin{aligned} & \text { ODOT } \\ & \text { Criteria } \\ & \text { NAAC } \end{aligned}$ | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing 2017 TNM + StructureBorne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + <br> StructureBorne Leq dB(A) | No <br> Build <br> 2040 <br> Increase <br> over <br> Existing <br> Noise <br> Level <br> dB | Build Alternative Leq dB(A) | Build 2040 TNM + StructureBorne Leq dB(A) | $\begin{gathered} \text { Build } \\ 2040 \\ \text { Increase } \\ \text { over } \\ \text { Existing } \\ \text { Noise } \\ \text { Level } \\ \text { dB } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R554 | Residence | B (65) | 1 | 58 | 60 | 62 | 61 | 63 | 1 | 62 | 63 | 1 |
| R555 | Residence | B (65) | 1 | 60 | 58 | 62 | 59 | 63 | 1 | 58 | 62 | 0 |
| R556 | Residence | B (65) | 1 | 59 | 62 | 64 | 62 | 64 | 0 | 62 | 64 | 0 |
| R557 | Residence | B (65) | 1 | 57 | 64 | 65 | 64 | 65 | 0 | 64 | 65 | 0 |
| R558 | Residence | B (65) | 1 | 58 | 59 | 62 | 60 | 62 | 0 | 59 | 62 | 0 |
| R559 | Residence | B (65) | 1 | 59 | 59 | 62 | 59 | 62 | 0 | 59 | 62 | 0 |
| R560 | Residence | B (65) | 1 | 61 | 61 | 64 | 61 | 64 | 0 | 60 | 63 | -1 |
| R561 | Residence | B (65) | 1 | 59 | 63 | 64 | 62 | 64 | 0 | 62 | 64 | 0 |
| R562 | Residence | B (65) | 1 | 57 | 64 | 65 | 64 | 65 | 0 | 64 | 65 | 0 |
| R563 | Residence | B (65) | 1 | 56 | 64 | 65 | 64 | 65 | 0 | 64 | 65 | 0 |
| R564 | Residence | B (65) | 1 | 55 | 64 | 64 | 64 | 65 | 1 | 64 | 65 | 1 |
| R565 | Residence | B (65) | 1 | 55 | 63 | 63 | 63 | 64 | 1 | 62 | 63 | 0 |
| R566 | Residence | B (65) | 1 | 55 | 63 | 63 | 63 | 64 | 1 | 62 | 63 | 0 |
| R567 | Residence | B (65) | 1 | 55 | 62 | 63 | 62 | 63 | 0 | 62 | 63 | 0 |
| R568 | Residence | B (65) | 1 | 55 | 62 | 62 | 62 | 63 | 1 | 62 | 63 | 1 |
| R569 | Residence | B (65) | 1 | 54 | 63 | 63 | 63 | 63 | 0 | 64 | 64 | 1 |
| R570 | Residence | B (65) | 1 | 53 | 62 | 63 | 63 | 63 | 0 | 63 | 63 | 0 |
| R571 | Residence | B (65) | 1 | 55 | 64 | 64 | 64 | 65 | 1 | 65 | 65 | 1 |
| R572 | Residence | B (65) | 1 | 55 | 63 | 64 | 64 | 64 | 0 | 64 | 64 | 0 |
| R573 | Best Western (Pool) | E (70) | 1 | 54 | 60 | 61 | 61 | 62 | 1 | 61 | 62 | 1 |
| R574 | $\begin{gathered} \text { Best Western (Outdoor } \\ \text { Seating) } \\ \hline \end{gathered}$ | E (70) | 1 | 54 | 59 | 60 | 60 | 61 | 1 | 61 | 62 | 2 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | $\begin{aligned} & \text { ODOT } \\ & \text { Criteria } \\ & \text { NAAC } \end{aligned}$ | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing 2017 TNM + StructureBorne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + StructureBorne Leq dB(A) | No <br> Build <br> 2040 <br> Increase <br> over <br> Existing <br> Noise <br> Level <br> dB | Build Alternative Leq dB(A) | Build 2040 TNM + StructureBorne Leq dB(A) | Build 2040 <br> Increase over Existing Noise Level dB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R575 | Best Western | E (70) | 1 | 58 | 65 | 66 | 65 | 66 | 0 | 66 | 67 | 1 |
| R693 | Residence | B (65) | 1 | N/A | 65 | 65 | 65 | 65 | 0 | 66 | 66 | 1 |
| R694 | Residence | B (65) | 1 | N/A | 66 | 66 | 66 | 66 | 0 | 67 | 67 | 1 |
| R695 | Residence | B (65) | 1 | N/A | 72 | 72 | 72 | 72 | 0 | 73 | 73 | 1 |
| R696 | Residence | B (65) | 1 | N/A | 68 | 68 | 69 | 69 | 1 | 69 | 69 | 1 |
| R697 | Residence | B (65) | 1 | N/A | 67 | 67 | 68 | 68 | 1 | 68 | 68 | 1 |
| R698 | Residence | B (65) | 1 | N/A | 66 | 66 | 66 | 66 | 0 | 67 | 67 | 1 |
| R699 | Residence | B (65) | 1 | N/A | 74 | 74 | 74 | 74 | 0 | 75 | 75 | 1 |
| R700 | Jon Storm Park | C (65) | 1 | 66 | 66 | 69 | 65 | 68 | -1 | 64 | 68 | -1 |
| R701 | Jon Storm Park | C (65) | 1 | 64 | 67 | 68 | 66 | 68 | 0 | 67 | 69 | 1 |
| R702 | Jon Storm Park | C (65) | 1 | 63 | 67 | 68 | 66 | 68 | 0 | 68 | 69 | 1 |
| R703 | Jon Storm Park | C (65) | 1 | 62 | 66 | 67 | 66 | 67 | 0 | 68 | 69 | 2 |
| R704 | Multi-Family | B (65) | 1 | N/A | 67 | 67 | 68 | 68 | 1 | 69 | 69 | 2 |
| R705 | Multi-Family | B (65) | 1 | N/A | 67 | 67 | 68 | 68 | 1 | 69 | 69 | 2 |
| R706 | Multi-Family | B (65) | 1 | N/A | 68 | 68 | 69 | 69 | 1 | 70 | 70 | 2 |
| R707 | Multi-Family | B (65) | 1 | N/A | 68 | 68 | 69 | 69 | 1 | 70 | 70 | 2 |
| R708 | Multi-Family | B (65) | 1 | N/A | 57 | 57 | 58 | 58 | 1 | 58 | 58 | 1 |
| R709 | Multi-Family | B (65) | 1 | N/A | 54 | 54 | 55 | 55 | 1 | 56 | 56 | 2 |
| R710 | Multi-Family | B (65) | 1 | N/A | 67 | 67 | 67 | 67 | 0 | 68 | 68 | 1 |
| R711 | Multi-Family | B (65) | 1 | N/A | 66 | 66 | 66 | 66 | 0 | 67 | 67 | 1 |
| R712 | Multi-Family | B (65) | 1 | N/A | 48 | 48 | 49 | 49 | 1 | 49 | 49 | 1 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | $\begin{aligned} & \text { ODOT } \\ & \text { Criteria } \\ & \text { NAAC } \end{aligned}$ | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing 2017 TNM $+$ StructureBorne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + <br> StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM + StructureBorne Leq dB(A) | $\begin{gathered} \text { Build } \\ 2040 \\ \text { Increase } \\ \text { over } \\ \text { Existing } \\ \text { Noise } \\ \text { Level } \\ \text { dB } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R713 | Multi-Family | B (65) | 1 | N/A | 51 | 51 | 52 | 52 | 1 | 53 | 53 | 2 |
| R714 | Multi-Family | B (65) | 1 | N/A | 55 | 55 | 56 | 56 | 1 | 56 | 56 | 1 |
| R715 | Multi-Family | B (65) | 1 | N/A | 56 | 56 | 56 | 56 | 0 | 57 | 57 | 1 |
| R716 | Multi-Family | B (65) | 1 | N/A | 43 | 43 | 45 | 45 | 2 | 45 | 45 | 2 |
| R717 | Multi-Family | B (65) | 1 | N/A | 43 | 43 | 45 | 45 | 2 | 45 | 45 | 2 |
| R718 | Multi-Family | B (65) | 1 | N/A | 44 | 44 | 45 | 45 | 1 | 46 | 46 | 2 |
| R719 | Multi-Family | B (65) | 1 | N/A | 45 | 45 | 46 | 46 | 1 | 46 | 46 | 1 |
| R720 | Multi-Family | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 63 | 63 | 2 |
| R721 | Multi-Family | B (65) | 1 | N/A | 60 | 60 | 61 | 61 | 1 | 61 | 61 | 1 |
| R722 | Multi-Family | B (65) | 1 | N/A | 58 | 58 | 59 | 59 | 1 | 59 | 59 | 1 |
| R723 | Multi-Family | B (65) | 1 | N/A | 57 | 57 | 58 | 58 | 1 | 59 | 59 | 2 |
| R724 | Multi-Family | B (65) | 1 | N/A | 50 | 50 | 51 | 51 | 1 | 52 | 52 | 2 |
| R725 | Multi-Family | B (65) | 1 | N/A | 49 | 49 | 51 | 51 | 2 | 52 | 52 | 3 |
| R726 | Multi-Family | B (65) | 1 | N/A | 49 | 49 | 50 | 50 | 1 | 51 | 51 | 2 |
| R727 | Multi-Family | B (65) | 1 | N/A | 46 | 46 | 47 | 47 | 1 | 48 | 48 | 2 |
| R728 | Multi-Family | B (65) | 1 | N/A | 45 | 45 | 46 | 46 | 1 | 47 | 47 | 2 |
| R729 | Multi-Family | B (65) | 1 | N/A | 45 | 45 | 46 | 46 | 1 | 46 | 46 | 1 |
| R730 | Multi-Family | B (65) | 1 | N/A | 51 | 51 | 51 | 51 | 0 | 53 | 53 | 2 |
| R731 | Multi-Family | B (65) | 1 | N/A | 52 | 52 | 52 | 52 | 0 | 54 | 54 | 2 |
| R732 | Multi-Family | B (65) | 1 | N/A | 52 | 52 | 52 | 52 | 0 | 53 | 53 | 1 |
| R733 | Multi-Family | B (65) | 1 | N/A | 52 | 52 | 52 | 52 | 0 | 53 | 53 | 1 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | $\begin{aligned} & \text { ODOT } \\ & \text { Criteria } \\ & \text { NAAC } \end{aligned}$ | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing <br> 2017 TNM <br> + <br> StructureBorne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + <br> StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM + StructureBorne Leq dB(A) | $\begin{gathered} \text { Build } \\ 2040 \\ \text { Increase } \\ \text { over } \\ \text { Existing } \\ \text { Noise } \\ \text { Level } \\ \text { dB } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R734 | Multi-Family | B (65) | 1 | N/A | 44 | 44 | 45 | 45 | 1 | 46 | 46 | 2 |
| R735 | Multi-Family | B (65) | 1 | N/A | 44 | 44 | 45 | 45 | 1 | 46 | 46 | 2 |
| R736 | Multi-Family | B (65) | 1 | N/A | 56 | 56 | 57 | 57 | 1 | 57 | 57 | 1 |
| R737 | Multi-Family | B (65) | 1 | N/A | 56 | 56 | 57 | 57 | 1 | 57 | 57 | 1 |
| R738 | Multi-Family | B (65) | 1 | N/A | 54 | 54 | 55 | 55 | 1 | 56 | 56 | 2 |
| R739 | Multi-Family | B (65) | 1 | N/A | 54 | 54 | 55 | 55 | 1 | 56 | 56 | 2 |
| R740 | Multi-Family | B (65) | 1 | N/A | 59 | 59 | 60 | 60 | 1 | 60 | 60 | 1 |
| R741 | Multi-Family | B (65) | 1 | N/A | 54 | 54 | 55 | 55 | 1 | 56 | 56 | 2 |
| R742 | Multi-Family | B (65) | 1 | N/A | 52 | 52 | 53 | 53 | 1 | 53 | 53 | 1 |
| R743 | Multi-Family | B (65) | 1 | N/A | 51 | 51 | 53 | 53 | 2 | 53 | 53 | 2 |
| R744 | Multi-Family | B (65) | 1 | N/A | 51 | 51 | 52 | 52 | 1 | 53 | 53 | 2 |
| R745 | Multi-Family | B (65) | 1 | N/A | 51 | 51 | 52 | 52 | 1 | 53 | 53 | 2 |
| R746 | Pool at Apts. | C (65) | 1 | N/A | 51 | 51 | 52 | 52 | 1 | 53 | 53 | 2 |
| R747 | Multi-Family | B (65) | 1 | N/A | 51 | 51 | 52 | 52 | 1 | 53 | 53 | 2 |
| R748 | Multi-Family | B (65) | 1 | N/A | 53 | 53 | 54 | 54 | 1 | 55 | 55 | 2 |
| R749 | Multi-Family | B (65) | 1 | N/A | 69 | 69 | 70 | 70 | 1 | 71 | 71 | 2 |
| R750 | Multi-Family | B (65) | 1 | N/A | 69 | 69 | 70 | 70 | 1 | 71 | 71 | 2 |
| R751 | Multi-Family | B (65) | 1 | N/A | 70 | 70 | 70 | 70 | 0 | 71 | 71 | 1 |
| R752 | Multi-Family | B (65) | 1 | N/A | 70 | 70 | 71 | 71 | 1 | 71 | 71 | 1 |
| R753 | Multi-Family | B (65) | 1 | N/A | 58 | 58 | 59 | 59 | 1 | 60 | 60 | 2 |
| R754 | Multi-Family | B (65) | 1 | N/A | 54 | 54 | 55 | 55 | 1 | 56 | 56 | 2 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | $\begin{aligned} & \text { ODOT } \\ & \text { Criteria } \\ & \text { NAAC } \end{aligned}$ | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing 2017 TNM + StructureBorne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM + StructureBorne Leq dB(A) | Build <br> 2040 <br> Increase over Existing Noise Level dB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R755 | Multi-Family | B (65) | 1 | N/A | 68 | 68 | 68 | 68 | 0 | 69 | 69 | 1 |
| R756 | Multi-Family | B (65) | 1 | N/A | 66 | 66 | 67 | 67 | 1 | 68 | 68 | 2 |
| R757 | Multi-Family | B (65) | 1 | N/A | 48 | 48 | 48 | 48 | 0 | 49 | 49 | 1 |
| R758 | Multi-Family | B (65) | 1 | N/A | 51 | 51 | 52 | 52 | 1 | 53 | 53 | 2 |
| R759 | Multi-Family | B (65) | 1 | N/A | 56 | 56 | 56 | 56 | 0 | 57 | 57 | 1 |
| R760 | Multi-Family | B (65) | 1 | N/A | 57 | 57 | 58 | 58 | 1 | 58 | 58 | 1 |
| R761 | Multi-Family | B (65) | 1 | N/A | 45 | 45 | 46 | 46 | 1 | 46 | 46 | 1 |
| R762 | Multi-Family | B (65) | 1 | N/A | 45 | 45 | 46 | 46 | 1 | 46 | 46 | 1 |
| R763 | Multi-Family | B (65) | 1 | N/A | 46 | 46 | 47 | 47 | 1 | 47 | 47 | 1 |
| R764 | Multi-Family | B (65) | 1 | N/A | 46 | 46 | 47 | 47 | 1 | 47 | 47 | 1 |
| R765 | Multi-Family | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 64 | 64 | 2 |
| R766 | Multi-Family | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 63 | 63 | 2 |
| R767 | Multi-Family | B (65) | 1 | N/A | 59 | 59 | 60 | 60 | 1 | 60 | 60 | 1 |
| R768 | Multi-Family | B (65) | 1 | N/A | 58 | 58 | 59 | 59 | 1 | 60 | 60 | 2 |
| R769 | Multi-Family | B (65) | 1 | N/A | 50 | 50 | 51 | 51 | 1 | 53 | 53 | 3 |
| R770 | Multi-Family | B (65) | 1 | N/A | 50 | 50 | 51 | 51 | 1 | 52 | 52 | 2 |
| R771 | Multi-Family | B (65) | 1 | N/A | 50 | 50 | 51 | 51 | 1 | 52 | 52 | 2 |
| R772 | Multi-Family | B (65) | 1 | N/A | 47 | 47 | 48 | 48 | 1 | 49 | 49 | 2 |
| R773 | Multi-Family | B (65) | 1 | N/A | 46 | 46 | 47 | 47 | 1 | 48 | 48 | 2 |
| R774 | Multi-Family | B (65) | 1 | N/A | 46 | 46 | 47 | 47 | 1 | 48 | 48 | 2 |
| R775 | Multi-Family | B (65) | 1 | N/A | 56 | 56 | 56 | 56 | 0 | 57 | 57 | 1 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | ODOT Criteria NAAC | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing <br> 2017 TNM $+$ StructureBorne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM + StructureBorne Leq dB(A) | Build <br> 2040 <br> Increase over Existing Noise Level dB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R776 | Multi-Family | B (65) | 1 | N/A | 55 | 55 | 56 | 56 | 1 | 56 | 56 | 1 |
| R777 | Multi-Family | B (65) | 1 | N/A | 54 | 54 | 54 | 54 | 0 | 55 | 55 | 1 |
| R778 | Multi-Family | B (65) | 1 | N/A | 54 | 54 | 54 | 54 | 0 | 55 | 55 | 1 |
| R779 | Multi-Family | B (65) | 1 | N/A | 45 | 45 | 46 | 46 | 1 | 47 | 47 | 2 |
| R780 | Multi-Family | B (65) | 1 | N/A | 45 | 45 | 46 | 46 | 1 | 47 | 47 | 2 |
| R781 | Multi-Family | B (65) | 1 | N/A | 57 | 57 | 58 | 58 | 1 | 59 | 59 | 2 |
| R782 | Multi-Family | B (65) | 1 | N/A | 57 | 57 | 58 | 58 | 1 | 59 | 59 | 2 |
| R783 | Multi-Family | B (65) | 1 | N/A | 56 | 56 | 57 | 57 | 1 | 58 | 58 | 2 |
| R784 | Multi-Family | B (65) | 1 | N/A | 56 | 56 | 57 | 57 | 1 | 57 | 57 | 1 |
| R785 | Multi-Family | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 62 | 62 | 1 |
| R786 | Multi-Family | B (65) | 1 | N/A | 60 | 60 | 61 | 61 | 1 | 61 | 61 | 1 |
| R787 | Multi-Family | B (65) | 1 | N/A | 54 | 54 | 56 | 56 | 2 | 56 | 56 | 2 |
| R788 | Multi-Family | B (65) | 1 | N/A | 54 | 54 | 55 | 55 | 1 | 56 | 56 | 2 |
| R789 | Multi-Family | B (65) | 1 | N/A | 54 | 54 | 55 | 55 | 1 | 56 | 56 | 2 |
| R790 | Multi-Family | B (65) | 1 | N/A | 54 | 54 | 55 | 55 | 1 | 56 | 56 | 2 |
| R791 | Multi-Family | B (65) | 1 | N/A | 54 | 54 | 55 | 55 | 1 | 56 | 56 | 2 |
| R792 | Multi-Family | B (65) | 1 | N/A | 54 | 54 | 55 | 55 | 1 | 56 | 56 | 2 |
| R793 | Multi-Family | B (65) | 1 | N/A | 70 | 70 | 71 | 71 | 1 | 72 | 72 | 2 |
| R794 | Multi-Family | B (65) | 1 | N/A | 70 | 70 | 71 | 71 | 1 | 72 | 72 | 2 |
| R795 | Multi-Family | B (65) | 1 | N/A | 71 | 71 | 71 | 71 | 0 | 72 | 72 | 1 |
| R796 | Multi-Family | B (65) | 1 | N/A | 71 | 71 | 72 | 72 | 1 | 72 | 72 | 1 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | $\begin{aligned} & \text { ODOT } \\ & \text { Criteria } \\ & \text { NAAC } \end{aligned}$ | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing 2017 TNM $+$ StructureBorne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + <br> StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM + StructureBorne Leq dB(A) | Build <br> 2040 <br> Increase over Existing Noise Level dB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R797 | Multi-Family | B (65) | 1 | N/A | 59 | 59 | 60 | 60 | 1 | 61 | 61 | 2 |
| R798 | Multi-Family | B (65) | 1 | N/A | 55 | 55 | 56 | 56 | 1 | 57 | 57 | 2 |
| R799 | Multi-Family | B (65) | 1 | N/A | 68 | 68 | 69 | 69 | 1 | 70 | 70 | 2 |
| R800 | Multi-Family | B (65) | 1 | N/A | 67 | 67 | 68 | 68 | 1 | 69 | 69 | 2 |
| R801 | Multi-Family | B (65) | 1 | N/A | 51 | 51 | 52 | 52 | 1 | 53 | 53 | 2 |
| R802 | Multi-Family | B (65) | 1 | N/A | 53 | 53 | 54 | 54 | 1 | 55 | 55 | 2 |
| R803 | Multi-Family | B (65) | 1 | N/A | 57 | 57 | 57 | 57 | 0 | 58 | 58 | 1 |
| R804 | Multi-Family | B (65) | 1 | N/A | 58 | 58 | 59 | 59 | 1 | 59 | 59 | 1 |
| R805 | Multi-Family | B (65) | 1 | N/A | 47 | 47 | 48 | 48 | 1 | 49 | 49 | 2 |
| R806 | Multi-Family | B (65) | 1 | N/A | 48 | 48 | 49 | 49 | 1 | 50 | 50 | 2 |
| R807 | Multi-Family | B (65) | 1 | N/A | 49 | 49 | 50 | 50 | 1 | 51 | 51 | 2 |
| R808 | Multi-Family | B (65) | 1 | N/A | 50 | 50 | 50 | 50 | 0 | 51 | 51 | 1 |
| R809 | Multi-Family | B (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 65 | 65 | 2 |
| R810 | Multi-Family | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 64 | 64 | 2 |
| R811 | Multi-Family | B (65) | 1 | N/A | 60 | 60 | 61 | 61 | 1 | 61 | 61 | 1 |
| R812 | Multi-Family | B (65) | 1 | N/A | 59 | 59 | 60 | 60 | 1 | 61 | 61 | 2 |
| R813 | Multi-Family | B (65) | 1 | N/A | 52 | 52 | 53 | 53 | 1 | 55 | 55 | 3 |
| R814 | Multi-Family | B (65) | 1 | N/A | 52 | 52 | 53 | 53 | 1 | 54 | 54 | 2 |
| R815 | Multi-Family | B (65) | 1 | N/A | 53 | 53 | 53 | 53 | 0 | 54 | 54 | 1 |
| R816 | Multi-Family | B (65) | 1 | N/A | 51 | 51 | 51 | 51 | 0 | 52 | 52 | 1 |
| R817 | Multi-Family | B (65) | 1 | N/A | 50 | 50 | 51 | 51 | 1 | 52 | 52 | 2 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | $\begin{aligned} & \text { ODOT } \\ & \text { Criteria } \\ & \text { NAAC } \end{aligned}$ | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing 2017 TNM $+$ StructureBorne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + <br> StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM + StructureBorne Leq dB(A) | $\begin{gathered} \text { Build } \\ 2040 \\ \text { Increase } \\ \text { over } \\ \text { Existing } \\ \text { Noise } \\ \text { Level } \\ \text { dB } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R818 | Multi-Family | B (65) | 1 | N/A | 50 | 50 | 50 | 50 | 0 | 51 | 51 | 1 |
| R819 | Multi-Family | B (65) | 1 | N/A | 57 | 57 | 58 | 58 | 1 | 59 | 59 | 2 |
| R820 | Multi-Family | B (65) | 1 | N/A | 57 | 57 | 57 | 57 | 0 | 58 | 58 | 1 |
| R821 | Multi-Family | B (65) | 1 | N/A | 56 | 56 | 57 | 57 | 1 | 58 | 58 | 2 |
| R822 | Multi-Family | B (65) | 1 | N/A | 56 | 56 | 57 | 57 | 1 | 58 | 58 | 2 |
| R823 | Multi-Family | B (65) | 1 | N/A | 49 | 49 | 50 | 50 | 1 | 50 | 50 | 1 |
| R824 | Multi-Family | B (65) | 1 | N/A | 48 | 48 | 49 | 49 | 1 | 50 | 50 | 2 |
| R825 | Multi-Family | B (65) | 1 | N/A | 59 | 59 | 60 | 60 | 1 | 61 | 61 | 2 |
| R826 | Multi-Family | B (65) | 1 | N/A | 60 | 60 | 60 | 60 | 0 | 61 | 61 | 1 |
| R827 | Multi-Family | B (65) | 1 | N/A | 57 | 57 | 58 | 58 | 1 | 59 | 59 | 2 |
| R828 | Multi-Family | B (65) | 1 | N/A | 56 | 56 | 57 | 57 | 1 | 58 | 58 | 2 |
| R829 | Multi-Family | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 63 | 63 | 1 |
| R830 | Multi-Family | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 62 | 62 | 1 |
| R831 | Multi-Family | B (65) | 1 | N/A | 59 | 59 | 60 | 60 | 1 | 61 | 61 | 2 |
| R832 | Multi-Family | B (65) | 1 | N/A | 58 | 58 | 59 | 59 | 1 | 60 | 60 | 2 |
| R833 | Multi-Family | B (65) | 1 | N/A | 58 | 58 | 59 | 59 | 1 | 60 | 60 | 2 |
| R834 | Multi-Family | B (65) | 1 | N/A | 58 | 58 | 59 | 59 | 1 | 60 | 60 | 2 |
| R835 | Multi-Family | B (65) | 1 | N/A | 58 | 58 | 59 | 59 | 1 | 60 | 60 | 2 |
| R836 | Multi-Family | B (65) | 1 | N/A | 59 | 59 | 60 | 60 | 1 | 60 | 60 | 1 |
| R837 | Multi-Family | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 63 | 63 | 2 |
| R838 | Multi-Family | B (65) | 1 | N/A | 68 | 68 | 69 | 69 | 1 | 69 | 69 | 1 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | $\begin{aligned} & \text { ODOT } \\ & \text { Criteria } \\ & \text { NAAC } \end{aligned}$ | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing 2017 TNM $+$ StructureBorne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + <br> StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM + StructureBorne Leq dB(A) | Build <br> 2040 <br> Increase over Existing Noise Level dB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R839 | Multi-Family | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 66 | 66 | 2 |
| R840 | Multi-Family | B (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 65 | 65 | 2 |
| R841 | Multi-Family | B (65) | 1 | N/A | 62 | 62 | 62 | 62 | 0 | 64 | 64 | 2 |
| R842 | Multi-Family | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 63 | 63 | 2 |
| R843 | Multi-Family | B (65) | 1 | N/A | 66 | 66 | 66 | 66 | 0 | 67 | 67 | 1 |
| R844 | Multi-Family | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 67 | 67 | 2 |
| R845 | Multi-Family | B (65) | 1 | N/A | 63 | 63 | 64 | 64 | 1 | 65 | 65 | 2 |
| R846 | Multi-Family | B (65) | 1 | N/A | 63 | 63 | 63 | 63 | 0 | 64 | 64 | 1 |
| R847 | Multi-Family | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 67 | 67 | 2 |
| R848 | Multi-Family | B (65) | 1 | N/A | 64 | 64 | 65 | 65 | 1 | 66 | 66 | 2 |
| R849 | Multi-Family | B (65) | 1 | N/A | 63 | 63 | 63 | 63 | 0 | 64 | 64 | 1 |
| R850 | Multi-Family | B (65) | 1 | N/A | 62 | 62 | 63 | 63 | 1 | 64 | 64 | 2 |
| R851 | Multi-Family | B (65) | 1 | N/A | 60 | 60 | 61 | 61 | 1 | 62 | 62 | 2 |
| R852 | Multi-Family | B (65) | 1 | N/A | 60 | 60 | 60 | 60 | 0 | 61 | 61 | 1 |
| R853 | Multi-Family | B (65) | 1 | N/A | 57 | 57 | 58 | 58 | 1 | 59 | 59 | 2 |
| R854 | Multi-Family | B (65) | 1 | N/A | 57 | 57 | 57 | 57 | 0 | 59 | 59 | 2 |
| R855 | Multi-Family | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 63 | 63 | 2 |
| R856 | Multi-Family | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 63 | 63 | 2 |
| R857 | Multi-Family | B (65) | 1 | N/A | 59 | 59 | 60 | 60 | 1 | 61 | 61 | 2 |
| R858 | Multi-Family | B (65) | 1 | N/A | 59 | 59 | 59 | 59 | 0 | 61 | 61 | 2 |
| R859 | Multi-Family | B (65) | 1 | N/A | 61 | 61 | 62 | 62 | 1 | 63 | 63 | 2 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | ODOT Criteria NAAC |  | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing 2017 TNM + <br> StructureBorne <br> Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + <br> StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM + <br> StructureBorne Leq dB(A) | Build <br> 2040 <br> Increase over Existing Noise Level dB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R860 | Multi-Family | B (65) | 1 | N/A | 61 | 61 | 61 | 61 | 0 | 62 | 62 | 1 |
| R861 | Multi-Family | B (65) | 1 | N/A | 59 | 59 | 59 | 59 | 0 | 60 | 60 | 1 |
| R862 | Multi-Family | B (65) | 1 | N/A | 58 | 58 | 59 | 59 | 1 | 60 | 60 | 2 |
| R863 | Multi-Family | B (65) | 1 | N/A | 67 | 67 | 67 | 67 | 0 | 68 | 68 | 1 |
| R864 | Multi-Family | B (65) | 1 | N/A | 66 | 66 | 67 | 67 | 1 | 68 | 68 | 2 |
| R865 | Multi-Family | B (65) | 1 | N/A | 66 | 66 | 66 | 66 | 0 | 67 | 67 | 1 |
| R866 | Multi-Family | B (65) | 1 | N/A | 65 | 65 | 66 | 66 | 1 | 67 | 67 | 2 |
| R867 | Multi-Family | B (65) | 1 | N/A | 66 | 66 | 66 | 66 | 0 | 67 | 67 | 1 |
| R868 | Multi-Family | B (65) | 1 | N/A | 66 | 66 | 66 | 66 | 0 | 67 | 67 | 1 |
| R869 | Multi-Family | B (65) | 1 | N/A | 65 | 65 | 65 | 65 | 0 | 66 | 66 | 1 |
| R870 | Multi-Family | B (65) | 1 | N/A | 65 | 65 | 65 | 65 | 0 | 66 | 66 | 1 |
| R871 | Multi-Family | B (65) | 1 | N/A | 69 | 69 | 70 | 70 | 1 | 71 | 71 | 2 |
| R872 | Multi-Family | B (65) | 1 | N/A | 69 | 69 | 70 | 70 | 1 | 70 | 70 | 1 |
| R873 | Multi-Family | B (65) | 1 | N/A | 68 | 68 | 69 | 69 | 1 | 70 | 70 | 2 |
| R874 | Multi-Family | B (65) | 1 | N/A | 68 | 68 | 68 | 68 | 0 | 69 | 69 | 1 |
| R875 | Multi-Family | B (65) | 1 | N/A | 69 | 69 | 69 | 69 | 0 | 70 | 70 | 1 |
| R876 | Multi-Family | B (65) | 1 | N/A | 69 | 69 | 69 | 69 | 0 | 70 | 70 | 1 |
| R877 | Multi-Family | B (65) | 1 | N/A | 68 | 68 | 68 | 68 | 0 | 69 | 69 | 1 |
| R878 | Multi-Family | B (65) | 1 | N/A | 67 | 67 | 68 | 68 | 1 | 69 | 69 | 2 |
| R879(6b) | Residence | B (65) | 1 | N/A | 58 | 58 | 57 | 57 | -1 | 58 | 58 | 0 |
| R880(6b) | Residence | B (65) | 1 | N/A | 58 | 58 | 57 | 57 | -1 | 58 | 58 | 0 |

Table 9. Predicted Noise Levels

| Receptor ID | Land Use | $\begin{aligned} & \text { ODOT } \\ & \text { Criteria } \\ & \text { NAAC } \end{aligned}$ | No. of Uses | StructureBorne Leq dB(A) | $\begin{aligned} & \text { Existing } \\ & 2017 \\ & \text { Leq } \\ & \text { TNM } \\ & \text { dB(A) } \end{aligned}$ | Existing 2017 TNM + StructureBorne Leq dB(A) | No Build 2040 <br> Alternative <br> Leq dB(A) | No Build 2040 TNM + StructureBorne Leq dB(A) | No Build 2040 Increase over Existing Noise Level dB | Build Alternative Leq dB(A) | Build 2040 TNM + StructureBorne Leq dB(A) | $\begin{gathered} \text { Build } \\ 2040 \\ \text { Increase } \\ \text { over } \\ \text { Existing } \\ \text { Noise } \\ \text { Level } \\ \text { dB } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R881(6b) | Residence | B (65) | 1 | N/A | 61 | 61 | 61 | 61 | 0 | 61 | 61 | 0 |
| R882(6b) | Residence | B (65) | 1 | N/A | 60 | 60 | 60 | 60 | 0 | 60 | 60 | 0 |
| R883(6b) | Residence | B (65) | 1 | N/A | 60 | 60 | 60 | 60 | 0 | 60 | 60 | 0 |
| R884(6b) | Residence | B (65) | 1 | N/A | 60 | 60 | 60 | 60 | 0 | 60 | 60 | 0 |
| R885(6a) | Residence | B (65) | 1 | N/A | 57 | 57 | 58 | 58 | 1 | 60 | 60 | 3 |
| R886(6a) | Residence | B (65) | 1 | N/A | 58 | 58 | 59 | 59 | 1 | 60 | 60 | 2 |
| R887(6a) | Residence | B (65) | 1 | N/A | 58 | 58 | 58 | 58 | 0 | 60 | 60 | 2 |
| R888(6a) | Residence | B (65) | 1 | N/A | 57 | 57 | 58 | 58 | 1 | 60 | 60 | 3 |
| R889(6a) | Residence | B (65) | 1 | N/A | 57 | 57 | 58 | 58 | 1 | 60 | 60 | 3 |
| R890(6a) | Residence | B (65) | 1 | N/A | 57 | 57 | 58 | 58 | 1 | 59 | 59 | 2 |
| R891(6a) | Residence | B (65) | 1 | N/A | 58 | 58 | 59 | 59 | 1 | 60 | 60 | 2 |
| R892(6a) | Residence | B (65) | 1 | N/A | 56 | 56 | 57 | 57 | 1 | 59 | 59 | 3 |
| R893(6a) | Residence | B (65) | 1 | N/A | 57 | 57 | 58 | 58 | 1 | 60 | 60 | 3 |
| R894(6a) | Residence | B (65) | 1 | N/A | 57 | 57 | 58 | 58 | 1 | 60 | 60 | 3 |
| R895(6a) | Residence | B (65) | 1 | N/A | 58 | 58 | 59 | 59 | 1 | 60 | 60 | 2 |
| R896(6a) | Residence | B (65) | 1 | N/A | 59 | 59 | 60 | 60 | 1 | 62 | 62 | 3 |

 identified as resulting in 25 dB reduction when going from noise exposure outdoors to indoors (FHWA 2011).

## 6 Evaluation of Noise Abatement Measures

Build Alternative traffic noise levels would meet or exceed the NAAC for 322 residences (NAAC B) and 8 Category C recreational receptors. Traffic noise mitigation measures were evaluated for all of these receptors.

Traffic noise mitigation must be feasible and reasonable to be included in the Project's design. ODOT identifies that acoustical feasibility is achieved if a simple majority of impacted receptors achieve a $5 \mathrm{~dB}(\mathrm{~A})$ or greater insertion loss (reduction) as a result of the mitigation measure. In addition, feasibility also considers engineering factors such as safety, topography, environmental constraints (i.e., presence of wetlands), drainage, and excessive barrier height. For noise abatement to be reasonable, ODOT must consider the viewpoints of the residents and property owners who would benefit from the mitigation measure, the cost-effectiveness of the abatement measure, and the ODOT noise reduction design goal of $7 \mathrm{~dB}(\mathrm{~A})$ at one or more benefited properties.

### 6.1 Noise Abatement Considerations

Several noise abatement options were considered for noise impacts under the Build Alternative. Some of these options include speed restrictions, truck restrictions, and alignment changes. The posted speed limits on I-205 range from 65 mph west of the $10^{\text {th }}$ Street interchange and 55 mph east of the $10^{\text {th }}$ Street interchange. Reducing speeds on I-205 would defeat one of the purposes of the Project which is to improve mobility on the facility and reduced traffic speeds are unlikely to reduce noise levels enough to be noticeable. Truck restrictions are not feasible because I-205 is a major truck route for moving goods to, from, and through the Portland metropolitan area.

ODOT also considers changes in Project alignment to abate traffic noise; however, the Project alignment has been identified to minimize property impacts potentially resulting from the Project, such as acquisitions, potentially resulting from the Project. Furthermore, ODOT has found that shifting roadway alignments typically only results in shifting of noise impacts to other properties and is not a reasonable approach for abating traffic noise impacts.

Noise barriers, such as noise walls, are ODOT's preferred method for abating traffic noise impacts from a given project. For this Project, noise barriers in the form of noise walls were evaluated for all impacted receptors. For a noise wall to be feasible it must reduce noise levels at over 50 percent of impacted receptors by $5 \mathrm{~dB}(\mathrm{~A})$ or greater. In order for a noise wall to be reasonable it must cost no more than $\$ 25,000$ per benefited receptor and achieve a $7 \mathrm{~dB}(\mathrm{~A})$ reduction at one or more receptors. For cost estimation purposes one square foot of noise barrier is assumed to cost $\$ 20$ to construct for walls up to 16 feet in height. For walls taller than 16 feet, it is assumed that they would cost $\$ 25$ per square foot to construct.

Noise barriers were modeled at ODOT's right of way unless Project engineers indicated that such a location would not be constructible for a variety of reasons. For example, there are several drainages and some steep topography throughout the noise study area that would, in some cases, make siting a noise wall infeasible at the ODOT right of way. In such cases, noise walls have been modeled in locations nearer to the edge of the roadway; such shifts are discussed in the noise barrier narratives in Section 6.3.

As part of this noise analysis, as-built drawings were reviewed for the original I-205 facility to identify if noise barriers, either berms or walls, were included as mitigation in the original facility. This review did not identify any existing noise barriers part of the original I-205 facility.

### 6.2 Rural and Other Individual Impacted Receptors

Individual impacted receptors, or those that are isolated from more densely developed noise-sensitive land uses, are situated throughout the corridor. For these receptors it is not possible to feasibly provide noise abatement. In general, noise walls cannot be constructed cost effectively since there is not sufficient receptor density to justify the costs. For example, an individually impacted residence is allotted $\$ 25,000$ for noise abatement, which equates to a 10 -foot tall noise wall with a maximum length of 125 feet. The FHWA has found that in order for a noise wall to feasibly reduce noise levels, it must block the line of sight from the receptor to the roadway noise source. To block line of sight, a noise barrier length would need to be roughly equivalent to four times the perpendicular distance from the proposed barrier to the receptor.

- The western portion of the project area, roughly the area from where Woodbine Road crosses beneath I-205 and the areas to the west, includes primarily rural low density developed areas. Impacts occur at the following receptors in this area: LT-1/ST-1, ST-2, ST-3, ST-4, R1, R2, R5 to R7, R12, R13, R14, R15, and R16. Other than LT-1/ST-1, which is a church/preschool/daycare, the remaining receptors are relatively isolated rural residences offset from one another by relatively large distances.
o For LT-1/ST-1 HMMH completed ODOT's NAAC C calculation table, the results of which are included in Appendix D. LT-1/ST-1 would be located 186 feet from the realigned I-205 facility, further away than it currently is from I-205 as a result of the roadway realignment to cross the Tualatin River. To block the line of sight from LT-1/ST-1 to the roadway a noise wall length would need to be four times the perpendicular distance from the barrier, which equates to 744 feet. Even at a height of 8 feet, a barrier of this length would be unreasonably expensive according to ODOT's NAAC C calculation methodology. Therefore, this barrier is not feasible because it cannot be constructed tall enough and long enough to achieve a $5 \mathrm{~dB}(\mathrm{~A})$ reduction.
- Another individual impact is predicted at R293, south of the I-205 NB lanes and 2,650 feet east of the $10^{\text {th }}$ Street interchange. This receptor is not clustered with other noise-sensitive receptors; therefore, a noise barrier cannot be feasibly constructed to reduce noise levels in the area.
- Receptor R466 is the Atlas Immersion Academy School. A noise barrier cannot be constructed in this area because it would need to cross three driveways that accessing the school. A noise wall in this area with gaps in it would not feasibly reduce noise levels at the impacted receptor.
- Two receptors, R693 and R694, located northeast of the I-205 and OR 213 interchange, also have driveways accessing the nearby roadway. A noise wall cannot feasibly reduce noise levels because it would have gaps allowing for driveway access.


### 6.3 Noise Walls

Thirteen noise walls were evaluated to determine if they could feasibly and reasonably reduce noise levels at clusters of impacted receptors. Noise walls were evaluated along the ODOT right of way unless otherwise stated and were analyzed at heights ranging from 10 to 24 feet in height. Detailed noise wall tabular analyses are included in Appendix D. Table 10 provides a summary of the Project noise wall abatement analysis and the subsections that follow provide a narrative descriptions of these analyses. Noise walls identified as being feasible and reasonable per ODOT regulations are shown in red on Figure 18 to Figure 32 in Section 11 of this report. Walls analyzed in detail but not recommended are shown in black on these same figures.

ODOT's Noise Manual provides a special use area worksheet for NAAC C land uses applicable to some NAAC C uses, such as parks. Other than in the analysis described in Section 6.2, this worksheet was not used in this noise abatement analysis, because each of the NAAC C land uses are co-located behind noise walls with other noise-sensitive land uses, such as NAAC B residences with outdoor uses at apartment complexes (i.e., balconies and patios). For this reason, other impacted NAAC C receptors were treated as being equivalent to "one" residential unit for considerations of cost reasonableness calculations.

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Table 10. Noise Wall Analysis Summary

| Wall | No. of Impacts | Length (feet) | Height (feet) | No. of Impacts Benefited | Acoustically Feasible? | Achieves Acoustic Design Goal? | Total Benefits | Estimated Cost per Benefit | Cost Reasonable? | Wall Recommended ? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 16 | 1,560 | 16 | 12 | Yes | Yes | 15 | \$33,288 | No | No |
| 2 | 41 | 2,070 | 12 | 24 | Yes | Yes | 29 | \$17,147 | Yes | Yes |
| 3 | 41 | 2,161 | 20 | 28 | Yes | Yes | 35 | \$30,840 | No | No |
| 4 | 37 | 1,517 | 14 | 33 | Yes | Yes | 75 | \$5,668 | Yes | Yes |
| 5 | 18 | 1,550 | 24 | 0 | No | N/A | 0 | N/A | N/A | No |
| 6a | 55 | 3,697 | 14 | 45 | Yes | Yes | 74 | \$14,024 | Yes | Yes |
| 6b | 10 | 1,165 | 14 | 10 | Yes | Yes | 11 | \$29,625 | No | No |
| 7 | 16 | 989 | 14 | 11 | Yes | Yes | 12 | \$22,725 | Yes | Yes |
| 8 | 25 | 683 | 24 | 12 | No | N/A | 17 | N/A | N/A | No |
| 9 | 17 | 594 | 24 | 8 | No | N/A | 8 | N/A | N/A | No |
| 10 | 12 | 3,257 | 17 | 7 | Yes | No | 15 | \$90,538 | N/A | No |
| 11 | 5 | 1,145 | 16 | 3 | Yes | Yes | 3 | \$152,675 | No | No |
| 12 | 43 | 1,381 | 18 | 23 | Yes | Yes | 46 | \$13,504 | Yes | Yes |

### 6.3.1 Noise Wall 1

Noise wall 1 was evaluated at a location 30 feet from the fog line of the NB I-205 lanes extending north from Blankenship Road 1,560 feet (see Figure 23). The noise wall was evaluated to determine if it could effectively abate noise at impacted residential receptors R49 to R53, R55 to R60, R62, R71, R73, R74, and R75. Analysis of noise walls in this area suggested a barrier positioned along the l-205 right of way cannot effectively block the line of sight to a sufficient number of impacted receptors to be feasible. As a result, ODOT elected to analyze the barrier closer to the l-205 travel lanes, at a position where a small earthen berm currently exists. Design engineers for the project indicated installation of a noise wall in this area would require removal and leveling of the top four feet of the berm. This adjustment in noise wall footing height was taken into consideration in this analysis. Noise modeling, as documented in the detailed tables in Appendix D, shows that a noise wall 14 feet or taller would reduce noise levels by $5 \mathrm{~dB}(\mathrm{~A})$ or greater at over 50 percent of the impacted receptors and is therefore feasible. A noise wall 16 feet tall and 1,560 feet long, would achieve the design goal of a $7 \mathrm{~dB}(\mathrm{~A})$ reduction at one or more receptors, would benefit 15 receptors, and would cost $\$ 499,320$ or $\$ 33,288$ per benefited receptor. Noise wall 1 would be feasible but not reasonable because it would exceed the ODOT guideline maximum of $\$ 25,000$ per benefited receptor, and is therefore not recommended for inclusion in the Project design at this time.

### 6.3.2 Noise Wall 2

Noise wall 2 was evaluated along the north side of the SB I-205 lanes where I-205 is elevated above the surrounding land uses and then would jog further away from $\mathrm{I}-205$ to the facilities right of way (see Figure 23). The noise wall would extend north from where I-205 crosses Blankenship Road approximately 2,070 feet. The noise wall would provide shielding to impacted residential receptors and an apartment pool IDs ST-5a, ST-5b, R20 to R41, R63 to R68, R76 to R81, and R96 to R101. Noise modeling, as documented in the detailed tables in Appendix $D$, shows that the noise wall at 12 feet would reduce noise levels by $5 \mathrm{~dB}(A)$ or greater at over 50 percent of the impacted receptors and is therefore feasible. A 12-foot tall noise wall, 2,070 feet long, would also achieve the design goal of $7 \mathrm{~dB}(\mathrm{~A})$ reduction at one or more receptors, would benefit 29 receptors, and would cost $\$ 497,260$ or $\$ 17,147$ per benefited receptor. Noise wall 2 would be both feasible and reasonable and is recommended for inclusion in the Project design. Note that the residential equivalency for the pool was considered to be one for the purposes of this analysis; however, even without its inclusion the noise wall would still be feasible and reasonable.

### 6.3.3 Noise Wall 3

Noise wall 3 was evaluated at a location 30 feet from the fog line of the I-205 NB lanes (See Figure 23 and Figure 24). The noise wall would extend south from where I-205 crosses Blankenship Road approximately 2,161 feet. The noise wall was analyzed to evaluate noise abatement at impacted residential receptor IDs ST-7,

R114 to R124, R126 to R131, R133 to R150, R152, R153, and R155 to R1557. Initial analysis of noise walls in this area identified that a barrier positioned along the I-205 right of way cannot effectively block the line of sight to a sufficient number of impacted receptors to be feasible. As a result, ODOT elected to analyze the barrier closer to the l-205 travel lanes, at a position where a small earthen berm currently exists. Design engineers for the project indicated installation of a noise wall in this area would require removal and leveling of the top four feet of the berm. This adjustment in noise wall footing height was taken into consideration in this analysis. Noise modeling, as documented in the detailed tables in Appendix D, shows that a noise wall 20 feet tall would reduce noise levels by $5 \mathrm{~dB}(\mathrm{~A})$ or greater at over 50 percent of the impacted receptors and is therefore feasible. The 20 -foot tall noise wall, 2,160 feet long, would achieve the design goal of $7 \mathrm{~dB}(\mathrm{~A})$ reduction at one or more receptors, would benefit 35 receptors, and would cost $\$ 1,079,400$ or $\$ 30,840$ per benefited receptor. Noise wall 3 would be feasible but not reasonable because it would exceed the ODOT guideline maximum of $\$ 25,000$ per benefited receptor, and is therefore not recommended for inclusion in the Project design at this time.

### 6.3.4 Noise Wall 4

Noise wall 4 was evaluated along the north side of the SB I-205 lanes where the facility is on elevated topography (See Figure 23 and Figure 24). The noise wall would extend south from where I-205 crosses Blankenship Road approximately 1,518 feet. Preliminary engineering identified that the barrier would need to stop at this point because of utility and/or drainage requirements. The noise wall would provide shielding to impacted residential receptors IDs R168, R169, R171, R172, R174, R175, R177, R178, R180, R181, R183, R187, R189, R191, R193, R195, R197, R199, R201, R203, R207, R209 to R211, R213, R215 to R217, R221 to R223, R226, R229, R232, R235, and R271 to R273. Noise modeling, as documented in the detailed tables in Appendix D, shows that at 10 feet or taller the noise wall would reduce noise levels by $5 \mathrm{~dB}(\mathrm{~A})$ or greater at over 50 percent of the impacted receptors and therefore would be feasible. A 14-foot tall noise wall, 1,517 feet long, would achieve the design goal of $7 \mathrm{~dB}(\mathrm{~A})$ reduction at one or more receptors, would benefit 75 receptors, and would cost $\$ 425,120$ or $\$ 5,688$ per benefited receptor. Noise wall 4 would be both feasible and reasonable and is recommended for inclusion in the Project design.

### 6.3.5 Noise Wall 5

Noise wall 5 was evaluated along the NB I-205 right of way extending northwest from $10^{\text {th }}$ Street 1,550 feet (see Figure 24 and Figure 25). The noise wall would provide shielding to impacted residential receptors IDs ST-8, R274 to R285, and R288 to R291. I-205 is at a higher elevation than the impacted receptors in this area and the topography between them is below both. At the ODOT right of way, the barrier would be approximately 10 feet below the elevation of the receptors and further below the highway. The noise wall cannot be located closer to the I-205 mainline due to the onramp from $10^{\text {th }}$ Street to $\mathrm{I}-205$ NB. As a result, a noise barrier even at 24 feet tall
would not break the line of sight to the receptors and would not reduce noise levels by $5 \mathrm{~dB}(\mathrm{~A})$ or greater at over 50 percent of the receptors. Therefore, noise wall 5 would not be feasible.

### 6.3.6 Noise Wall 6a

Noise wall 6a was evaluated along the north side of the SB I-205 lanes 3,697 feet south of the $10^{\text {th }}$ Street Interchange and located on a ridge at the SB I-205 right-ofway (See Figure 26, Figure 27, and Figure 28). Initially noise wall 6a and noise wall 6 b were a continuous noise barrier; however, detailed survey of the are identified that an approximately 100 foot wide gap would be needed due to steep topography where a drainage passes through the area. For this reason the noise wall was divided into noise walls $6 a$ and 6 b. The noise wall would extend south from the Sunset Avenue overcrossing along a ridge between Imperial Drive and the I-205 SB lanes for 3,697 feet. The noise wall would provide shielding to impacted residential receptors IDs ST-9, R306, R310, R311, R322 to R330, R333, R337 to R352, R360 to R364, R371 to R386, R395, R404, R405, and R423. Noise modeling, as documented in the detailed tables in Appendix D, shows that at 10 feet or taller the noise wall would reduce noise levels by $5 \mathrm{~dB}(\mathrm{~A})$ or greater at over 50 percent of the impacted receptors and therefore would be feasible. A 14-foot tall noise wall, 3,697 feet long, would achieve the design goal of $7 \mathrm{~dB}(\mathrm{~A})$ reduction at one or more receptors, would benefit 74 receptors, and would cost $\$ 1,037,740$ or $\$ 14,024$ per benefited receptor. Noise wall 6a would be both feasible and reasonable and is recommended for inclusion in the Project design.

### 6.3.7 Noise Wall 6b

Noise wall 6b was evaluated along the north side of the SB I-205 lanes beginning the drainage gully described in Section 6.3.7. (See Figure 26). The noise wall would extend along a ridge between Imperial Drive and the I-205 SB lanes for 1,165 feet. The noise wall would provide shielding to impacted residential receptors IDs R296 to R305. Noise modeling, as documented in the detailed tables in Appendix D, shows that at 12 feet or taller the noise wall would reduce noise levels by $5 \mathrm{~dB}(\mathrm{~A})$ or greater at over 50 percent of the impacted receptors and therefore would be feasible. A 14foot tall noise wall, 1,165 feet long, would achieve the design goal of $7 \mathrm{~dB}(\mathrm{~A})$ reduction at one or more receptors, would benefit 11 receptors, and would cost $\$ 325,880$ or $\$ 29,625$ per benefited receptor. Noise wall 6 b would be feasible but not reasonable because it would exceed the ODOT guideline maximum of $\$ 25,000$ per benefited receptor, and is therefore not recommended for inclusion in the Project design at this time.

### 6.3.8 Noise Wall 7

Noise wall 7 was evaluated along the north side of the SB I-205 right of way extending 959 feet to the east from where Sunset Avenue crosses I-205 (See Figure 28). The noise wall would provide shielding to impacted residential receptor IDs R423, R426, R427, R429, R432, R440, R442 to R449, R452, and R453. The
impacted receptors are situated on a ridge overlooking I-205 below. Detailed topographic survey of the area was conducted to ascertain engineering feasibility. The noise wall location analyzed is the most feasible from an engineering perspective. Noise modeling, as documented in the detailed tables in Appendix $D$, shows that at 14 feet or taller the noise wall would reduce noise levels by $5 \mathrm{~dB}(\mathrm{~A})$ or greater at over 50 percent of the impacted receptors and therefore would be feasible. A 14-foot tall noise wall, 989 feet long, would achieve the design goal of $7 \mathrm{~dB}(\mathrm{~A})$ reduction at one or more receptors, would benefit 12 receptors, and would cost $\$ 272,700$ or $\$ 22,725$ per benefited receptor. Noise wall 7 would be both feasible and reasonable and is recommended for inclusion in the Project design.

### 6.3.9 Noise Wall 8

Noise wall 8 was evaluated north of the I-205 SB lanes between A Street and OR 43, in an area where the existing Broadway Bridge overpass would be removed as part of the project (See Figure 29). ODOT obtained detailed survey data to identify the specific height of the footing of the noise wall in this area since there are steep slopes adjacent to the south between the on-ramp to I-205 SB from OR 43 and the noise sensitive receptors. The noise wall was evaluated to determine if it would effectively abate traffic noise at impacted residential receptor IDs R489 to R493, R496, R497, R501 to R507, R521 to R525, and R527 to R532. The impacted residences are situated on a ridge overlooking I-205 below. Noise modeling, as documented in the detailed tables in Appendix D, shows that even at 24 feet tall the noise wall would not reduce noise levels by $5 \mathrm{~dB}(\mathrm{~A})$ or greater at over 50 percent of the impacted receptors and therefore would not be feasible per ODOT policy. For this reason noise wall 8 is not recommended for inclusion in the Project design.

### 6.3.10 Noise Wall 9

Noise Wall 9 would be located along the I-205 NB exit ramp to OR 43 and would provide shielding to impacted residential receptor IDs R467 to 483, apartment units at two separate structures (See Figure 29). Topography in the area includes a relatively steep slope as one moves away from I-205 towards the apartments and down the exit ramp. Noise modeling, as documented in the detailed tables in Appendix D, shows that even at 24 feet the noise wall would not reduce noise levels by $5 \mathrm{~dB}(\mathrm{~A})$ or greater at over 50 percent of the impacted receptors and therefore would not be feasible. Noise wall 9 is not recommended for inclusion in the Project design at this time.

### 6.3.11 Noise Wall 10

Noise wall 10 was evaluated along the north side of the I-205 Abernethy Bridge structure adjacent to the SB I-205 lanes and exit ramps to OR 43 and OR 99E (See Figure 29 and Figure 30). The Abernethy structure noise wall would provide shielding to impacted receptors located north of the bridge on both sides of the Willamette River and would be 3,257 feet long. Bridge deck noise that emanates through the deck itself cannot be abated with a noise wall on the structure. For this reason, the
contribution of bridge deck noise was analyzed via a noise monitoring effort as described in Section 4.2.1. Structure-borne noise was added to the TNM noise levels for receptors near the bridge as to not overestimate the reductions in traffic noise that would be expected with a noise wall on the bridge. Noise wall heights ranging from 9 feet to 17 feet were evaluated. Design engineers identified (HDR 2017a) that a 17 -foot on structure barrier is as tall as feasible without reinforcing the structure to accommodate the barrier which is considered infeasible. The noise wall would provide shielding to impacted residential receptors and Jon Storm Park, specifically:

- Residential IDs: R552, R553, R557, R562 to R564, and R571
- Jon Storm Park outdoor use areas IDs: ST-13 and R700 to R703

Noise modeling, as documented in the detailed tables in Appendix D, shows that even at 15 feet or taller the noise wall would reduce noise levels by $5 \mathrm{~dB}(\mathrm{~A})$ or greater at over 50 percent of the impacted receptors and is therefore feasible. However, even at 17 -feet tall a noise wall would not achieve the design goal of 7 $\mathrm{dB}(\mathrm{A})$ reduction at one or more receptors, and at 17 -feet tall a noise wall would cost $\$ 90,538$ per benefitted receptor which is unreasonably expensive for noise abatement. For these reasons noise wall 10 is not recommended for inclusion in the Project design at this time.

### 6.3.12 Noise Wall 11

Noise wall 11 was evaluated along the north side of the SB I-205 right of way to provide shielding to noise-sensitive receptors situated in the northeast quadrant of the I-205 and OR 213 interchange (See Figure 32). The noise wall would provide shielding to impacted residential receptor IDs R695 to R699. Noise modeling, as documented in the detailed tables in Appendix D , shows that at 16 feet or taller a noise wall would reduce noise levels by $5 \mathrm{~dB}(\mathrm{~A})$ or greater at over 50 percent of the impacted receptors and therefore would be feasible. A 16-foot tall noise wall, 1,145 feet long, would achieve the design goal of $7 \mathrm{~dB}(\mathrm{~A})$ reduction at one or more receptors, would benefit three receptors, and would cost $\$ 458,025$ or $\$ 152,675$ per benefited receptor. Noise wall 11 would be feasible but would not be reasonable because it would exceed the ODOT guideline maximum of $\$ 25,000$ per benefited receptor and is therefore not recommended for inclusion in the Project design.

### 6.3.13 Noise Wall 12

Noise wall 12 was evaluated along the north side of the SB I-205 right of way to provide shielding to the Grand Cove Development, specifically the Edgewater at the Cove Apartments, in Oregon City (See Figure 31). The apartment development is currently under construction and is behind the Oregon City Shopping Center, east of OR 99E. Several units have balconies or patios that will face l-205, resulting in impacts at 43 outdoor use areas (i.e., balconies or patios). Receptor IDs R704 to R706, R710, R711, R749 to R752, R755, R756, R793 to R796, R799, R800, R809, R838 to R840, R843 to R845, R847, R848, and R863 to R878 are predicted to exceed the NAAC at the complex. Noise modeling, as documented in the detailed
tables in Appendix D, shows that at 18 feet or taller a noise wall would reduce noise levels by $5 \mathrm{~dB}(\mathrm{~A})$ or greater at over 50 percent of the impacted receptors and therefore would be feasible. An 18-foot tall noise wall, 1,381 feet long, would achieve the design goal of $7 \mathrm{~dB}(\mathrm{~A})$ reduction at one or more receptors, would benefit 46 receptors, and would cost $\$ 621,200$ or $\$ 13,504$ per benefited receptor. Noise wall 12 would be both feasible and reasonable and is recommended for inclusion in the Project design.

## 7 Construction Noise and Vibration Analysis

Analysis of temporary construction noise and vibration impacts was completed for the Project. This effort included a qualitative assessment of noise and vibration from general construction of the roadway as well as a semi-quantitative analysis of blasting noise and vibration associated with the rock cut.

### 7.1 General Construction Noise and Vibration

If the Build Alternative were constructed sensitive land uses and structures would be exposed to temporarily elevated noise and vibration levels which may be a source of annoyance to the public.

Construction noise would be the result of operating construction equipment along the Project right of way. Noise levels from construction equipment would be dependent upon several factors such as the type of equipment, construction schedule, and distance to the equipment in use for the various Project construction activities.

Temporary construction vibration, similar to construction noise, would result in temporary elevated vibration levels; however, construction vibration attenuates more quickly with distance than noise. As a result, only sensitive structures in much closer proximity to the Project could be potentially impacted by construction vibration.

Typical construction equipment maximum noise ( $L_{\max }$ ) and vibration (peak particle velocity in inches per second [ppv]) levels are provided in Table 11 and Table 12, respectively.

Table 11. Typical Construction Equipment Noise Levels

|  |  |  | Specified |  |
| :---: | :---: | :---: | :---: | :---: |
| Equipment Description | Impulsive Noise Device? ${ }^{1}$ | Acoustical use Factor (\%) ${ }^{2}$ | $\begin{gathered} L_{\text {max }} @ 50 f t \\ (\mathrm{~dB}(\mathrm{~A}), \\ \text { slow })^{3} \end{gathered}$ | Actual Measured $L_{\text {max }}$ @ 50ft $(\mathrm{dB}(\mathrm{A}) \text {, slow })^{4}$ |
| All Other Equipment > 5 HP | No | 50 | 85 | -N/A- |
| Auger Drill Rig | No | 20 | 85 | 84 |
| Backhoe | No | 40 | 80 | 78 |

Table 11. Typical Construction Equipment Noise Levels

| Equipment Description | Impulsive Noise Device? ${ }^{1}$ | Acoustical use Factor (\%) ${ }^{2}$ | Specified <br> Lmax @ 50ft <br> (dB(A), slow) ${ }^{3}$ | Actual Measured Lmax @ 50ft (dB(A), slow) ${ }^{4}$ |
| :---: | :---: | :---: | :---: | :---: |
| Bar Bender | No | 20 | 80 | -N/A- |
| Blasting | Yes | -N/A- | 94 | -N/A- |
| Boring Jack Power Unit | No | 50 | 80 | 83 |
| Chain Saw | No | 20 | 85 | 84 |
| Clam Shovel (dropping) | Yes | 20 | 93 | 87 |
| Compactor (ground) | No | 20 | 80 | 83 |
| Compressor (air) | No | 40 | 80 | 78 |
| Concrete Batch Plant | No | 15 | 83 | -N/A- |
| Concrete Mixer Truck | No | 40 | 85 | 79 |
| Concrete Pump Truck | No | 20 | 82 | 81 |
| Concrete Saw | No | 20 | 90 | 90 |
| Crane | No | 16 | 85 | 81 |
| Dozer | No | 40 | 85 | 82 |
| Drill Rig Truck | No | 20 | 84 | 79 |
| Drum Mixer | No | 50 | 80 | 80 |
| Dump Truck | No | 40 | 84 | 76 |
| Excavator | No | 40 | 85 | 81 |
| Flat Bed Truck | No | 40 | 84 | 74 |
| Front End Loader | No | 40 | 80 | 79 |
| Generator | No | 50 | 82 | 81 |

Table 11. Typical Construction Equipment Noise Levels

| Equipment Description | Impulsive Noise Device? ${ }^{1}$ | Acoustical use Factor (\%) ${ }^{2}$ | Specified <br> $L_{\text {max }} @ 50 f t$ <br> (dB(A), <br> slow) ${ }^{3}$ | Actual Measured Lmax @ 50ft $(\mathrm{dB}(\mathrm{A}) \text {, slow })^{4}$ |
| :---: | :---: | :---: | :---: | :---: |
| Generator (<25KVA, VMS signs) | No | 50 | 70 | 73 |
| Gradall | No | 40 | 85 | 83 |
| Grader | No | 40 | 85 | -N/A- |
| Grapple (on backhoe) | No | 40 | 85 | 87 |
| Horizontal Boring Hydr. Jack | No | 25 | 80 | 82 |
| Hydra Break Ram | Yes | 10 | 90 | -N/A- |
| Impact Pile Driver | Yes | 20 | 95 | 101 |
| Jackhammer | Yes | 20 | 85 | 89 |
| Man Lift | No | 20 | 85 | 75 |
| Mounted Impact hammer (hoe ram) | Yes | 20 | 90 | 90 |
| Pavement Scarafier | No | 20 | 85 | 90 |
| Paver | No | 50 | 85 | 77 |
| Pickup Truck | No | 40 | 55 | 75 |
| Pneumatic Tools | No | 50 | 85 | 85 |
| Pumps | No | 50 | 77 | 81 |
| Refrigerator Unit | No | 100 | 82 | 73 |
| Rivit Buster/chipping gun | Yes | 20 | 85 | 79 |
| Rock Drill | No | 20 | 85 | 81 |
| Roller | No | 20 | 85 | 80 |
| Sand Blasting (Single Nozzle) | No | 20 | 85 | 96 |

Table 11. Typical Construction Equipment Noise Levels

| Equipment Description | Impulsive Noise Device? ${ }^{1}$ | Acoustical use Factor (\%) ${ }^{2}$ | Specified <br> $L_{\text {max }}$ @ 50ft (dB(A), slow) ${ }^{3}$ | Actual Measured Lmax @ 50ft (dB(A), slow) ${ }^{4}$ |
| :---: | :---: | :---: | :---: | :---: |
| Scraper | No | 40 | 85 | 84 |
| Shears (on backhoe) | No | 40 | 85 | 96 |
| Slurry Plant | No | 100 | 78 | 78 |
| Slurry Trenching Machine | No | 50 | 82 | 80 |
| Soil Mix Drill Rig | No | 50 | 80 | -N/A- |
| Tractor | No | 40 | 84 | -N/A- |
| Vacuum Excavator (Vactruck) | No | 40 | 85 | 85 |
| Vacuum Street Sweeper | No | 10 | 80 | 82 |
| Ventilation Fan | No | 100 | 85 | 79 |
| Vibrating Hopper | No | 50 | 85 | 87 |
| Vibratory Concrete Mixer | No | 20 | 80 | 80 |
| Vibratory Pile Driver | No | 20 | 95 | 101 |
| Warning Horn | No | 5 | 85 | 83 |
| Welder/Torch | No | 40 | 73 | 74 |
| Notes: <br> 1. An indication as to whether or not the equipment is an impact device. <br> 2. The acoustical usage factor to assume for modeling purposes. <br> 3. The specification "spec" limit for each piece of equipment expressed as an Lmax level in $\mathrm{dB}(\mathrm{A})$ at a reference distance of 50 feet. <br> 4. The measured "ACTUAL" noise level at 50 feet for each piece of equipment. <br> Source: FHWA, 2006 |  |  |  |  |

Table 12. Typical Construction Equipment Vibration Levels

| Equipment Description |  | PPV at 25 ft |
| :--- | :--- | :--- |
| Pile Driver(impact) | Upper range | 1.518 |
| Pile Driver (sonic) | Typical | 0.644 |
| Clam shovel drop (slurry wall) | Typical | 0.170 |
| Hydromill (slurry wall) |  | 0.202 |
| Vibratory Roller | In soil | 0.008 |
| Hoe Ram |  | 0.017 |
| Large bulldozer |  | 0.210 |
| Caisson drilling |  | 0.089 |
| Loaded Trucks |  | 0.089 |
| Jackhammer |  | 0.089 |
| Small bulldozer |  | 0.076 |
| Source: FTA, 2006 |  | 0.035 |

### 7.2 Rock Cut (Blasting) Noise and Vibration

Blasting would be required to accomplish the rock cut needed to accommodate the widening of the I-205 facility from the Sunset Avenue overpass to the A Street overpass. Consequently, blast noise and vibration could result in impacts to nearby sensitive land uses. Blast vibration is calculated using the methods described in the Department of Interior Office of Surface Mining Reclamation and Enforcement (OSMRE) Blasting Guidance Manual (OSMRE, 1987). This approach uses the Scaled Distance Equation, which describes the relationship between distance in feet from a blast to a receptor point and the maximum explosive charge weight in pounds (lbs) per 8 milliseconds delay period. Using this equation, preliminary engineering determined the rock cut could be accomplished, without damaging nearby structures, with charge weights (per 8-millisecond delay period) ranging from 2 lbs to 40 lbs (Shannon and Wilson, 2017). The estimated range of distances to impact thresholds for vibration damage are provided in Table 13 for these sizes of charges, and include an upper bounds (i.e., worst case) and lower bounds (i.e., best case). The damage thresholds are from the Federal Transmit Administration's guidance manual (FTA, 2006) and the vibration attenuation rates are based on OSMRE's construction vibration calculation methodology. The range of distances to air blast damage levels are provided in Table 14. Attenuation rates for air blasts (blast noise) were also calculated assuming a construction detonation. The blasting effort will be designed to
avoid structural damage at nearby sensitive areas while minimizing annoyance to the extent practicable.

## Table 13. Estimated Blast Vibration Damage Distances

| Building Category | Damage Threshold (PPV in/sec) | Lower Bounds |  | Upper Bounds |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Distance to Damage Threshold for 2 lb Charge (feet) | Distance to Damage Threshold for 40 lb Charge (feet) | Distance to Damage Threshold for 2 lb Charge (feet) | Distance to Damage Threshold for 40 lb Charge (feet) |
| Reinforced-concrete, steel, or timber (Category 1) | 0.5 | 16 | 71 | 67 | 300 |
| Engineered concrete and masonry, no plaster (Category 2) | 0.3 | 22 | 98 | 92 | 415 |
| Non-engineered timber and masonry buildings | 0.2 | 28 | 125 | 120 | 535 |
| Buildings extremely susceptible to vibration damage | 0.12 | 38 | 175 | 165 | 720 |

Source: Shannon and Wilson, 2017 and HMMH, 2018

Table 14. Estimated Blast Noise Levels

| Charge Weight (lbs) | Damage Criteria <br> [linear decibels <br> $(\mathrm{dBL})]$ | Distance to <br> Annoyance Criteria <br> (dBL) | Distance to <br> Criteria <br> (feet) | Annoyance <br> Criteria <br> (feet) |
| :--- | :---: | :---: | :---: | :---: | :---: |
| 9 lbs | 151 dBL | 120 | 4 | 325 |
| 40 lbs |  |  | 7 | 550 |

Source: Shannon and Wilson, 2017 and HMMH, 2018

### 7.3 Construction Noise and Vibration Abatement

To avoid, minimize, and abate temporary adverse noise and vibration impacts the following measures, as described in Section 290.32 of ODOT standard specifications, should be taken to the extent practicable:

- The contractor shall comply with all state and local sound control and noise level rules, regulations, and ordinances that would apply to any work performed pursuant to the contract.
- The contractor must provide a detailed construction noise control plan, which would list all of the proposed construction equipment and types of construction activity.
- All equipment shall comply with pertinent equipment noise standards of the US Environmental Protection Agency (EPA).
- All equipment used shall have sound control devices no less effective than those provided on the original equipment. No equipment shall have unmuffled exhaust.
- All equipment shall comply with the pertinent equipment noise standards found in the FHWA Roadway Construction Noise Model (FHWA 2006).
- No construction shall be performed within 1,000 feet of an occupied dwelling unit on weekends, legal holidays, and between the hours of 10:00 p.m. and 7:00 a.m. on other days without the approval of ODOT's Project Manager.
- No pile driving, hoe ramming, or blasting operations shall be performed within 3,000 feet of any occupied dwelling unit on weekends, legal holidays, and between the hours of 10:00 p.m. and 7:00 a.m. on other days without the approval of ODOT's Project Manager.
- The noise from rock crushing or screening operations within 3,000 feet of any occupied dwelling shall be mitigated by strategic placement of material stockpiles between the operation and the affected dwelling or by other means approved by ODOT's Project Manager.

Should specific noise complaints occur during the construction of the project, one or more of the following noise abatement measures may be required at the Contractor's expense, as directed by ODOT's Project Manager:

- Locate stationary construction equipment as far from the nearby noise-sensitive properties as possible.
- Shut off idling equipment.
- Use alternative methods or equipment which produces less noise.
- Reschedule construction operations to avoid periods of noise annoyance identified in the complaint.
- Notify nearby residences whenever extremely noisy work will be occurring.
- Install temporary or portable acoustic barriers around stationary construction noise sources.
- Operate electric-powered equipment using line voltage power instead of on-site generators.
- Use manually adjustable or new broadband backup alarms which can be localized and focused to the danger zone and set to the low noise setting on all construction vehicles used during nighttime hours.

ODOT employs several methods to ensure successful and safe blasting, specifically (ODOT 2018):

- Require an approved blasting consultant to design/approve the blasting plans
- Perform pre-blast surveys. These are done either by or through the blasting contractor prior to the blast to document the condition of structures, foundations, and windows prior to exposure to vibration from blasting.
- ODOT reviews the submitted blasting plans prior to allowing the blasts to proceed
- Require ground vibration monitoring during the blasts
- Require that blast mats be laid upon the blast area to help contain flying rock • Blasting contractors are licensed and bonded

ODOT will obtain construction noise variances as needed from West Linn, Oregon City, and Clackamas County.

## 8 Information for Local Government Officials

A copy of this report will be provided to the planning departments of the City of West Linn, the City of Oregon City, and Clackamas County by ODOT. By providing this to the local agencies responsible for planning in the areas analyzed it will be possible for these agencies to inform development.

At the time of the development of this report several vacant lands are located within the study area. Most of the vacant areas are located between the Stafford Road and $10^{\text {th }}$ Street interchanges with several other smaller vacant areas between $10^{\text {th }}$ Avenue and OR 43 as well as between OR 99E and OR 213. Table 15 provides the distances to ODOT's NAAC. Local agencies should consider whether residential (NAAC B), public use such as schools and parks (NAAC C), and commercial uses (NAAC E) are compatible in these areas.

Table 15. Distances to NAACs for Local Planning Agencies

| I-205 Segment | Distance to NAAC B \& C <br> Threshold (feet) | Distance to NAAC E <br> Threshold (feet) |
| :--- | :---: | :---: |
| Stafford Road to $10^{\text {th }}$ Street | 420 | 150 |
| $10^{\text {th }}$ Street to OR 43 | 435 | 155 |
| OR 99E to OR 213 | 480 | 170 |

## 9 Statement of Likelihood

Based on the findings of this noise technical report, ODOT will further evaluate traffic noise abatement measures in the form of noise walls during the final design of the roadway. At a minimum, the following seven locations will be reevaluated in detail:

- Noise Wall 2: North of Blankenship Road located parallel to the SB I-205 lanes.
- Noise Wall 4: South of Blankenship Road located parallel to the SB I-205 lanes.
- Noise Wall 6a: 4,750 feet south of the $10^{\text {th }}$ Street interchange and located on a ridge at the SB I-205 right of way.
- Noise Wall 7: North of the Sunset Avenue overcrossing and west of the I-205 SB lanes extending for approximately 960 feet.

These noise walls would abate impacts at 108 residences and would benefit an additional 36 residences and the retirement home. Preliminary costs for the noise walls would total $\$ 2,315,640$. If during final design of the roadway these conditions have changed substantially, the abatement measure might no longer be feasible and reasonable and therefore not provided. A final decision will be made upon completion of the Project's final design, a cost estimating process, and the public involvement process.

## 10 References

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## 11 Figures



Figure 2. Comprehensive Plan Designations



Figure 4. Existing Conditions/No Build Alternative



Figure 6. Existing Conditions/No Build Alternative



Figure 8. Existing Conditions/No Build Alternative



Figure 10. Existing Conditions/No Build Alternative


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1-205: Stafford Road to OR 99E Corridor Widenin \& Abernethy Bridge Seismic Retrofit / Widening Figure 11
Measured and Modeled Receptor Sites Existing Conditions and No Build Alternative
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Figure 12. Existing Conditions/No Build Alternative



Figure 14. Existing Conditions/No Build Alternative



Figure 16. Existing Conditions/No Build Alternative



Figure 18. Build Alternative


Figure 19. Build Alternative


Figure 20. Build Alternative



Figure 22. Build Alternative



Figure 24. Build Alternative



Figure 26. Build Alternative



Figure 28. Build Alternative







Figure 32. Build Alternative



i) $\Gamma_{0}^{200} \underset{400 \text { Feet }}{\sim}$


1-205: Stafford Road to OR 99E Corridor Widening \& Abernethy Bridge Seismic Retrofit / Widening Figure 33
Structure-Borne Noise Measurement Locations
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Figure 34. Structure-Borne Analysis Schematic Drawing


Figure 35. Structure-Borne Analysis Drop of Rates Chart


## Appendix A. Noise Measurement Data Sheets, Photographs, and NCHRP 791 Worksheets

## SHORT-TERM NOISE MEASUREMENT DATA SHEET

PROJECT: K19786:I-205CW
JOB NO.: 309180.000
MEASUREMENT SITE NO.: ST-1
PERSONNEL: SRN
ADDRESS/DESCRIPTION: Southlake Church and Preschool
DATE: 8/29/17

| \# | Time | $\begin{gathered} \hline \text { Leq } \\ (\mathrm{dBA}) \end{gathered}$ | $\begin{gathered} L_{\text {min }} \\ (d B A) \end{gathered}$ | $\begin{aligned} & \mathrm{L}_{\max } \\ & (\mathrm{dBA}) \end{aligned}$ | $\begin{gathered} \mathrm{L}_{10} \\ (\mathrm{dBA}) \end{gathered}$ | $\begin{gathered} \mathrm{L}_{33} \\ (\mathrm{dBA}) \end{gathered}$ | $\begin{gathered} \mathrm{L}_{50} \\ (\mathrm{dBA}) \end{gathered}$ | $\begin{gathered} \mathrm{L}_{90} \\ (\mathrm{dBA}) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 12:35:00 | 72.5 | 68.7 | 75.3 | 74.8 | 72.8 | 72.0 | 70.2 |
| 2 | 12:36:00 | 72.1 | 65.8 | 75.2 | 74.0 | 72.5 | 71.9 | 69.7 |
| 3 | 12:37:00 | 72.4 | 63.7 | 77.7 | 74.5 | 72.8 | 71.9 | 68.3 |
| 4 | 12:38:00 | 73.4 | 67.3 | 77.4 | 75.6 | 74.0 | 72.9 | 70.2 |
| 5 | 12:39:00 | 72.4 | 66.4 | 75.6 | 74.3 | 73.2 | 72.4 | 67.9 |
| 6 | 12:40:00 | 72.5 | 69.1 | 74.8 | 73.9 | 72.8 | 72.3 | 70.8 |
| 7 | 12:41:00 | 73.4 | 64.2 | 76.2 | 75.6 | 74.1 | 73.2 | 69.9 |
| 8 | 12:42:00 | 72.1 | 65.6 | 76.0 | 74.2 | 72.8 | 72.1 | 68.8 |
| 9 | 12:43:00 | 72.3 | 66.0 | 76.5 | 75.1 | 72.6 | 71.6 | 68.7 |
| 10 | 12:44:00 | 74.0 | 68.9 | 77.9 | 76.3 | 74.5 | 73.5 | 70.4 |
| 11 | 12:45:00 | 72.2 | 64.7 | 74.8 | 73.9 | 72.9 | 72.4 | 68.7 |
| 12 | 12:46:00 | 73.1 | 68.1 | 76.8 | 75.7 | 73.1 | 72.3 | 70.5 |
| 13 | 12:47:00 | 72.3 | 69.3 | 75.2 | 73.6 | 72.9 | 72.4 | 70.3 |
| 14 | 12:48:00 | 72.2 | 65.5 | 75.2 | 74.2 | 72.9 | 71.9 | 68.3 |
| 15 | 12:49:00 | 72.1 | 63.5 | 76.1 | 73.8 | 72.7 | 72.0 | 68.4 |
| 16 | 12:50:00 | 71.6 | 67.0 | 75.1 | 73.0 | 72.2 | 71.4 | 68.8 |
| Total for Period |  | 72.6 | 63.5 | 77.9 | 74.5 | 73.1 | 72.3 | 69.4 |

Harris Miller Miller \& Hanson inc.

PROJECT: K19786:I-205CW
JOB NO.: 309180.000

## SHORT-TERM NOISE MEASUREMENT SITE LOG

| ASSESSMENT AREA: | WEST LINN | MEASUREMENT SITE NO.: | ST-1 |
| :---: | :---: | :---: | :---: |
| ADDRESS: | 1555 SW BORLAND ROAD |  |  |
| OWNER: |  |  |  |
| DESCRIPTION: | CHURCH AND PRESCHOOL |  |  |
| NOISE SOURCES: | I-205 TRAFFIC |  |  |
| NOISE MONITOR: | B\&K 2250 | S/N: | 2579777 |
| MICROPHONE: | B\&K |  |  |
| CALIBRATOR: | B\&K |  |  |
| TEMP. RANGE ( ${ }^{\circ} \mathrm{F}$ ): | 71 | WEATHER CONDITIONS: | SUNNY |



Notes: I-205 dominant. Vehicles are visible in both directions of travel on I-205 from measurement site.


MEASUREMENT SITE NO.: ST-2
PERSONNEL: SRN
ADDRESS/DESCRIPTION: 22400 Johnson Road
DATE: 8/29/17

| $\#$ | Time | $L_{\text {eq }}$ <br> $(d B A)$ | $L_{\text {min }}$ <br> $(d B A)$ | $L_{m a x}$ <br> $(d B A)$ | $L_{10}$ <br> $(d B A)$ | $L_{33}$ <br> $(d B A)$ | $L_{50}$ <br> $(d B A)$ | $L_{90}$ <br> $(d B A)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $13: 24: 00$ | 66.4 | 63.9 | 70.1 | 67.8 | 66.8 | 66.3 | 64.6 |
| 2 | $13: 25: 00$ | 65.4 | 62.5 | 67.4 | 66.7 | 65.8 | 65.4 | 63.7 |
| 3 | $13: 26: 00$ | 65.1 | 62.3 | 67.2 | 66.5 | 65.7 | 65.2 | 63.0 |
| 4 | $13: 27: 00$ | 66.1 | 64.3 | 68.4 | 67.0 | 66.5 | 66.1 | 65.0 |
| 5 | $13: 28: 00$ | 65.8 | 62.5 | 68.6 | 67.2 | 66.2 | 65.7 | 64.1 |
| 6 | $13: 29: 00$ | 65.6 | 62.9 | 67.3 | 66.7 | 65.9 | 65.5 | 64.1 |
| 7 | $13: 30: 00$ | 65.5 | 63.4 | 67.5 | 66.6 | 65.8 | 65.4 | 64.3 |
| 8 | $13: 31: 00$ | 65.4 | 60.9 | 68.1 | 67.1 | 65.9 | 65.2 | 62.8 |
| 9 | $13: 32: 00$ | 65.4 | 63.3 | 67.8 | 66.7 | 65.8 | 65.1 | 63.8 |
| 10 | $13: 33: 00$ | 65.1 | 62.6 | 67.0 | 66.3 | 65.5 | 65.1 | 63.8 |
| 11 | $13: 34: 00$ | 65.3 | 63.6 | 66.9 | 66.1 | 65.6 | 65.3 | 64.3 |
| 12 | $13: 35: 00$ | 65.0 | 62.8 | 67.0 | 65.9 | 65.3 | 64.9 | 63.9 |
| 13 | $13: 36: 00$ | 65.6 | 63.5 | 68.0 | 66.7 | 65.8 | 65.4 | 64.4 |
| 14 | $13: 37: 00$ | 65.1 | 61.6 | 66.9 | 66.0 | 65.6 | 65.3 | 63.3 |
| 15 | $13: 38: 00$ | 65.9 | 63.9 | 68.5 | 67.3 | 66.2 | 65.7 | 64.4 |
| 16 | $13: 39: 00$ | 65.0 | 61.7 | 68.1 | 66.8 | 65.5 | 64.9 | 62.4 |
| 17 | $13: 40: 00$ | 64.8 | 61.1 | 66.7 | 65.9 | 65.3 | 64.9 | 62.9 |
| 18 | $13: 41: 00$ | 64.9 | 62.9 | 67.2 | 66.1 | 65.2 | 64.8 | 63.7 |
| 19 | $13: 42: 00$ | 65.4 | 63.3 | 67.1 | 66.4 | 65.7 | 65.4 | 64.2 |
| 20 | $13: 43: 00$ | 65.2 | 62.1 | 67.0 | 66.3 | 65.6 | 65.2 | 63.6 |
| 21 | $13: 44: 00$ | 65.4 | 62.6 | 67.5 | 66.5 | 65.7 | 65.4 | 64.2 |
| 22 | $13: 45: 00$ | 65.3 | 61.4 | 67.5 | 66.7 | 65.7 | 65.2 | 63.4 |
| 23 | $13: 46: 00$ | 65.6 | 63.9 | 67.8 | 66.7 | 65.8 | 65.4 | 64.3 |
| 24 | $13: 47: 00$ | 65.1 | 62.2 | 68.4 | 66.8 | 65.5 | 64.8 | 63.3 |
| 25 | $13: 48: 00$ | 64.9 | 62.4 | 67.5 | 66.1 | 65.2 | 64.7 | 63.5 |
| 26 | $13: 49: 00$ | 64.7 | 59.7 | 66.9 | 66.0 | 65.4 | 65.0 | 62.0 |
| 27 | $13: 50: 00$ | 65.0 | 62.5 | 66.5 | 65.8 | 65.4 | 65.0 | 63.7 |
| 28 | $13: 51: 00$ | 65.6 | 63.3 | 67.4 | 66.6 | 65.9 | 65.5 | 64.4 |
| 29 | $13: 52: 00$ | 65.7 | 63.3 | 68.0 | 66.9 | 66.1 | 65.6 | 64.3 |
| Total $70 r ~ P e r i o d$ | 64.5 | 59.7 | 70.1 | 66.6 | 65.8 | 65.3 | 63.8 |  |

Harris Miller Miller \& Hanson inc.

PROJECT: K19786:I-205CW
JOB NO.: 309180.000

## SHORT-TERM NOISE MEASUREMENT SITE LOG

| ASSESSMENT AREA: | WEST LINN | MEASUREMENT SITE NO.: ST-2 |  |
| :---: | :---: | :---: | :---: |
| ADDRESS: | 22400 JOHNSON ROAD |  |  |
| OWNER: |  |  |  |
| DESCRIPTION: | SINGLE-FAMILY RESIDENTIAL |  |  |
| NOISE SOURCES: | I-205 TRAFFIC |  |  |
| NOISE MONITOR: | LD 824 | S/N: | A3975 |
| MICROPHONE: | GRAS |  |  |
| CALIBRATOR: | CAL200 |  |  |
| TEMP. RANGE ( ${ }^{\circ} \mathrm{F}$ ): | 61 | WEATHER CONDITIONS: | SMOKEY |

SITE MAP:


Notes: Johnson Road is elevated above receptors by 25-30 feet as it approaches overcrossing of I-205.


## SHORT-TERM NOISE MEASUREMENT DATA SHEET

PROJECT: K19786:I-205CW
JOB NO.: 309180.000
MEASUREMENT SITE NO.: ST-3
PERSONNEL: SRN
ADDRESS/DESCRIPTION: 22501 S. Grapevine Road
DATE: 8/30/17

| \# | Time | $\begin{gathered} \hline \mathrm{L}_{\text {eq }} \\ (\mathrm{dBA}) \end{gathered}$ | $\begin{gathered} L_{\text {min }} \\ (\mathrm{dBA}) \end{gathered}$ | $\begin{aligned} & \mathrm{L}_{\max } \\ & (\mathrm{dBA}) \end{aligned}$ | $\begin{gathered} \mathrm{L}_{10} \\ (\mathrm{dBA}) \end{gathered}$ | $\begin{gathered} \mathrm{L}_{33} \\ (\mathrm{dBA}) \end{gathered}$ | $\begin{gathered} \mathrm{L}_{50} \\ (\mathrm{dBA}) \end{gathered}$ | $\begin{gathered} \mathrm{L}_{90} \\ (\mathrm{dBA}) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 9:38:07 | 62.5 | 60.6 | 64.4 | 63.7 | 63.0 | 62.5 | 61.3 |
| 2 | 9:39:07 | 62.1 | 60.1 | 65.3 | 63.3 | 62.5 | 62.0 | 61.1 |
| 3 | 9:40:07 | 63.1 | 61.3 | 65.2 | 64.0 | 63.4 | 63.0 | 62.2 |
| 4 | 9:41:07 | 62.5 | 60.4 | 67.1 | 63.6 | 62.7 | 62.3 | 61.3 |
| 5 | 9:42:07 | 62.6 | 60.7 | 64.1 | 63.7 | 63.0 | 62.6 | 61.4 |
| 6 | 9:43:07 | 62.8 | 60.5 | 65.2 | 63.9 | 63.1 | 62.7 | 61.4 |
| 7 | 9:44:07 | 61.9 | 60.0 | 63.9 | 63.0 | 62.3 | 61.8 | 60.4 |
| 8 | 9:45:07 | 62.7 | 61.2 | 66.6 | 63.8 | 62.8 | 62.4 | 61.4 |
| 9 | 9:46:07 | 62.9 | 61.5 | 64.6 | 63.8 | 63.2 | 62.8 | 62.1 |
| 10 | 9:47:07 | 63.2 | 61.7 | 65.5 | 64.2 | 63.6 | 63.2 | 62.2 |
| 11 | 9:48:07 | 64.5 | 61 | 70.6 | 67.0 | 64.3 | 63.6 | 62.2 |
| 12 | 9:49:07 | 63.0 | 61.3 | 67.3 | 63.9 | 62.9 | 62.6 | 62.0 |
| 13 | 9:50:07 | 62.9 | 60.9 | 65.9 | 64.0 | 62.9 | 62.6 | 61.7 |
| 14 | 9:51:07 | 65.1 | 61.1 | 74.0 | 68.8 | 63.6 | 62.7 | 61.4 |
| 15 | 9:52:07 | 63.1 | 61.1 | 67.7 | 64.9 | 63.0 | 62.6 | 61.6 |
| Total for Period |  | 63.1 | 60.0 | 74.0 | 64.4 | 63.1 | 62.6 | 61.6 |

PROJECT: K19786:I-205CW
JOB NO.: 309180.000

## SHORT-TERM NOISE MEASUREMENT SITE LOG

| ASSESSMENT AREA: | WEST LINN | MEASUREMENT SITE NO.: | ST-3 |
| :---: | :---: | :---: | :---: |
| ADDRESS: | 22501 S. GRAPEVINE ROAD |  |  |
| OWNER: |  |  |  |
| DESCRIPTION: | SINGLE-FAMILY RESIDENTIAL |  |  |
| NOISE SOURCES: | I-205 TRAFFIC |  |  |
| NOISE MONITOR: | LD 824 |  | A3975 |
| MICROPHONE: | GRAS |  |  |
| CALIBRATOR: | CAL200 |  |  |
| TEMP. RANGE ( ${ }^{\circ} \mathrm{F}$ ): | 61 | WEATHER CONDITIONS: | CLOUDY |

SITE MAP:


Notes: I-205 dominant. Grapevine Road proceeds south of site to pass under I-205.


## SHORT-TERM NOISE MEASUREMENT DATA SHEET

PROJECT: K19786:I-205CW
JOB NO.: 309180.000
MEASUREMENT SITE NO.: ST-4
PERSONNEL: SRN
ADDRESS/DESCRIPTION: 23400 Johnson Road
DATE: 8/30/17

| $\#$ | Time | $L_{\text {eq }}$ <br> $(d B A)$ | $L_{\text {min }}$ <br> $(d B A)$ | $L_{\text {max }}$ <br> $(d B A)$ | $L_{10}$ <br> $(d B A)$ | $L_{33}$ <br> $(d B A)$ | $L_{50}$ <br> $(d B A)$ | $L_{90}$ <br> $(d B A)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $10: 16: 00$ | 64.7 | 62 | 75.4 | 65.9 | 64.7 | 64.0 | 63.0 |
| 2 | $10: 17: 00$ | 64.5 | 61 | 67.6 | 66.1 | 64.8 | 64.3 | 62.5 |
| 3 | $10: 18: 00$ | 64.2 | 60.5 | 66.3 | 65.4 | 64.6 | 64.2 | 62.5 |
| 4 | $10: 19: 00$ | 64.6 | 57.7 | 69.4 | 66.2 | 65.2 | 64.6 | 61.1 |
| 5 | $10: 20: 00$ | 63.2 | 58.4 | 65.7 | 64.7 | 63.8 | 63.3 | 60.3 |
| 6 | $10: 21: 00$ | 63.5 | 59.8 | 66.3 | 65.4 | 64.2 | 63.0 | 61.1 |
| 7 | $10: 22: 00$ | 63.5 | 56 | 66.8 | 65.0 | 64.4 | 63.8 | 57.5 |
| 8 | $10: 23: 00$ | 63.6 | 58.8 | 65.9 | 65.3 | 64.2 | 63.4 | 61.2 |
| 9 | $10: 24: 00$ | 63.8 | 59.8 | 66.5 | 65.3 | 64.3 | 63.8 | 62.1 |
| 10 | $10: 25: 00$ | 63.8 | 60.7 | 66.9 | 65.5 | 64.2 | 63.6 | 62.0 |
| 11 | $10: 26: 00$ | 63.3 | 55.1 | 66.1 | 64.9 | 64.2 | 63.4 | 60.3 |
| 12 | $10: 27: 00$ | 64.4 | 54.5 | 69.1 | 67.2 | 64.8 | 64.2 | 57.0 |
| 13 | $10: 28: 00$ | 63.8 | 61.3 | 66.2 | 64.9 | 64.2 | 63.7 | 62.2 |
| 14 | $10: 29: 00$ | 64.1 | 57.1 | 71.6 | 65.9 | 64.3 | 63.5 | 59.6 |
| 15 | $10: 30: 00$ | 63.8 | 60.1 | 67.7 | 66.0 | 64.4 | 63.4 | 61.2 |
| Total $\boldsymbol{f o r}$ Period | 63.9 | 54.5 | 75.4 | 65.6 | 64.4 | 63.8 | 60.9 |  |

PROJECT: K19786:I-205CW
JOB NO.: 309180.000

## SHORT-TERM NOISE MEASUREMENT SITE LOG

| ASSESSMENT AREA: | WEST LINN | MEASUREMENT SITE NO.: | ST-4 |
| :---: | :---: | :---: | :---: |
| ADDRESS: | 23400 JOHNSON ROAD |  |  |
| OWNER: |  |  |  |
| DESCRIPTION: | SINGLE-FAMILY RESIDENTIAL |  |  |
| NOISE SOURCES: | I-205 TRAFFIC |  |  |
| NOISE MONITOR: | LD 824 | S/N: | A3975 |
| MICROPHONE: | GRAS |  |  |
| CALIBRATOR: | CAL200 |  |  |
| TEMP. RANGE ( ${ }^{\circ} \mathrm{F}$ ): | 63 | WEATHER CONDITIONS: | CLOUDY |

SITE MAP:


Notes: I-205 dominant. Vehicles are visible in both directions of travel on I-205 from measurement site.


## SHORT-TERM NOISE MEASUREMENT DATA SHEET

PROJECT: K19786:I-205CW
JOB NO.:

$$
309180.000
$$

MEASUREMENT SITE NO.: ST-5a
PERSONNEL: SRN
ADDRESS/DESCRIPTION: 2384 Margery Street
DATE: 8/30/17

| $\#$ | Time | $L_{e q}$ <br> $(d B A)$ | $L_{\text {min }}$ <br> $(d B A)$ | $L_{\text {max }}$ <br> $(d B A)$ | $L_{10}$ <br> $(d B A)$ | $L_{33}$ <br> $(d B A)$ | $L_{50}$ <br> $(d B A)$ | $L_{90}$ <br> $(d B A)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $10: 49: 04$ | 67.3 | 63.2 | 69.9 | 68.8 | 68.1 | 67.4 | 64.4 |
| 2 | $10: 50: 04$ | 68 | 63.6 | 70.5 | 69.5 | 68.6 | 68.2 | 65.1 |
| 3 | $10: 51: 04$ | 69.2 | 66.1 | 75.6 | 71.1 | 69.4 | 68.5 | 66.8 |
| 4 | $10: 52: 04$ | 69 | 64.9 | 73.4 | 70.6 | 69.4 | 68.8 | 66.6 |
| 5 | $10: 53: 04$ | 69.9 | 66.2 | 76 | 72.0 | 69.9 | 69.0 | 67.3 |
| 6 | $10: 54: 04$ | 69.9 | 65.3 | 72.9 | 71.4 | 70.4 | 69.9 | 67.6 |
| 7 | $10: 55: 04$ | 69.9 | 66.2 | 76.1 | 71.6 | 70.2 | 69.6 | 67.7 |
| 8 | $10: 56: 04$ | 68.8 | 65.7 | 71.6 | 69.9 | 69.0 | 68.6 | 67.3 |
| 9 | $10: 57: 04$ | 69.6 | 66.3 | 72.8 | 71.1 | 70.1 | 69.3 | 67.6 |
| 10 | $10: 58: 04$ | 70 | 67.9 | 72.5 | 71.1 | 70.4 | 69.9 | 68.6 |
| 11 | $10: 59: 04$ | 69.4 | 66.3 | 73.7 | 71.1 | 69.6 | 69.0 | 67.5 |
| 12 | $11: 00: 04$ | 69.1 | 66.4 | 71.6 | 70.5 | 69.5 | 69.0 | 67.6 |
| 13 | $11: 01: 04$ | 69.9 | 67.3 | 74.3 | 71.4 | 70.2 | 69.5 | 68.1 |
| 14 | $11: 02: 04$ | 70.2 | 67.1 | 75.8 | 72.3 | 69.9 | 69.4 | 68.0 |
| 15 | $11: 03: 04$ | 69.4 | 64.6 | 73.3 | 71.3 | 70.0 | 69.3 | 66.0 |
| 16 | $11: 04: 04$ | 70 | 65.2 | 73.8 | 71.5 | 70.4 | 69.9 | 68.0 |
| Total for Period | 69.4 | 63.2 | 76.1 | 71.0 | 69.7 | 69.1 | 67.1 |  |

PROJECT: K19786:I-205CW
JOB NO.: 309180.000

## SHORT-TERM NOISE MEASUREMENT SITE LOG

| ASSESSMENT AREA: | WEST LINN | MEASUREMENT SITE NO.: | ST-5A |
| :---: | :---: | :---: | :---: |
| ADDRESS: | 2384 MARGERY STREET |  |  |
| OWNER: |  |  |  |
| DESCRIPTION: | SINGLE-FAMILY RESIDENTIAL |  |  |
| NOISE SOURCES: | I-205 TRAFFIC |  |  |
| NOISE MONITOR: | LD 824 | S/N: | A3975 |
| MICROPHONE: | GRAS |  |  |
| CALIBRATOR: | CAL200 |  |  |
| TEMP. RANGE ( ${ }^{\circ} \mathrm{F}$ ): | 63 | WEATHER CONDITIONS: | PARTLY CLOUDY |



Notes: I-205 dominant.


## SHORT-TERM NOISE MEASUREMENT DATA SHEET

PROJECT: K19786:I-205CW
JOB NO.: 309180.000
MEASUREMENT SITE NO.: ST-5b
PERSONNEL: SRN
ADDRESS/DESCRIPTION: 2383 Margery Street
DATE: 8/30/17

| \# | Time | $\begin{gathered} \hline \mathrm{L}_{\mathrm{eq}} \\ (\mathrm{dBA}) \end{gathered}$ | $\begin{gathered} \mathrm{L}_{\text {min }} \\ (\mathrm{dBA}) \end{gathered}$ | $\begin{gathered} \hline \mathrm{L}_{\max } \\ (\mathrm{dBA}) \end{gathered}$ | $\begin{gathered} \mathrm{L}_{10} \\ (\mathrm{dBA}) \end{gathered}$ | $\begin{gathered} \mathrm{L}_{33} \\ (\mathrm{dBA}) \end{gathered}$ | $\begin{gathered} \mathrm{L}_{50} \\ (\mathrm{dBA}) \end{gathered}$ | $\begin{gathered} \mathrm{L}_{90} \\ (\mathrm{dBA}) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 11:06:40 | 64.3 | 60.8 | 66.5 | 65.5 | 64.7 | 64.3 | 62.5 |
| 2 | 11:07:40 | 64.6 | 62 | 67.5 | 66.0 | 64.9 | 64.5 | 63.1 |
| 3 | 11:08:40 | 65 | 62.8 | 68.4 | 66.0 | 65.2 | 64.7 | 63.6 |
| 4 | 11:09:40 | 65.2 | 63.3 | 68.9 | 66.4 | 65.5 | 65.1 | 64.0 |
| 5 | 11:10:40 | 65.4 | 62.9 | 68.5 | 66.7 | 65.7 | 65.2 | 63.9 |
| 6 | 11:11:40 | 64.9 | 61.4 | 67.6 | 66.6 | 65.6 | 64.7 | 62.5 |
| 7 | 11:12:40 | 65.1 | 61.6 | 68.4 | 66.7 | 65.5 | 64.8 | 63.1 |
| 8 | 11:13:40 | 65 | 63 | 67.3 | 66.1 | 65.4 | 64.9 | 63.6 |
| 9 | 11:14:40 | 65.5 | 63 | 70.2 | 66.6 | 65.7 | 65.3 | 64.0 |
| 10 | 11:15:40 | 64.7 | 61.7 | 66.7 | 65.9 | 65.2 | 64.8 | 62.7 |
| 11 | 11:16:40 | 65.3 | 63 | 67.7 | 66.5 | 65.7 | 65.3 | 63.8 |
| 12 | 11:17:40 | 63.9 | 61 | 66.2 | 65.0 | 64.5 | 64.1 | 62.2 |
| 13 | 11:18:40 | 64.7 | 61.6 | 68.8 | 66.1 | 65.0 | 64.4 | 62.5 |
| 14 | 11:19:40 | 65 | 62.4 | 68.2 | 67.0 | 65.0 | 64.5 | 63.1 |
| 15 | 11:20:40 | 64.7 | 60.5 | 67.3 | 66.0 | 65.4 | 64.9 | 62.4 |
| Total for Period |  | 64.9 | 60.5 | 70.2 | 66.2 | 65.3 | 64.8 | 63.1 |

PROJECT: K19786:I-205CW
JOB NO.: 309180.000

## SHORT-TERM NOISE MEASUREMENT SITE LOG

| ASSESSMENT AREA: | WEST LINN | MEASUREMENT SITE NO.: | ST-5B |
| :---: | :---: | :---: | :---: |
| ADDRESS: | 2383 MARGERY STREET |  |  |
| OWNER: |  |  |  |
| DESCRIPTION: | SINGLE-FAMILY RESIDENTIAL |  |  |
| NOISE SOURCES: | I-205 TRAFFIC |  |  |
| NOISE MONITOR: | LD 824 | S/N: | A3975 |
| MICROPHONE: | GRAS |  |  |
| CALIBRATOR: | CAL200 |  |  |
| TEMP. RANGE ( ${ }^{\circ} \mathrm{F}$ ): | 63 | WEATHER CONDITIONS: | PARTLY CLOUDY |



Notes: I-205 dominant.


PROJECT: K19786:I-205CW
JOB NO.: 309180.000

MEASUREMENT SITE NO.: ST-6
ADDRESS/DESCRIPTION: 1709 Blankenship Rd
PERSONNEL: SRN

| $\#$ | Time | $L_{\text {eq }}$ <br> $(d B A)$ | $L_{\text {min }}$ <br> $(d B A)$ | $L_{\text {max }}$ <br> $(d B A)$ | $L_{10}$ <br> $(d B A)$ | $L_{33}$ <br> $(d B A)$ | $L_{50}$ <br> $(d B A)$ | $L_{90}$ <br> $(d B A)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $12: 36: 36$ | 56.5 | 55.3 | 61.8 | 57.1 | 56.7 | 56.4 | 55.5 |
| 2 | $12: 37: 36$ | 57.2 | 55.6 | 60.2 | 58.0 | 57.5 | 57.2 | 56.2 |
| 3 | $12: 38: 36$ | 58.1 | 55.7 | 67.5 | 58.9 | 57.8 | 57.4 | 56.3 |
| 4 | $12: 39: 36$ | 57.2 | 55.1 | 60.1 | 58.2 | 57.5 | 57.0 | 56.1 |
| 5 | $12: 40: 36$ | 57.7 | 54.1 | 60.3 | 59.0 | 58.0 | 57.6 | 55.5 |
| 6 | $12: 41: 36$ | 59.4 | 54.8 | 66.6 | 60.9 | 59.8 | 59.2 | 55.8 |
| 7 | $12: 42: 36$ | 58.3 | 56.2 | 60.2 | 59.5 | 58.7 | 58.3 | 57.1 |
| 8 | $12: 43: 36$ | 57.6 | 54.7 | 62.3 | 60.1 | 57.5 | 56.9 | 55.4 |
| 9 | $12: 44: 36$ | 56.2 | 54 | 60.6 | 57.8 | 56.4 | 55.8 | 54.5 |
| 10 | $12: 45: 36$ | 55.5 | 53.6 | 57.6 | 56.7 | 55.8 | 55.3 | 54.2 |
| 11 | $12: 46: 36$ | 56.6 | 55.4 | 58.1 | 57.6 | 56.9 | 56.6 | 55.9 |
| 12 | $12: 47: 36$ | 56.8 | 52.3 | 60.5 | 58.8 | 57.6 | 56.9 | 53.1 |
| 13 | $12: 48: 36$ | 58.1 | 54.9 | 64.9 | 60.5 | 57.5 | 57.0 | 56.1 |
| 14 | $12: 49: 36$ | 57.4 | 54.5 | 60.1 | 58.5 | 57.7 | 57.4 | 56.0 |
| 15 | $12: 50: 36$ | 58.7 | 56.9 | 63.3 | 59.9 | 59.0 | 58.4 | 57.3 |
| 16 | $12: 51: 36$ | 59.6 | 57.3 | 62.2 | 60.8 | 59.8 | 59.5 | 58.2 |
| 17 | $12: 52: 36$ | 59.6 | 57.8 | 61.8 | 60.6 | 59.9 | 59.6 | 58.5 |
| 18 | $12: 53: 36$ | 58.2 | 55.9 | 60.5 | 59.7 | 58.8 | 58.0 | 56.4 |
| 19 | $12: 54: 36$ | 59.4 | 56.4 | 62.0 | 60.9 | 60.0 | 59.2 | 57.4 |
| 20 | $12: 55: 36$ | 58.4 | 55.5 | 60.5 | 59.5 | 58.7 | 58.3 | 56.8 |
| 21 | $12: 56: 36$ | 58.0 | 54.6 | 63.0 | 59.7 | 58.4 | 57.8 | 56.0 |
| 22 | $12: 57: 36$ | 58.2 | 56.7 | 60.1 | 58.9 | 58.5 | 58.2 | 57.2 |
| 23 | $12: 58: 36$ | 58.1 | 54.5 | 60.9 | 59.6 | 58.8 | 58.1 | 56.1 |
| 24 | $12: 59: 36$ | 55.8 | 53.8 | 57.7 | 56.8 | 56.1 | 55.7 | 54.6 |
| 25 | $13: 00: 36$ | 61.0 | 54.7 | 72.9 | 62.3 | 57.3 | 56.7 | 55.3 |
| 26 | $13: 01: 36$ | 55.5 | 53.4 | 57.6 | 56.9 | 55.9 | 55.4 | 54.1 |
| Total $f 0 r ~ P e r i o d$ | 58.0 | 52.3 | 72.9 | 59.1 | 57.9 | 57.5 | 56.0 |  |

PROJECT: K19786:I-205CW
JOB NO.: 309180.000

## SHORT-TERM NOISE MEASUREMENT SITE LOG

| ASSESSMENT AREA: | WEST LINN | MEASUREMENT SITE NO.: ST-6 |
| :---: | :---: | :---: |
| ADDRESS: | 1709 BLANKENSHIP RD (WILLAMETTE TERRACE APTS) |  |
| OWNER: |  |  |
| DESCRIPTION: | MULITI-FAMILY RESIDENTIAL (76 TOTAL UNITS) |  |
| NOISE SOURCES: | I-205 TRAFFIC, ENGINE BREAKING ON I-205 |  |
| NOISE MONITOR: | LD 824 | S/N: A3975 |
| MICROPHONE: | GRAS |  |
| CALIBRATOR: | CAL200 |  |
| TEMP. RANGE ( ${ }^{\circ} \mathrm{F}$ ): | 67 | WEATHER CONDITIONS: SUNNY |

SITE MAP:


Notes: I-205 dominant. Interstate is elevated above the apartments by approximately 25 feet as it crosses over Blankenship Road.


## SHORT-TERM NOISE MEASUREMENT DATA SHEET

PROJECT: K19786:I-205CW
JOB NO.: 309180.000
MEASUREMENT SITE NO.: ST-7
PERSONNEL: SRN
ADDRESS/DESCRIPTION: 1788 Jamie Circle
DATE: 8/30/17

| \# | Time | $\begin{gathered} \hline \mathrm{L}_{\text {eq }} \\ (\mathrm{dBA}) \end{gathered}$ | $\begin{gathered} \mathrm{L}_{\text {min }} \\ (\mathrm{dBA}) \end{gathered}$ | $\begin{gathered} \mathrm{L}_{\max } \\ (\mathrm{dBA}) \end{gathered}$ | $\begin{gathered} \mathrm{L}_{10} \\ (\mathrm{dBA}) \end{gathered}$ | $\begin{gathered} \hline \mathrm{L}_{33} \\ (\mathrm{dBA}) \end{gathered}$ | $\begin{gathered} \hline \mathrm{L}_{50} \\ (\mathrm{dBA}) \end{gathered}$ | $\begin{gathered} \mathrm{L}_{90} \\ (\mathrm{dBA}) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 15:06:14 | 59.8 | 56.8 | 65.4 | 61.2 | 59.8 | 59.3 | 57.6 |
| 2 | 15:07:14 | 58.6 | 54.7 | 65.5 | 62.1 | 57.8 | 56.9 | 55.3 |
| 3 | 15:08:14 | 55.4 | 52.6 | 59.6 | 56.8 | 55.9 | 55.3 | 53.5 |
| 4 | 15:09:14 | 56.1 | 52.9 | 60.0 | 58.2 | 56.4 | 55.8 | 53.9 |
| 5 | 15:10:14 | 57.9 | 55.5 | 60.8 | 59.3 | 58.3 | 57.7 | 56.2 |
| 6 | 15:11:14 | 58.5 | 56.4 | 61.0 | 59.7 | 58.8 | 58.4 | 57.2 |
| 7 | 15:12:14 | 58.3 | 55.4 | 63.3 | 59.6 | 58.7 | 58.2 | 56.5 |
| 8 | 15:13:14 | 57.5 | 54.3 | 61.0 | 59.2 | 57.8 | 57.1 | 55.4 |
| 9 | 15:14:14 | 58.8 | 56.2 | 61.8 | 60.4 | 59.2 | 58.5 | 57.1 |
| 10 | 15:15:14 | 57.8 | 53.9 | 63.3 | 59.9 | 57.8 | 57.1 | 54.8 |
| 11 | 15:16:14 | 55.8 | 52.6 | 62.0 | 57.3 | 56.1 | 55.4 | 53.5 |
| 12 | 15:17:14 | 56.6 | 54.3 | 60.8 | 58.5 | 57.1 | 56.0 | 54.4 |
| 13 | 15:18:14 | 58.4 | 54.9 | 61.4 | 60.1 | 58.8 | 58.3 | 56.0 |
| 14 | 15:19:14 | 59.2 | 57.2 | 61.9 | 60.5 | 59.6 | 59.0 | 57.8 |
| 15 | 15:20:14 | 59.9 | 57.5 | 63.3 | 61.6 | 60.1 | 59.5 | 58.2 |
| Total for Period |  | 58.1 | 52.6 | 65.5 | 59.1 | 57.9 | 57.5 | 56.0 |

Harris Miller Miller \& Hanson inc.

PROJECT: K19786:I-205CW
JOB NO.: 309180.000

## SHORT-TERM NOISE MEASUREMENT SITE LOG

| ASSESSMENT AREA: | WEST LINN | MEASUREMENT SITE NO.: | ST-7 |
| :---: | :---: | :---: | :---: |
| ADDRESS: | 1788 JAMIE CIRCLE |  |  |
| OWNER: |  |  |  |
| DESCRIPTION: | SINGLE-FAMILY RESIDENTIAL |  |  |
| NOISE SOURCES: | I-205 TRAFFIC, ENGINE BREAKING ON I-205 |  |  |
| NOISE MONITOR: | LD 824 | S/N: | A3975 |
| MICROPHONE: | GRAS |  |  |
| CALIBRATOR: | CAL200 |  |  |
| TEMP. RANGE ( ${ }^{\circ} \mathrm{F}$ ): | 75 | WEATHER CONDITIONS: | SUNNY |

SITE MAP:


Notes: I-205 dominant. Interstate is elevated above the single family home by approximately 10.


MEASUREMENT SITE NO.: ST-8
PERSONNEL: SRN
ADDRESS/DESCRIPTION: $23188^{\text {th }}$ Street
DATE: 8/31/17

| $\#$ | Time | $L_{e q}$ <br> $(d B A)$ | $L_{\text {min }}$ <br> $(d B A)$ | $L_{\text {max }}$ <br> $(d B A)$ | $L_{10}$ <br> $(d B A)$ | $L_{33}$ <br> $(d B A)$ | $L_{50}$ <br> $(d B A)$ | $L_{90}$ <br> $(d B A)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $9: 38: 10$ | 63.5 | 58.8 | 68.3 | 65.8 | 63.9 | 63.1 | 60.3 |
| 2 | $9: 39: 10$ | 63.6 | 60.9 | 66.1 | 65.0 | 64.3 | 63.6 | 61.5 |
| 3 | $9: 40: 10$ | 62.9 | 59.1 | 71 | 64.6 | 63.2 | 62.5 | 60.2 |
| 4 | $9: 41: 10$ | 63.9 | 60.7 | 69.6 | 65.8 | 64.0 | 63.3 | 61.7 |
| 5 | $9: 42: 10$ | 62.8 | 59.8 | 66.6 | 64.6 | 63.2 | 62.6 | 60.6 |
| 6 | $9: 43: 10$ | 64.8 | 59.9 | 67.6 | 66.5 | 65.4 | 64.7 | 62.3 |
| 7 | $9: 44: 10$ | 64 | 60.8 | 68.3 | 65.9 | 64.5 | 63.6 | 61.6 |
| 8 | $9: 45: 10$ | 63.1 | 59.8 | 67.4 | 65.5 | 63.0 | 62.3 | 60.9 |
| 9 | $9: 46: 10$ | 62.1 | 55.2 | 66.4 | 64.9 | 63.1 | 61.6 | 57.1 |
| 10 | $9: 47: 10$ | 63.5 | 61 | 74 | 64.8 | 63.7 | 63.1 | 62.0 |
| 11 | $9: 48: 10$ | 63.8 | 59.2 | 66.9 | 65.5 | 64.4 | 63.7 | 61.3 |
| 12 | $9: 49: 10$ | 62.6 | 59.1 | 65.6 | 64.6 | 63.1 | 62.3 | 59.8 |
| 13 | $9: 50: 10$ | 62.9 | 58.7 | 66.7 | 65.2 | 63.6 | 62.4 | 59.8 |
| 14 | $9: 51: 10$ | 63.8 | 59.7 | 68.3 | 66.4 | 63.8 | 63.1 | 61.2 |
| 15 | $9: 52: 10$ | 62.2 | 57.3 | 68.9 | 64.7 | 62.7 | 61.6 | 58.8 |
| 16 | $9: 53: 10$ | 64.3 | 59.5 | 69.1 | 66.4 | 64.9 | 64.1 | 60.9 |
| 17 | $9: 54: 10$ | 62.4 | 58.7 | 65.5 | 63.9 | 63.0 | 62.5 | 59.8 |
| 18 | $9: 55: 10$ | 62.3 | 57.5 | 66.1 | 63.9 | 62.8 | 62.1 | 59.7 |
| 19 | $9: 56: 10$ | 62.5 | 59.4 | 66.7 | 64.0 | 62.9 | 62.4 | 60.5 |
| 20 | $9: 57: 10$ | 61.5 | 58.6 | 64.6 | 63.0 | 61.9 | 61.3 | 59.6 |
| Total for Period | 63.2 | 55.2 | 64.6 | 65.1 | 63.6 | 62.8 | 60.5 |  |

PROJECT: K19786:I-205CW
JOB NO.: 309180.000

## SHORT-TERM NOISE MEASUREMENT SITE LOG

| ASSESSMENT AREA: | WEST LINN | MEASUREMENT SITE NO.: ST-8 |
| :---: | :---: | :---: |
| ADDRESS: | $23188^{\text {TH }}$ STREET |  |
| OWNER: |  |  |
| DESCRIPTION: | SINGLE-FAMILY RESIDENTIAL |  |
| NOISE SOURCES: | I-205 TRAFFIC, ENGINE BREAKING ON I-205 |  |
| NOISE MONITOR: | LD 824 | S/N: A3975 |
| MICROPHONE: | GRAS |  |
| CALIBRATOR: | CAL200 |  |
| TEMP. RANGE ( ${ }^{\circ} \mathrm{F}$ ): | 61 | WEATHER CONDITIONS: SUNNY |

SITE MAP:


Notes: I-205 is audible and dominates; however traffic on Willamette Falls Drive, while lower traffic volumes, is louder when present.


Harris Miller Miller \& Hanson inc.

PROJECT: K19786:I-205CW
JOB NO.: 309180.000
MEASUREMENT SITE NO.: ST-9
PERSONNEL: SRN
ADDRESS/DESCRIPTION: 4107 Imperial Drive
DATE: 8/31/17

| $\#$ | Time | $L_{\text {eq }}$ <br> $(d B A)$ | $L_{\text {min }}$ <br> $(d B A)$ | $L_{\text {max }}$ <br> $(d B A)$ | $L_{10}$ <br> $(d B A)$ | $L_{33}$ <br> $(d B A)$ | $L_{50}$ <br> $(d B A)$ | $L_{90}$ <br> $(d B A)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $10: 25: 06$ | 55.5 | 53.7 | 57.5 | 56.5 | 55.7 | 55.4 | 54.3 |
| 2 | $10: 26: 06$ | 55.2 | 53.8 | 59.2 | 56.0 | 55.4 | 55.0 | 54.2 |
| 3 | $10: 27: 06$ | 54.8 | 52.6 | 57.9 | 56.0 | 55.1 | 54.7 | 53.4 |
| 4 | $10: 28: 06$ | 54.6 | 52.3 | 59.1 | 56.3 | 55.1 | 54.3 | 53.0 |
| 5 | $10: 29: 06$ | 55.5 | 52.5 | 65.0 | 56.3 | 55.0 | 54.6 | 53.3 |
| 6 | $10: 30: 06$ | 55.8 | 52.9 | 62.1 | 56.9 | 55.8 | 55.3 | 54.0 |
| 7 | $10: 31: 06$ | 56.8 | 54.1 | 67.3 | 58.4 | 55.8 | 55.5 | 54.4 |
| 8 | $10: 32: 06$ | 55.9 | 53.0 | 64.0 | 56.8 | 56.2 | 55.8 | 54.4 |
| 9 | $10: 33: 06$ | 54.9 | 53.2 | 58.2 | 55.9 | 54.9 | 54.6 | 53.8 |
| 10 | $10: 34: 06$ | 55.2 | 53.4 | 58.9 | 56.9 | 55.3 | 54.7 | 53.7 |
| 11 | $10: 35: 06$ | 54.1 | 51.9 | 58.6 | 55.0 | 54.4 | 53.9 | 53.0 |
| 12 | $10: 36: 06$ | 56.8 | 53.4 | 61.9 | 58.6 | 57.3 | 56.6 | 54.3 |
| 13 | $10: 37: 06$ | 56.7 | 54.7 | 61.0 | 57.9 | 57.0 | 56.5 | 55.3 |
| 14 | $10: 38: 06$ | 58.4 | 54.8 | 64.0 | 61.5 | 58.2 | 57.4 | 55.5 |
| 15 | $10: 39: 06$ | 57.5 | 55.5 | 63.1 | 58.4 | 57.7 | 57.4 | 56.3 |
| 16 | $10: 40: 06$ | 56.6 | 55.4 | 58.5 | 57.5 | 56.8 | 56.5 | 55.8 |
| Total for Period | 56.0 | 51.9 | $\mathbf{6 7 . 3}$ | 57.2 | 56.0 | 55.5 | 54.3 |  |

PROJECT: K19786:I-205CW
JOB NO.: 309180.000

## SHORT-TERM NOISE MEASUREMENT SITE LOG

| ASSESSMENT AREA: | WEST LINN | MEASUREMENT SITE NO.: | ST-9 |
| :---: | :---: | :---: | :---: |
| ADDRESS: | 4701 IMPERIAL DRIVE |  |  |
| OWNER: |  |  |  |
| DESCRIPTION: | SINGLE-FAMILY RESIDENTIAL |  |  |
| NOISE SOURCES: | I-205 TRAFFIC |  |  |
| NOISE MONITOR: | LD 824 | S/N: | A3975 |
| MICROPHONE: | GRAS |  |  |
| CALIBRATOR: | CAL200 |  |  |
| TEMP. RANGE ( $\left.{ }^{\circ} \mathrm{F}\right)$ : | 68 | WEATHER CONDITIONS: | SUNNY |

SITE MAP:


Notes: I-205 dominates; however, sound of water flowing in Tanner Creek also audible. I-205 is approximately at grade with receptor.


PROJECT: K19786:I-205CW
JOB NO.: 309180.000
MEASUREMENT SITE NO.: ST-10
PERSONNEL: SRN
ADDRESS/DESCRIPTION: 4329 Imperial Drive
DATE: 8/30/17

| $\#$ | Time | $L_{e q}$ <br> $(d B A)$ | $L_{\text {min }}$ <br> $(d B A)$ | $L_{\text {max }}$ <br> $(d B A)$ | $L_{10}$ <br> $(d B A)$ | $L_{33}$ <br> $(d B A)$ | $L_{50}$ <br> $(d B A)$ | $L_{90}$ <br> $(d B A)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $14: 35: 00$ | 59.2 | 57.9 | 60.7 | 60.0 | 59.4 | 58.9 | 58.4 |
| 2 | $14: 36: 00$ | 59.1 | 57.7 | 60.7 | 60.0 | 59.5 | 58.9 | 58.2 |
| 3 | $14: 37: 00$ | 59.5 | 58.0 | 65.0 | 60.1 | 59.5 | 59.1 | 58.3 |
| 4 | $14: 38: 00$ | 58.8 | 57.0 | 60.9 | 60.2 | 58.8 | 58.6 | 57.8 |
| 5 | $14: 39: 00$ | 58.3 | 57.2 | 59.6 | 59.0 | 58.5 | 58.3 | 57.6 |
| 6 | $14: 40: 00$ | 57.7 | 56.0 | 59.3 | 58.8 | 58.0 | 57.5 | 56.8 |
| 7 | $14: 41: 00$ | 56.4 | 55.1 | 57.4 | 57.0 | 56.6 | 56.4 | 55.9 |
| 8 | $14: 42: 00$ | 56.6 | 54.7 | 66.6 | 56.3 | 55.8 | 55.6 | 55.0 |
| 9 | $14: 43: 00$ | 56.0 | 54.4 | 59.6 | 57.4 | 55.8 | 55.6 | 55.1 |
| 10 | $14: 44: 00$ | 55.9 | 55.0 | 57.0 | 56.4 | 56.0 | 55.9 | 55.5 |
| 11 | $14: 45: 00$ | 56.1 | 55.4 | 57.0 | 56.6 | 56.3 | 56.1 | 55.5 |
| 12 | $14: 46: 00$ | 56.4 | 54.6 | 58.8 | 57.7 | 56.6 | 56.4 | 54.9 |
| 13 | $14: 47: 00$ | 55.9 | 55.0 | 56.8 | 56.3 | 56.1 | 56.0 | 55.3 |
| 14 | $14: 48: 00$ | 55.8 | 54.8 | 56.7 | 56.3 | 56.0 | 55.8 | 55.1 |
| 15 | $14: 49: 00$ | 56.8 | 56.1 | 57.9 | 57.1 | 56.9 | 56.8 | 56.4 |
| 16 | $14: 50: 00$ | 56.3 | 54.3 | 58.8 | 57.5 | 56.7 | 55.8 | 55.3 |
| Total for Period | 57.4 | 54.3 | 66.6 | 57.9 | 57.3 | 57.0 | 56.3 |  |

## SHORT-TERM NOISE MEASUREMENT SITE LOG

| ASSESSMENT AREA: | WEST LINN | MEASUREMENT SITE NO.: | ST-10 |
| :---: | :---: | :---: | :---: |
| ADDRESS: | 4329 IMPERIAL DRIVE |  |  |
| OWNER: |  |  |  |
| DESCRIPTION: | ATTACHED SINGLE-FAMILY RESIDENTIAL (DUPLEX) |  |  |
| NOISE SOURCES: | I-205 TRAFFIC |  |  |
| NOISE MONITOR: | LD 824 | S/N: | A3975 |
| MICROPHONE: | GRAS |  |  |
| CALIBRATOR: | CAL200 |  |  |
| TEMP. RANGE ( ${ }^{\circ} \mathrm{F}$ ): | 72 | WEATHER CONDITIONS: | SUNNY |

SITE MAP:


Notes: I-205 dominates, but is not visible from the receptor since the interstate is approximately 25 feet below the receptor which is attop a bluff.


Harris Miller Miller \& Hanson inc.

PROJECT: K19786:I-205CW
JOB NO.: 309180.000
MEASUREMENT SITE NO.: ST-11
PERSONNEL: SRN
ADDRESS/DESCRIPTION: 4835 Willamette Falls Drive DATE: 8/31/17

| \# | Time | $\begin{gathered} \hline \mathrm{L}_{\mathrm{eq}} \\ (\mathrm{dBA}) \end{gathered}$ | $\begin{gathered} \mathrm{L}_{\text {min }} \\ (\mathrm{dBA}) \end{gathered}$ | $\begin{gathered} \mathrm{L}_{\max } \\ (\mathrm{dBA}) \end{gathered}$ | $\begin{gathered} \mathrm{L}_{10} \\ (\mathrm{dBA}) \end{gathered}$ | $\begin{gathered} \mathrm{L}_{33} \\ (\mathrm{dBA}) \end{gathered}$ | $\begin{gathered} \mathrm{L}_{50} \\ (\mathrm{dBA}) \end{gathered}$ | $\begin{gathered} \mathrm{L}_{90} \\ (\mathrm{dBA}) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 13:07:00 | 59.0 | 50.7 | 64.3 | 61.8 | 59.7 | 58.3 | 53.3 |
| 2 | 13:08:00 | 56.9 | 50.3 | 64 | 59.7 | 57.4 | 56.0 | 52.2 |
| 3 | 13:09:00 | 57.3 | 49.8 | 71.9 | 59.9 | 57.4 | 55.8 | 50.9 |
| 4 | 13:10:00 | 57.8 | 51.4 | 63.2 | 60.9 | 58.4 | 57.2 | 52.2 |
| 5 | 13:11:00 | 55.4 | 48.6 | 60.4 | 58.8 | 55.9 | 54.0 | 50.3 |
| 6 | 13:12:00 | 58.8 | 52.3 | 64.8 | 62.2 | 59.2 | 57.3 | 53.5 |
| 7 | 13:13:00 | 56.0 | 50.3 | 65.3 | 59.3 | 55.5 | 53.9 | 51.3 |
| 8 | 13:14:00 | 54.5 | 48.8 | 62.7 | 58.1 | 54.0 | 51.8 | 49.5 |
| 9 | 13:15:00 | 55.7 | 50.4 | 62.5 | 58.8 | 56.5 | 53.7 | 51.1 |
| 10 | 13:16:00 | 59.1 | 51.4 | 65.6 | 62.8 | 58.9 | 57.1 | 53.1 |
| 11 | 13:17:00 | 56.2 | 49.9 | 61.4 | 59.0 | 56.3 | 55.2 | 51.4 |
| 12 | 13:18:00 | 60.0 | 50.9 | 66.3 | 62.7 | 60.9 | 59.6 | 52.3 |
| 13 | 13:19:00 | 57.3 | 51.3 | 70.6 | 59.8 | 57.3 | 55.9 | 52.6 |
| 14 | 13:20:00 | 58.0 | 50.7 | 64.6 | 61.7 | 57.9 | 55.8 | 52.0 |
| 15 | 13:21:00 | 58.7 | 50.7 | 65.8 | 61.7 | 58.9 | 57.7 | 52.2 |
| Total for Period |  | 57.6 | 48.6 | 71.9 | 60.5 | 57.6 | 56.0 | 51.9 |

## SHORT-TERM NOISE MEASUREMENT SITE LOG

| ASSESSMENT AREA: | WEST LINN | MEASUREMENT SITE NO.: | ST-11 |
| :---: | :---: | :---: | :---: |
| ADDRESS: | 4835 WILLAMETTE FALLS DRIVE |  |  |
| OWNER: |  |  |  |
| DESCRIPTION: | SINGLE-FAMILY RESIDENTIAL |  |  |
| NOISE SOURCES: | TRAFFIC ON WILLAMETTE FALLS DRIVE, I-205 TRAFFIC |  |  |
| NOISE MONITOR: | LD 824 | S/N: | A3975 |
| MICROPHONE: | GRAS |  |  |
| CALIBRATOR: | CAL200 |  |  |
| TEMP. RANGE ( ${ }^{\circ} \mathrm{F}$ ): | 72 | WEATHER CONDITIONS: | SUNNY |

SITE MAP:


Notes: I-205 is approximately 30-35 feet above the home and traffic noise from I-205 is audible but not when traffic is present on Willamette Falls Drive. The home is also approximately 10-12 feet lower than Willamette Falls Drive. Terrain is providing sheilding from noise on I-205.

Harris Miller Miller \& Hanson inc.


MEASUREMENT SITE NO.: ST-12
PERSONNEL: SRN
ADDRESS/DESCRIPTION: 5345 Grove Street
DATE: 8/31/17

| $\#$ | Time | $L_{e q}$ <br> $(d B A)$ | $L_{\text {min }}$ <br> $(d B A)$ | $L_{\text {max }}$ <br> $(d B A)$ | $L_{10}$ <br> $(d B A)$ | $L_{33}$ <br> $(d B A)$ | $L_{50}$ <br> $(d B A)$ | $L_{90}$ <br> $(d B A)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $13: 39: 25$ | 60.8 | 57.6 | 66.1 | 64.1 | 60.6 | 59.4 | 58.1 |
| 2 | $13: 40: 25$ | 58.9 | 57.3 | 61.9 | 59.9 | 59.2 | 58.8 | 57.7 |
| 3 | $13: 41: 25$ | 59.6 | 57.4 | 63.3 | 61.0 | 60.1 | 59.4 | 57.9 |
| 4 | $13: 42: 25$ | 59.8 | 57.8 | 62.8 | 60.9 | 60.1 | 59.6 | 58.4 |
| 5 | $13: 43: 25$ | 59.4 | 57.2 | 61.9 | 60.6 | 59.7 | 59.4 | 58.0 |
| 6 | $13: 44: 25$ | 59.5 | 56.6 | 63.3 | 60.9 | 59.7 | 59.2 | 58.0 |
| 7 | $13: 45: 25$ | 60.0 | 57.4 | 62.7 | 61.6 | 60.4 | 59.8 | 58.3 |
| 8 | $13: 46: 25$ | 59.5 | 57.7 | 62.3 | 60.7 | 59.7 | 59.3 | 58.2 |
| 9 | $13: 47: 25$ | 61.0 | 59.2 | 62.5 | 61.8 | 61.3 | 61.0 | 60.0 |
| 10 | $13: 48: 25$ | 61.5 | 59.1 | 67.3 | 63.8 | 61.3 | 60.7 | 59.4 |
| 11 | $13: 49: 25$ | 60.8 | 58.9 | 64.1 | 62.2 | 61.1 | 60.6 | 59.4 |
| 12 | $13: 50: 25$ | 62.2 | 59.8 | 65.1 | 64.0 | 62.5 | 61.8 | 60.5 |
| 13 | $13: 51: 25$ | 60.0 | 57.9 | 62.5 | 61.0 | 60.4 | 59.9 | 58.8 |
| 14 | $13: 52: 25$ | 58.2 | 55.6 | 60.5 | 59.2 | 58.6 | 58.2 | 56.8 |
| 15 | $13: 53: 25$ | 58.7 | 55.3 | 63.1 | 60.4 | 59.2 | 58.5 | 56.4 |
| 16 | $13: 54: 25$ | 58.7 | 54.6 | 64.5 | 60.4 | 59.0 | 58.4 | 56.5 |
| 17 | $13: 55: 25$ | 60.2 | 55.7 | 71.3 | 60.9 | 58.6 | 58.0 | 56.9 |
| 18 | $13: 56: 25$ | 58.8 | 56.7 | 62.7 | 60.0 | 59.0 | 58.6 | 57.4 |
| 19 | $13: 57: 25$ | 60.2 | 57.7 | 63.7 | 61.7 | 60.6 | 60.0 | 58.4 |
| 20 | $13: 58: 25$ | 59.1 | 56.2 | 62.5 | 60.5 | 59.5 | 59.0 | 57.5 |
| 21 | $13: 59: 25$ | 57.8 | 55.1 | 63.2 | 59.4 | 58.3 | 57.6 | 56.1 |
| 22 | $14: 00: 25$ | 59.2 | 56.5 | 64.8 | 60.5 | 59.5 | 58.9 | 57.3 |
| Total for Period | 59.9 | 54.6 | 71.3 | 61.2 | 59.9 | 59.4 | 58.0 |  |
|  |  |  |  |  |  |  |  |  |

Harris Miller Miller \& Hanson inc.

## SHORT-TERM NOISE MEASUREMENT SITE LOG

| ASSESSMENT AREA: | WEST LINN | MEASUREMENT SITE NO.: | ST-12 |
| :---: | :---: | :---: | :---: |
| ADDRESS: | 5345 GROVE STREET |  |  |
| OWNER: |  |  |  |
| DESCRIPTION: | SINGLE-FAMILY RESIDENTIAL |  |  |
| NOISE SOURCES: | l-205 TRAFFIC, BARKING SEALS |  |  |
| NOISE MONITOR: | LD 824 | S/N: | A3975 |
| MICROPHONE: | GRAS |  |  |
| CALIBRATOR: | CAL200 |  |  |
| TEMP. RANGE ( ${ }^{\circ} \mathrm{F}$ ): | 72 | WEATHER CONDITIONS: | SUNNY |

SITE MAP:


Notes: I-205 on Abernathy Bridge 35-40 feet above the home. A number of seals live in the river and bark repeatedly; however, the interstate dominates the acoustic environment.


MEASUREMENT SITE NO.: ST-13
PERSONNEL: SRN
ADDRESS/DESCRIPTION: Jon Storm Park
DATE: 8/31/17

| $\#$ | Time | $L_{\text {eq }}$ <br> $(d B A)$ | $L_{\text {min }}$ <br> $(d B A)$ | $L_{\text {max }}$ <br> $(d B A)$ | $L_{10}$ <br> $(d B A)$ | $L_{33}$ <br> $(d B A)$ | $L_{50}$ <br> $(d B A)$ | $L_{90}$ <br> $(d B A)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $14: 14: 46$ | 64.0 | 61.6 | 71.2 | 65.4 | 64.3 | 63.8 | 62.4 |
| 2 | $14: 15: 46$ | 63.6 | 60.6 | 71.3 | 65.3 | 62.9 | 62.3 | 61.2 |
| 3 | $14: 16: 46$ | 63.8 | 61.1 | 70.1 | 65.1 | 63.8 | 63.4 | 62.1 |
| 4 | $14: 17: 46$ | 63.4 | 61.1 | 66.3 | 64.7 | 63.7 | 63.3 | 62.0 |
| 5 | $14: 18: 46$ | 63.3 | 60.6 | 67.3 | 64.7 | 63.6 | 63.2 | 61.6 |
| 6 | $14: 19: 46$ | 63.8 | 60.0 | 66.9 | 65.5 | 64.3 | 63.7 | 61.5 |
| 7 | $14: 20: 46$ | 61.7 | 59.0 | 65.3 | 63.7 | 62.0 | 61.2 | 59.7 |
| 8 | $14: 21: 46$ | 61.4 | 58.6 | 65.2 | 63.2 | 61.8 | 61.0 | 59.2 |
| 9 | $14: 22: 46$ | 61.7 | 57.8 | 65.5 | 63.6 | 62.3 | 61.5 | 59.0 |
| 10 | $14: 23: 46$ | 62.6 | 59.5 | 70.2 | 64.4 | 62.6 | 61.8 | 60.2 |
| 11 | $14: 24: 46$ | 66.2 | 59.4 | 74.2 | 70.4 | 64.8 | 63.9 | 60.8 |
| 12 | $14: 25: 46$ | 62.0 | 58.9 | 65.9 | 64.2 | 62.4 | 61.1 | 59.7 |
| 13 | $14: 26: 46$ | 64.6 | 61.6 | 70.1 | 66.4 | 64.8 | 64.1 | 62.4 |
| 14 | $14: 27: 46$ | 65.7 | 60.1 | 74.3 | 68.9 | 64.7 | 63.4 | 61.4 |
| 15 | $14: 28: 46$ | 61.3 | 58.8 | 64.8 | 63.2 | 61.5 | 60.8 | 59.5 |
| 16 | $14: 29: 46$ | 63.7 | 60.3 | 71.9 | 65.7 | 63.5 | 62.7 | 61.3 |
| 17 | $14: 30: 46$ | 61.9 | 59.0 | 65.4 | 63.5 | 62.2 | 61.6 | 60.1 |
| 18 | $14: 31: 46$ | 63.7 | 59.2 | 67.5 | 66.3 | 63.8 | 63.2 | 60.4 |
| 19 | $14: 32: 46$ | 62.0 | 58.8 | 64.2 | 63.4 | 62.6 | 62.2 | 59.7 |
| Total $\operatorname{for}$ Period | 63.4 | 57.8 | 74.3 | 65.1 | 63.2 | 62.5 | 60.7 |  |

## SHORT-TERM NOISE MEASUREMENT SITE LOG

| ASSESSMENT AREA: | WEST LINN | MEASUREMENT SITE NO.: | ST-13 |
| :---: | :---: | :---: | :---: |
| ADDRESS: | 1801 CLACKAMETTE DRIVE |  |  |
| OWNER: |  |  |  |
| DESCRIPTION: | JON STORM PARK |  |  |
| NOISE SOURCES: | I-205 TRAFFIC, HIGHWAY 99E |  |  |
| NOISE MONITOR: | LD 824 | S/N: | A3975 |
| MICROPHONE: | GRAS |  |  |
| CALIBRATOR: | CAL200 |  |  |
| TEMP. RANGE ( ${ }^{\circ} \mathrm{F}$ ): | 73 | WEATHER CONDITIONS: | SUNNY |

SITE MAP:


Notes: I-205 on Abernathy Bridge 35-40 feet above the park. Highway 99E is also a major source of traffic noise.


## SHORT-TERIV NOISE IVEASUREIVENT SHE LOG

ASSESSMENT AREA: Jon stain PARA $(0)$ MEASUREMENT SITE NO.: $\qquad$
ADDRESS:
John storm PAQK
OVVNER:
DESCRIPTION:
NOISE SOURCES:
NOISE MONITOR:
MICROPHONE:
CALIBRATOR:
TEMP. RANGE ( ${ }^{\circ}$ ) :


SITE SKETCH: Show roadway, homes, local roads, reference distances, arrows for North \& wind direction, where roadway is in cut, at grade, elevated, where direct lines of sight exist.


PHOTOS: YES

## SHORT-TERM NOISE MEASUREMENT DATA SHEET

PROJECT: K19786:I-205CW

$$
\text { JOB NO.: } \quad 309180.000
$$

MEASUREMENT SITE NO: OC Structure Berre Me\&tsommts PERSONNEL: SRN ADDRESSIDESCRIPTION: Jun Storm Park

| $66$ | Minute <br> Period Starting | Meas'd Leq <br> (dBA) | V or $\times$ | Autos | Medium Trucks | Heavy Trucks | Other Noise Sources | COMMENTS (Include Calibration Data) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Dree mbye | 72.3 |  |  |  |  |  | if:17~n - 12:23pm |
| 2 |  |  |  |  |  |  |  |  |
| 3 | So' | 68.5 |  |  |  |  |  | $11: 170 \mathrm{~m}$ - 12:230m |
| 4 |  |  |  |  |  |  |  | - |
| 5 | $100^{\prime}$ | 68:3 |  |  |  |  |  | 11:/7im $-12: 23 \mathrm{pm}$ |
| 6 |  |  |  |  |  |  |  |  |
| 7 |  |  |  |  |  |  |  |  |
| 8 |  |  |  |  |  |  |  |  |
| 9 |  |  |  |  |  |  |  |  |
| 10 |  |  |  |  |  |  |  |  |
| 11 |  |  |  |  |  |  |  |  |
| 12 |  |  |  |  |  |  |  |  |
| 13 |  |  |  |  |  |  |  |  |
| 14 |  |  |  |  |  |  |  |  |
| 15 |  |  |  |  |  |  |  |  |
| 16 |  |  |  |  |  |  |  |  |
| 17 |  |  |  |  |  |  |  |  |
| 18 |  |  |  |  |  |  |  |  |
| 19 |  |  |  |  |  |  |  |  |
| 20 |  |  |  |  |  |  |  |  |
| 21 |  |  |  |  |  |  |  |  |
| 22 |  |  |  |  |  |  |  |  |
| 23 |  |  |  |  |  |  |  |  |
| 24 |  |  |  |  |  |  |  |  |
| 25 |  |  |  |  |  |  |  |  |
| 26 |  |  |  |  |  |  |  |  |
| 27 |  |  |  |  |  |  |  |  |
| 28 |  |  |  |  |  |  |  |  |
| 29 |  |  |  |  |  |  |  |  |
| 30 |  |  |  |  |  |  |  |  |

TOTAL Leq =
SUBSET Leq =
$V=$ Other sources contributed to Leq $\quad \mathrm{X}=$ Exclude period - contaminated by non-characteristic sources
$>$ ADD SKETCH AND WEATHER CONDITIONS TO REVERSE OR OTHER SHEET <<

Oregon City - John Storm Park Structure-Borne Noise Measurements


100 feet

Drip Edge


50 feet

| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| Oregon City Side of Crossing |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 50 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 25 |
| w: Width of Structure |  |  |  | 100 |
| Mw: Midpoint of structure (w/2) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 50 |
| Dref: Reference distance - from S to Aref |  |  |  | 55.9 |
| Measured Noise Level at Drip Edge, dB (A) |  |  |  | 72.3 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from <br> Drip Edge (ft.) | Distance from <br> Analysis Point <br> (ft.) | Measured Noise Level at Drip Edge Leq in $\mathrm{dB}(\mathrm{A})$ | Calculated <br> Noise Level <br> Drop-off Rate $=3.0 \mathrm{~dB} / \mathrm{DD}$ |
| Aref | 0 | 55.9 | 72.3 |  |
| A25 | 25 | 80.9 |  | 71 |
| A50 | 50 | 105.9 |  | 70 |
| A100 | 100 | 155.9 |  | 68 |
| A200 | 200 | 255.9 |  | 66 |
| A400 | 400 | 455.9 |  | 63 |
| A500 | 500 | 555.9 |  | 62 |
| Analysis Point | Distance from <br> Drip Edge (ft.) | Distance from <br> Analysis Point <br> (ft.) | Measured Noise Level at Drip Edge Leq in $\mathrm{dB}(\mathrm{A})$ | Calculated Noise Level Drop-off Rate $=4.5 \mathrm{~dB} / \mathrm{DD}$ |
| Aref | 0 | 55.9 | 72.3 |  |
| A25 | 25 | 80.9 |  | 69.9 |
| A50 | 50 | 105.9 |  | 68.1 |
| A100 | 100 | 155.9 |  | 65.6 |
| A200 | 200 | 255.9 |  | 62.4 |
| A400 | 400 | 455.9 |  | 58.6 |
| A500 | 500 | 555.9 |  | 57.3 |
| Analysis Point | Distance from <br> Drip Edge (ft.) | Distance from <br> Analysis Point <br> (ft.) | Measured Noise Level at Drip Edge Leq in $\mathrm{dB}(\mathrm{A})$ | Calculated Noise Level Drop-off Rate $=6.0 \mathrm{~dB} / \mathrm{DD}$ |
| Aref | 0 | 55.9 | 72.3 |  |
| A25 | 25 | 80.9 |  | 69 |
| A50 | 50 | 105.9 |  | 67 |
| A100 | 100 | 155.9 |  | 63 |
| A200 | 200 | 255.9 |  | 59 |
| A400 | 400 | 455.9 |  | 54 |
| A500 | 500 | 555.9 |  | 52 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| Southbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 50 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 25 |
| w: Width of Structure |  |  |  | 100 |
| Mw: Midpoint of structure (w/2) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 50 |
| Dref: Reference distance - from S to Aref |  |  |  | 55.9 |
| Measured Noise Level at Drip Edge, $\mathrm{dB}(\mathrm{A})$ |  |  |  | 72.3 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from <br> Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in dB(A) | ```Calculated Noise Level Drop-off Rate = 4.5 dB/DD``` |
| Aref | 0 | 55.9 | 72.3 |  |
| A1 | 1 | 56.9 |  | 72.2 |
| A2 | 2 | 57.9 |  | 72.1 |
| A3 | 3 | 58.9 |  | 72.0 |
| A4 | 4 | 59.9 |  | 71.8 |
| A5 | 5 | 60.9 |  | 71.7 |
| A6 | 6 | 61.9 |  | 71.6 |
| A7 | 7 | 62.9 |  | 71.5 |
| A8 | 8 | 63.9 |  | 71.4 |
| A9 | 9 | 64.9 |  | 71.3 |
| A10 | 10 | 65.9 |  | 71.2 |
| A11 | 11 | 66.9 |  | 71.1 |
| A12 | 12 | 67.9 |  | 71.0 |
| A13 | 13 | 68.9 |  | 70.9 |
| A14 | 14 | 69.9 |  | 70.8 |
| A15 | 15 | 70.9 |  | 70.8 |
| A16 | 16 | 71.9 |  | 70.7 |
| A17 | 17 | 72.9 |  | 70.6 |
| A18 | 18 | 73.9 |  | 70.5 |
| A19 | 19 | 74.9 |  | 70.4 |
| A20 | 20 | 75.9 |  | 70.3 |
| A21 | 21 | 76.9 |  | 70.2 |
| A22 | 22 | 77.9 |  | 70.1 |
| A23 | 23 | 78.9 |  | 70.1 |
| A24 | 24 | 79.9 |  | 70.0 |
| A25 | 25 | 80.9 |  | 69.9 |
| A26 | 26 | 81.9 |  | 69.8 |
| A27 | 27 | 82.9 |  | 69.7 |
| A28 | 28 | 83.9 |  | 69.7 |
| A29 | 29 | 84.9 |  | 69.6 |
| A30 | 30 | 85.9 |  | 69.5 |
| A31 | 31 | 86.9 |  | 69.4 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| Southbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 50 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 25 |
| w: Width of Structure |  |  |  | 100 |
| Mw: Midpoint of structure (w/2) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 50 |
| Dref: Reference distance - from S to Aref |  |  |  | 55.9 |
| Measured Noise Level at Drip Edge, $\mathrm{dB}(\mathrm{A})$ |  |  |  | 72.3 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from <br> Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in dB(A) | $\begin{gathered} \text { Calculated Noise Level } \\ \text { Drop-off Rate = } 4.5 \\ \text { dB/DD } \end{gathered}$ |
| A32 | 32 | 87.9 |  | 69.4 |
| A33 | 33 | 88.9 |  | 69.3 |
| A34 | 34 | 89.9 |  | 69.2 |
| A35 | 35 | 90.9 |  | 69.1 |
| A36 | 36 | 91.9 |  | 69.1 |
| A37 | 37 | 92.9 |  | 69.0 |
| A38 | 38 | 93.9 |  | 68.9 |
| A39 | 39 | 94.9 |  | 68.9 |
| A40 | 40 | 95.9 |  | 68.8 |
| A41 | 41 | 96.9 |  | 68.7 |
| A42 | 42 | 97.9 |  | 68.6 |
| A43 | 43 | 98.9 |  | 68.6 |
| A44 | 44 | 99.9 |  | 68.5 |
| A45 | 45 | 100.9 |  | 68.5 |
| A46 | 46 | 101.9 |  | 68.4 |
| A47 | 47 | 102.9 |  | 68.3 |
| A48 | 48 | 103.9 |  | 68.3 |
| A49 | 49 | 104.9 |  | 68.2 |
| A50 | 50 | 105.9 |  | 68.1 |
| A51 | 51 | 106.9 |  | 68.1 |
| A52 | 52 | 107.9 |  | 68.0 |
| A53 | 53 | 108.9 |  | 68.0 |
| A54 | 54 | 109.9 |  | 67.9 |
| A55 | 55 | 110.9 |  | 67.8 |
| A56 | 56 | 111.9 |  | 67.8 |
| A57 | 57 | 112.9 |  | 67.7 |
| A58 | 58 | 113.9 |  | 67.7 |
| A59 | 59 | 114.9 |  | 67.6 |
| A60 | 60 | 115.9 |  | 67.6 |
| A61 | 61 | 116.9 |  | 67.5 |
| A62 | 62 | 117.9 |  | 67.4 |
| A63 | 63 | 118.9 |  | 67.4 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| Southbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 50 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 25 |
| w: Width of Structure |  |  |  | 100 |
| Mw: Midpoint of structure (w/2) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 50 |
| Dref: Reference distance - from S to Aref |  |  |  | 55.9 |
| Measured Noise Level at Drip Edge, $\mathrm{dB}(\mathrm{A})$ |  |  |  | 72.3 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from <br> Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in dB(A) | ```Calculated Noise Level Drop-off Rate = 4.5 dB/DD``` |
| A64 | 64 | 119.9 |  | 67.3 |
| A65 | 65 | 120.9 |  | 67.3 |
| A66 | 66 | 121.9 |  | 67.2 |
| A67 | 67 | 122.9 |  | 67.2 |
| A68 | 68 | 123.9 |  | 67.1 |
| A69 | 69 | 124.9 |  | 67.1 |
| A70 | 70 | 125.9 |  | 67.0 |
| A71 | 71 | 126.9 |  | 67.0 |
| A72 | 72 | 127.9 |  | 66.9 |
| A73 | 73 | 128.9 |  | 66.9 |
| A74 | 74 | 129.9 |  | 66.8 |
| A75 | 75 | 130.9 |  | 66.8 |
| A76 | 76 | 131.9 |  | 66.7 |
| A77 | 77 | 132.9 |  | 66.7 |
| A78 | 78 | 133.9 |  | 66.6 |
| A79 | 79 | 134.9 |  | 66.6 |
| A80 | 80 | 135.9 |  | 66.5 |
| A81 | 81 | 136.9 |  | 66.5 |
| A82 | 82 | 137.9 |  | 66.4 |
| A83 | 83 | 138.9 |  | 66.4 |
| A84 | 84 | 139.9 |  | 66.3 |
| A85 | 85 | 140.9 |  | 66.3 |
| A86 | 86 | 141.9 |  | 66.2 |
| A87 | 87 | 142.9 |  | 66.2 |
| A88 | 88 | 143.9 |  | 66.1 |
| A89 | 89 | 144.9 |  | 66.1 |
| A90 | 90 | 145.9 |  | 66.1 |
| A91 | 91 | 146.9 |  | 66.0 |
| A92 | 92 | 147.9 |  | 66.0 |
| A93 | 93 | 148.9 |  | 65.9 |
| A94 | 94 | 149.9 |  | 65.9 |
| A95 | 95 | 150.9 |  | 65.8 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| Southbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 50 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 25 |
| w: Width of Structure |  |  |  | 100 |
| Mw: Midpoint of structure (w/2) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 50 |
| Dref: Reference distance - from S to Aref |  |  |  | 55.9 |
| Measured Noise Level at Drip Edge, $\mathrm{dB}(\mathrm{A})$ |  |  |  | 72.3 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from <br> Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in dB(A) | ```Calculated Noise Level Drop-off Rate = 4.5 dB/DD``` |
| A96 | 96 | 151.9 |  | 65.8 |
| A97 | 97 | 152.9 |  | 65.7 |
| A98 | 98 | 153.9 |  | 65.7 |
| A99 | 99 | 154.9 |  | 65.7 |
| A100 | 100 | 155.9 |  | 65.6 |
| A101 | 101 | 156.9 |  | 65.6 |
| A102 | 102 | 157.9 |  | 65.5 |
| A103 | 103 | 158.9 |  | 65.5 |
| A104 | 104 | 159.9 |  | 65.5 |
| A105 | 105 | 160.9 |  | 65.4 |
| A106 | 106 | 161.9 |  | 65.4 |
| A107 | 107 | 162.9 |  | 65.3 |
| A108 | 108 | 163.9 |  | 65.3 |
| A109 | 109 | 164.9 |  | 65.3 |
| A110 | 110 | 165.9 |  | 65.2 |
| A111 | 111 | 166.9 |  | 65.2 |
| A112 | 112 | 167.9 |  | 65.1 |
| A113 | 113 | 168.9 |  | 65.1 |
| A114 | 114 | 169.9 |  | 65.1 |
| A115 | 115 | 170.9 |  | 65.0 |
| A116 | 116 | 171.9 |  | 65.0 |
| A117 | 117 | 172.9 |  | 64.9 |
| A118 | 118 | 173.9 |  | 64.9 |
| A119 | 119 | 174.9 |  | 64.9 |
| A120 | 120 | 175.9 |  | 64.8 |
| A121 | 121 | 176.9 |  | 64.8 |
| A122 | 122 | 177.9 |  | 64.8 |
| A123 | 123 | 178.9 |  | 64.7 |
| A124 | 124 | 179.9 |  | 64.7 |
| A125 | 125 | 180.9 |  | 64.6 |
| A126 | 126 | 181.9 |  | 64.6 |
| A127 | 127 | 182.9 |  | 64.6 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| Southbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 50 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 25 |
| w: Width of Structure |  |  |  | 100 |
| Mw: Midpoint of structure (w/2) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 50 |
| Dref: Reference distance - from S to Aref |  |  |  | 55.9 |
| Measured Noise Level at Drip Edge, $\mathrm{dB}(\mathrm{A})$ |  |  |  | 72.3 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in dB(A) | ```Calculated Noise Level Drop-off Rate = 4.5 dB/DD``` |
| A128 | 128 | 183.9 |  | 64.5 |
| A129 | 129 | 184.9 |  | 64.5 |
| A130 | 130 | 185.9 |  | 64.5 |
| A131 | 131 | 186.9 |  | 64.4 |
| A132 | 132 | 187.9 |  | 64.4 |
| A133 | 133 | 188.9 |  | 64.4 |
| A134 | 134 | 189.9 |  | 64.3 |
| A135 | 135 | 190.9 |  | 64.3 |
| A136 | 136 | 191.9 |  | 64.3 |
| A137 | 137 | 192.9 |  | 64.2 |
| A138 | 138 | 193.9 |  | 64.2 |
| A139 | 139 | 194.9 |  | 64.2 |
| A140 | 140 | 195.9 |  | 64.1 |
| A141 | 141 | 196.9 |  | 64.1 |
| A142 | 142 | 197.9 |  | 64.1 |
| A143 | 143 | 198.9 |  | 64.0 |
| A144 | 144 | 199.9 |  | 64.0 |
| A145 | 145 | 200.9 |  | 64.0 |
| A146 | 146 | 201.9 |  | 63.9 |
| A147 | 147 | 202.9 |  | 63.9 |
| A148 | 148 | 203.9 |  | 63.9 |
| A149 | 149 | 204.9 |  | 63.8 |
| A150 | 150 | 205.9 |  | 63.8 |
| A151 | 151 | 206.9 |  | 63.8 |
| A152 | 152 | 207.9 |  | 63.7 |
| A153 | 153 | 208.9 |  | 63.7 |
| A154 | 154 | 209.9 |  | 63.7 |
| A155 | 155 | 210.9 |  | 63.7 |
| A156 | 156 | 211.9 |  | 63.6 |
| A157 | 157 | 212.9 |  | 63.6 |
| A158 | 158 | 213.9 |  | 63.6 |
| A159 | 159 | 214.9 |  | 63.5 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| Southbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 50 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 25 |
| w: Width of Structure |  |  |  | 100 |
| Mw: Midpoint of structure (w/2) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 50 |
| Dref: Reference distance - from S to Aref |  |  |  | 55.9 |
| Measured Noise Level at Drip Edge, $\mathrm{dB}(\mathrm{A})$ |  |  |  | 72.3 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in dB(A) | ```Calculated Noise Level Drop-off Rate = 4.5 dB/DD``` |
| A160 | 160 | 215.9 |  | 63.5 |
| A161 | 161 | 216.9 |  | 63.5 |
| A162 | 162 | 217.9 |  | 63.4 |
| A163 | 163 | 218.9 |  | 63.4 |
| A164 | 164 | 219.9 |  | 63.4 |
| A165 | 165 | 220.9 |  | 63.3 |
| A166 | 166 | 221.9 |  | 63.3 |
| A167 | 167 | 222.9 |  | 63.3 |
| A168 | 168 | 223.9 |  | 63.3 |
| A169 | 169 | 224.9 |  | 63.2 |
| A170 | 170 | 225.9 |  | 63.2 |
| A171 | 171 | 226.9 |  | 63.2 |
| A172 | 172 | 227.9 |  | 63.1 |
| A173 | 173 | 228.9 |  | 63.1 |
| A174 | 174 | 229.9 |  | 63.1 |
| A175 | 175 | 230.9 |  | 63.1 |
| A176 | 176 | 231.9 |  | 63.0 |
| A177 | 177 | 232.9 |  | 63.0 |
| A178 | 178 | 233.9 |  | 63.0 |
| A179 | 179 | 234.9 |  | 62.9 |
| A180 | 180 | 235.9 |  | 62.9 |
| A181 | 181 | 236.9 |  | 62.9 |
| A182 | 182 | 237.9 |  | 62.9 |
| A183 | 183 | 238.9 |  | 62.8 |
| A184 | 184 | 239.9 |  | 62.8 |
| A185 | 185 | 240.9 |  | 62.8 |
| A186 | 186 | 241.9 |  | 62.8 |
| A187 | 187 | 242.9 |  | 62.7 |
| A188 | 188 | 243.9 |  | 62.7 |
| A189 | 189 | 244.9 |  | 62.7 |
| A190 | 190 | 245.9 |  | 62.6 |
| A191 | 191 | 246.9 |  | 62.6 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| Southbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 50 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 25 |
| w: Width of Structure |  |  |  | 100 |
| Mw: Midpoint of structure (w/2) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 50 |
| Dref: Reference distance - from S to Aref |  |  |  | 55.9 |
| Measured Noise Level at Drip Edge, $\mathrm{dB}(\mathrm{A})$ |  |  |  | 72.3 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from <br> Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in dB(A) | ```Calculated Noise Level Drop-off Rate = 4.5 dB/DD``` |
| A192 | 192 | 247.9 |  | 62.6 |
| A193 | 193 | 248.9 |  | 62.6 |
| A194 | 194 | 249.9 |  | 62.5 |
| A195 | 195 | 250.9 |  | 62.5 |
| A196 | 196 | 251.9 |  | 62.5 |
| A197 | 197 | 252.9 |  | 62.5 |
| A198 | 198 | 253.9 |  | 62.4 |
| A199 | 199 | 254.9 |  | 62.4 |
| A200 | 200 | 255.9 |  | 62.4 |
| A201 | 201 | 256.9 |  | 62.4 |
| A202 | 202 | 257.9 |  | 62.3 |
| A203 | 203 | 258.9 |  | 62.3 |
| A204 | 204 | 259.9 |  | 62.3 |
| A205 | 205 | 260.9 |  | 62.3 |
| A206 | 206 | 261.9 |  | 62.2 |
| A207 | 207 | 262.9 |  | 62.2 |
| A208 | 208 | 263.9 |  | 62.2 |
| A209 | 209 | 264.9 |  | 62.2 |
| A210 | 210 | 265.9 |  | 62.1 |
| A211 | 211 | 266.9 |  | 62.1 |
| A212 | 212 | 267.9 |  | 62.1 |
| A213 | 213 | 268.9 |  | 62.1 |
| A214 | 214 | 269.9 |  | 62.0 |
| A215 | 215 | 270.9 |  | 62.0 |
| A216 | 216 | 271.9 |  | 62.0 |
| A217 | 217 | 272.9 |  | 62.0 |
| A218 | 218 | 273.9 |  | 61.9 |
| A219 | 219 | 274.9 |  | 61.9 |
| A220 | 220 | 275.9 |  | 61.9 |
| A221 | 221 | 276.9 |  | 61.9 |
| A222 | 222 | 277.9 |  | 61.9 |
| A223 | 223 | 278.9 |  | 61.8 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| Southbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 50 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 25 |
| w: Width of Structure |  |  |  | 100 |
| Mw: Midpoint of structure (w/2) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 50 |
| Dref: Reference distance - from S to Aref |  |  |  | 55.9 |
| Measured Noise Level at Drip Edge, $\mathrm{dB}(\mathrm{A})$ |  |  |  | 72.3 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from <br> Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in dB(A) | $\begin{gathered} \text { Calculated Noise Level } \\ \text { Drop-off Rate = } 4.5 \\ \text { dB/DD } \end{gathered}$ |
| A224 | 224 | 279.9 |  | 61.8 |
| A225 | 225 | 280.9 |  | 61.8 |
| A226 | 226 | 281.9 |  | 61.8 |
| A227 | 227 | 282.9 |  | 61.7 |
| A228 | 228 | 283.9 |  | 61.7 |
| A229 | 229 | 284.9 |  | 61.7 |
| A230 | 230 | 285.9 |  | 61.7 |
| A231 | 231 | 286.9 |  | 61.6 |
| A232 | 232 | 287.9 |  | 61.6 |
| A233 | 233 | 288.9 |  | 61.6 |
| A234 | 234 | 289.9 |  | 61.6 |
| A235 | 235 | 290.9 |  | 61.6 |
| A236 | 236 | 291.9 |  | 61.5 |
| A237 | 237 | 292.9 |  | 61.5 |
| A238 | 238 | 293.9 |  | 61.5 |
| A239 | 239 | 294.9 |  | 61.5 |
| A240 | 240 | 295.9 |  | 61.4 |
| A241 | 241 | 296.9 |  | 61.4 |
| A242 | 242 | 297.9 |  | 61.4 |
| A243 | 243 | 298.9 |  | 61.4 |
| A244 | 244 | 299.9 |  | 61.4 |
| A245 | 245 | 300.9 |  | 61.3 |
| A246 | 246 | 301.9 |  | 61.3 |
| A247 | 247 | 302.9 |  | 61.3 |
| A248 | 248 | 303.9 |  | 61.3 |
| A249 | 249 | 304.9 |  | 61.2 |
| A250 | 250 | 305.9 |  | 61.2 |
| A251 | 251 | 306.9 |  | 61.2 |
| A252 | 252 | 307.9 |  | 61.2 |
| A253 | 253 | 308.9 |  | 61.2 |
| A254 | 254 | 309.9 |  | 61.1 |
| A255 | 255 | 310.9 |  | 61.1 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| Southbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 50 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 25 |
| w: Width of Structure |  |  |  | 100 |
| Mw: Midpoint of structure (w/2) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 50 |
| Dref: Reference distance - from S to Aref |  |  |  | 55.9 |
| Measured Noise Level at Drip Edge, $\mathrm{dB}(\mathrm{A})$ |  |  |  | 72.3 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in dB(A) | ```Calculated Noise Level Drop-off Rate = 4.5 dB/DD``` |
| A256 | 256 | 311.9 |  | 61.1 |
| A257 | 257 | 312.9 |  | 61.1 |
| A258 | 258 | 313.9 |  | 61.1 |
| A259 | 259 | 314.9 |  | 61.0 |
| A260 | 260 | 315.9 |  | 61.0 |
| A261 | 261 | 316.9 |  | 61.0 |
| A262 | 262 | 317.9 |  | 61.0 |
| A263 | 263 | 318.9 |  | 61.0 |
| A264 | 264 | 319.9 |  | 60.9 |
| A265 | 265 | 320.9 |  | 60.9 |
| A266 | 266 | 321.9 |  | 60.9 |
| A267 | 267 | 322.9 |  | 60.9 |
| A268 | 268 | 323.9 |  | 60.9 |
| A269 | 269 | 324.9 |  | 60.8 |
| A270 | 270 | 325.9 |  | 60.8 |
| A271 | 271 | 326.9 |  | 60.8 |
| A272 | 272 | 327.9 |  | 60.8 |
| A273 | 273 | 328.9 |  | 60.8 |
| A274 | 274 | 329.9 |  | 60.7 |
| A275 | 275 | 330.9 |  | 60.7 |
| A276 | 276 | 331.9 |  | 60.7 |
| A277 | 277 | 332.9 |  | 60.7 |
| A278 | 278 | 333.9 |  | 60.7 |
| A279 | 279 | 334.9 |  | 60.6 |
| A280 | 280 | 335.9 |  | 60.6 |
| A281 | 281 | 336.9 |  | 60.6 |
| A282 | 282 | 337.9 |  | 60.6 |
| A283 | 283 | 338.9 |  | 60.6 |
| A284 | 284 | 339.9 |  | 60.5 |
| A285 | 285 | 340.9 |  | 60.5 |
| A286 | 286 | 341.9 |  | 60.5 |
| A287 | 287 | 342.9 |  | 60.5 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| Southbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 50 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 25 |
| w: Width of Structure |  |  |  | 100 |
| Mw: Midpoint of structure (w/2) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 50 |
| Dref: Reference distance - from S to Aref |  |  |  | 55.9 |
| Measured Noise Level at Drip Edge, $\mathrm{dB}(\mathrm{A})$ |  |  |  | 72.3 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from <br> Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in dB(A) | ```Calculated Noise Level Drop-off Rate = 4.5 dB/DD``` |
| A288 | 288 | 343.9 |  | 60.5 |
| A289 | 289 | 344.9 |  | 60.4 |
| A290 | 290 | 345.9 |  | 60.4 |
| A291 | 291 | 346.9 |  | 60.4 |
| A292 | 292 | 347.9 |  | 60.4 |
| A293 | 293 | 348.9 |  | 60.4 |
| A294 | 294 | 349.9 |  | 60.4 |
| A295 | 295 | 350.9 |  | 60.3 |
| A296 | 296 | 351.9 |  | 60.3 |
| A297 | 297 | 352.9 |  | 60.3 |
| A298 | 298 | 353.9 |  | 60.3 |
| A299 | 299 | 354.9 |  | 60.3 |
| A300 | 300 | 355.9 |  | 60.2 |
| A301 | 301 | 356.9 |  | 60.2 |
| A302 | 302 | 357.9 |  | 60.2 |
| A303 | 303 | 358.9 |  | 60.2 |
| A304 | 304 | 359.9 |  | 60.2 |
| A305 | 305 | 360.9 |  | 60.2 |
| A306 | 306 | 361.9 |  | 60.1 |
| A307 | 307 | 362.9 |  | 60.1 |
| A308 | 308 | 363.9 |  | 60.1 |
| A309 | 309 | 364.9 |  | 60.1 |
| A310 | 310 | 365.9 |  | 60.1 |
| A311 | 311 | 366.9 |  | 60.0 |
| A312 | 312 | 367.9 |  | 60.0 |
| A313 | 313 | 368.9 |  | 60.0 |
| A314 | 314 | 369.9 |  | 60.0 |
| A315 | 315 | 370.9 |  | 60.0 |
| A316 | 316 | 371.9 |  | 60.0 |
| A317 | 317 | 372.9 |  | 59.9 |
| A318 | 318 | 373.9 |  | 59.9 |
| A319 | 319 | 374.9 |  | 59.9 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| Southbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 50 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 25 |
| w: Width of Structure |  |  |  | 100 |
| Mw: Midpoint of structure (w/2) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 50 |
| Dref: Reference distance - from S to Aref |  |  |  | 55.9 |
| Measured Noise Level at Drip Edge, $\mathrm{dB}(\mathrm{A})$ |  |  |  | 72.3 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in dB(A) | ```Calculated Noise Level Drop-off Rate = 4.5 dB/DD``` |
| A320 | 320 | 375.9 |  | 59.9 |
| A321 | 321 | 376.9 |  | 59.9 |
| A322 | 322 | 377.9 |  | 59.9 |
| A323 | 323 | 378.9 |  | 59.8 |
| A324 | 324 | 379.9 |  | 59.8 |
| A325 | 325 | 380.9 |  | 59.8 |
| A326 | 326 | 381.9 |  | 59.8 |
| A327 | 327 | 382.9 |  | 59.8 |
| A328 | 328 | 383.9 |  | 59.7 |
| A329 | 329 | 384.9 |  | 59.7 |
| A330 | 330 | 385.9 |  | 59.7 |
| A331 | 331 | 386.9 |  | 59.7 |
| A332 | 332 | 387.9 |  | 59.7 |
| A333 | 333 | 388.9 |  | 59.7 |
| A334 | 334 | 389.9 |  | 59.6 |
| A335 | 335 | 390.9 |  | 59.6 |
| A336 | 336 | 391.9 |  | 59.6 |
| A337 | 337 | 392.9 |  | 59.6 |
| A338 | 338 | 393.9 |  | 59.6 |
| A339 | 339 | 394.9 |  | 59.6 |
| A340 | 340 | 395.9 |  | 59.5 |
| A341 | 341 | 396.9 |  | 59.5 |
| A342 | 342 | 397.9 |  | 59.5 |
| A343 | 343 | 398.9 |  | 59.5 |
| A344 | 344 | 399.9 |  | 59.5 |
| A345 | 345 | 400.9 |  | 59.5 |
| A346 | 346 | 401.9 |  | 59.4 |
| A347 | 347 | 402.9 |  | 59.4 |
| A348 | 348 | 403.9 |  | 59.4 |
| A349 | 349 | 404.9 |  | 59.4 |
| A350 | 350 | 405.9 |  | 59.4 |
| A351 | 351 | 406.9 |  | 59.4 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| Southbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 50 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 25 |
| w: Width of Structure |  |  |  | 100 |
| Mw: Midpoint of structure (w/2) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 50 |
| Dref: Reference distance - from S to Aref |  |  |  | 55.9 |
| Measured Noise Level at Drip Edge, $\mathrm{dB}(\mathrm{A})$ |  |  |  | 72.3 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from <br> Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in dB(A) | ```Calculated Noise Level Drop-off Rate = 4.5 dB/DD``` |
| A352 | 352 | 407.9 |  | 59.4 |
| A353 | 353 | 408.9 |  | 59.3 |
| A354 | 354 | 409.9 |  | 59.3 |
| A355 | 355 | 410.9 |  | 59.3 |
| A356 | 356 | 411.9 |  | 59.3 |
| A357 | 357 | 412.9 |  | 59.3 |
| A358 | 358 | 413.9 |  | 59.3 |
| A359 | 359 | 414.9 |  | 59.2 |
| A360 | 360 | 415.9 |  | 59.2 |
| A361 | 361 | 416.9 |  | 59.2 |
| A362 | 362 | 417.9 |  | 59.2 |
| A363 | 363 | 418.9 |  | 59.2 |
| A364 | 364 | 419.9 |  | 59.2 |
| A365 | 365 | 420.9 |  | 59.1 |
| A366 | 366 | 421.9 |  | 59.1 |
| A367 | 367 | 422.9 |  | 59.1 |
| A368 | 368 | 423.9 |  | 59.1 |
| A369 | 369 | 424.9 |  | 59.1 |
| A370 | 370 | 425.9 |  | 59.1 |
| A371 | 371 | 426.9 |  | 59.1 |
| A372 | 372 | 427.9 |  | 59.0 |
| A373 | 373 | 428.9 |  | 59.0 |
| A374 | 374 | 429.9 |  | 59.0 |
| A375 | 375 | 430.9 |  | 59.0 |
| A376 | 376 | 431.9 |  | 59.0 |
| A377 | 377 | 432.9 |  | 59.0 |
| A378 | 378 | 433.9 |  | 59.0 |
| A379 | 379 | 434.9 |  | 58.9 |
| A380 | 380 | 435.9 |  | 58.9 |
| A381 | 381 | 436.9 |  | 58.9 |
| A382 | 382 | 437.9 |  | 58.9 |
| A383 | 383 | 438.9 |  | 58.9 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| Southbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 50 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 25 |
| w: Width of Structure |  |  |  | 100 |
| Mw: Midpoint of structure (w/2) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 50 |
| Dref: Reference distance - from S to Aref |  |  |  | 55.9 |
| Measured Noise Level at Drip Edge, $\mathrm{dB}(\mathrm{A})$ |  |  |  | 72.3 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from <br> Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in dB(A) | $\begin{gathered} \text { Calculated Noise Level } \\ \text { Drop-off Rate }=4.5 \\ \text { dB/DD } \end{gathered}$ |
| A384 | 384 | 439.9 |  | 58.9 |
| A385 | 385 | 440.9 |  | 58.8 |
| A386 | 386 | 441.9 |  | 58.8 |
| A387 | 387 | 442.9 |  | 58.8 |
| A388 | 388 | 443.9 |  | 58.8 |
| A389 | 389 | 444.9 |  | 58.8 |
| A390 | 390 | 445.9 |  | 58.8 |
| A391 | 391 | 446.9 |  | 58.8 |
| A392 | 392 | 447.9 |  | 58.7 |
| A393 | 393 | 448.9 |  | 58.7 |
| A394 | 394 | 449.9 |  | 58.7 |
| A395 | 395 | 450.9 |  | 58.7 |
| A396 | 396 | 451.9 |  | 58.7 |
| A397 | 397 | 452.9 |  | 58.7 |
| A398 | 398 | 453.9 |  | 58.7 |
| A399 | 399 | 454.9 |  | 58.6 |
| A400 | 400 | 455.9 |  | 58.6 |
| A401 | 401 | 456.9 |  | 58.6 |
| A402 | 402 | 457.9 |  | 58.6 |
| A403 | 403 | 458.9 |  | 58.6 |
| A404 | 404 | 459.9 |  | 58.6 |
| A405 | 405 | 460.9 |  | 58.6 |
| A406 | 406 | 461.9 |  | 58.5 |
| A407 | 407 | 462.9 |  | 58.5 |
| A408 | 408 | 463.9 |  | 58.5 |
| A409 | 409 | 464.9 |  | 58.5 |
| A410 | 410 | 465.9 |  | 58.5 |
| A411 | 411 | 466.9 |  | 58.5 |
| A412 | 412 | 467.9 |  | 58.5 |
| A413 | 413 | 468.9 |  | 58.4 |
| A414 | 414 | 469.9 |  | 58.4 |
| A415 | 415 | 470.9 |  | 58.4 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| Southbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 50 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 25 |
| w: Width of Structure |  |  |  | 100 |
| Mw: Midpoint of structure (w/2) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 50 |
| Dref: Reference distance - from S to Aref |  |  |  | 55.9 |
| Measured Noise Level at Drip Edge, $\mathrm{dB}(\mathrm{A})$ |  |  |  | 72.3 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from <br> Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in dB(A) | ```Calculated Noise Level Drop-off Rate = 4.5 dB/DD``` |
| A416 | 416 | 471.9 |  | 58.4 |
| A417 | 417 | 472.9 |  | 58.4 |
| A418 | 418 | 473.9 |  | 58.4 |
| A419 | 419 | 474.9 |  | 58.4 |
| A420 | 420 | 475.9 |  | 58.3 |
| A421 | 421 | 476.9 |  | 58.3 |
| A422 | 422 | 477.9 |  | 58.3 |
| A423 | 423 | 478.9 |  | 58.3 |
| A424 | 424 | 479.9 |  | 58.3 |
| A425 | 425 | 480.9 |  | 58.3 |
| A426 | 426 | 481.9 |  | 58.3 |
| A427 | 427 | 482.9 |  | 58.3 |
| A428 | 428 | 483.9 |  | 58.2 |
| A429 | 429 | 484.9 |  | 58.2 |
| A430 | 430 | 485.9 |  | 58.2 |
| A431 | 431 | 486.9 |  | 58.2 |
| A432 | 432 | 487.9 |  | 58.2 |
| A433 | 433 | 488.9 |  | 58.2 |
| A434 | 434 | 489.9 |  | 58.2 |
| A435 | 435 | 490.9 |  | 58.1 |
| A436 | 436 | 491.9 |  | 58.1 |
| A437 | 437 | 492.9 |  | 58.1 |
| A438 | 438 | 493.9 |  | 58.1 |
| A439 | 439 | 494.9 |  | 58.1 |
| A440 | 440 | 495.9 |  | 58.1 |
| A441 | 441 | 496.9 |  | 58.1 |
| A442 | 442 | 497.9 |  | 58.1 |
| A443 | 443 | 498.9 |  | 58.0 |
| A444 | 444 | 499.9 |  | 58.0 |
| A445 | 445 | 500.9 |  | 58.0 |
| A446 | 446 | 501.9 |  | 58.0 |
| A447 | 447 | 502.9 |  | 58.0 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| Southbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 50 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 25 |
| w: Width of Structure |  |  |  | 100 |
| Mw: Midpoint of structure (w/2) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 50 |
| Dref: Reference distance - from S to Aref |  |  |  | 55.9 |
| Measured Noise Level at Drip Edge, $\mathrm{dB}(\mathrm{A})$ |  |  |  | 72.3 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from <br> Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in dB(A) | ```Calculated Noise Level Drop-off Rate = 4.5 dB/DD``` |
| A448 | 448 | 503.9 |  | 58.0 |
| A449 | 449 | 504.9 |  | 58.0 |
| A450 | 450 | 505.9 |  | 58.0 |
| A451 | 451 | 506.9 |  | 57.9 |
| A452 | 452 | 507.9 |  | 57.9 |
| A453 | 453 | 508.9 |  | 57.9 |
| A454 | 454 | 509.9 |  | 57.9 |
| A455 | 455 | 510.9 |  | 57.9 |
| A456 | 456 | 511.9 |  | 57.9 |
| A457 | 457 | 512.9 |  | 57.9 |
| A458 | 458 | 513.9 |  | 57.8 |
| A459 | 459 | 514.9 |  | 57.8 |
| A460 | 460 | 515.9 |  | 57.8 |
| A461 | 461 | 516.9 |  | 57.8 |
| A462 | 462 | 517.9 |  | 57.8 |
| A463 | 463 | 518.9 |  | 57.8 |
| A464 | 464 | 519.9 |  | 57.8 |
| A465 | 465 | 520.9 |  | 57.8 |
| A466 | 466 | 521.9 |  | 57.7 |
| A467 | 467 | 522.9 |  | 57.7 |
| A468 | 468 | 523.9 |  | 57.7 |
| A469 | 469 | 524.9 |  | 57.7 |
| A470 | 470 | 525.9 |  | 57.7 |
| A471 | 471 | 526.9 |  | 57.7 |
| A472 | 472 | 527.9 |  | 57.7 |
| A473 | 473 | 528.9 |  | 57.7 |
| A474 | 474 | 529.9 |  | 57.6 |
| A475 | 475 | 530.9 |  | 57.6 |
| A476 | 476 | 531.9 |  | 57.6 |
| A477 | 477 | 532.9 |  | 57.6 |
| A478 | 478 | 533.9 |  | 57.6 |
| A479 | 479 | 534.9 |  | 57.6 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| Southbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 50 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 25 |
| w: Width of Structure |  |  |  | 100 |
| Mw: Midpoint of structure (w/2) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 50 |
| Dref: Reference distance - from S to Aref |  |  |  | 55.9 |
| Measured Noise Level at Drip Edge, dB(A) |  |  |  | 72.3 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from <br> Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in dB(A) | ```Calculated Noise Level Drop-off Rate = 4.5 dB/DD``` |
| A480 | 480 | 535.9 |  | 57.6 |
| A481 | 481 | 536.9 |  | 57.6 |
| A482 | 482 | 537.9 |  | 57.6 |
| A483 | 483 | 538.9 |  | 57.5 |
| A484 | 484 | 539.9 |  | 57.5 |
| A485 | 485 | 540.9 |  | 57.5 |
| A486 | 486 | 541.9 |  | 57.5 |
| A487 | 487 | 542.9 |  | 57.5 |
| A488 | 488 | 543.9 |  | 57.5 |
| A489 | 489 | 544.9 |  | 57.5 |
| A490 | 490 | 545.9 |  | 57.5 |
| A491 | 491 | 546.9 |  | 57.4 |
| A492 | 492 | 547.9 |  | 57.4 |
| A493 | 493 | 548.9 |  | 57.4 |
| A494 | 494 | 549.9 |  | 57.4 |
| A495 | 495 | 550.9 |  | 57.4 |
| A496 | 496 | 551.9 |  | 57.4 |
| A497 | 497 | 552.9 |  | 57.4 |
| A498 | 498 | 553.9 |  | 57.4 |
| A499 | 499 | 554.9 |  | 57.3 |
| A500 | 500 | 555.9 |  | 57.3 |

## SHORT-TERIVI NOISE IVIEASUREIVENT SITE LOG

ASSESSMENT AREA: $\omega L$ side MEASUREMENT SITE NO: $\omega L$ \&trcutur Burke ADDRESS:

OWNER:
DESCRIPTION:
NOISE SOURCES:
NOISE MONITOR:
MICROPHONE:
CALIBRATOR:
TEMP. RANGE ( $\left.{ }^{\circ} \mathrm{F}\right)$ : west Linn (WL) Sade of Abranetuy Barde Crossly
west Un n
Pod Trail/ ROW OBOT
I-205
$\frac{\frac{13+K 2250}{13+K}}{\frac{13+K}{65^{\circ}}}$

S/N: kits $4,5,6$
SIN: $\qquad$
SIN:
$\qquad$

SITE SKETCH: Show roadway, homes, local roads, reference distances, arrows for North \& wind direction, where roadway is in cut, at grade, elevated, where direct lines of sight exist.


PHOTOS: $/ E 5$
GPS COORDINATES: $N / A$ STE GAS MAP

PROJECT: K19786:I-205CWV
JOB NO.: 309180.000

MEASUREMENT SITE NO.: West in^ Structure Bar me Noise ADDRESSIDESCRIPTION: West linn Side of Crossing

PERSONNEL: RN
DATE: $6 / 13 / 18-6 / 19 / 18$


TOTAL Leq =
$V=$ Other sources contributed to Led

SUBSET Req =
X $=$ Exclude period - contaminated by non-characteristic sources
>> ADD SKETCH AND WEATHER CONDITIONS TO REVERSE OR OTHER SHEET <<

West Linn- Structure-Borne Noise Measurements


Drip Edge


Drip Edge View 2


50 Feet


85 feet


120 feet

| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| West Linn Abernethy Bridge Northbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 85 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 42.5 |
| w: Width of Structure |  |  |  | 140 |
| Mw: Midpoint of structure (w/2) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 70 |
| Dref: Reference distance - from S to Aref |  |  |  | 81.9 |
| Measured Noise Level at Drip Edge, dB(A) |  |  |  | 67.1 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from <br> Drip Edge (ft.) | Distance from <br> Analysis Point <br> (ft.) | Measured Noise Level at Drip Edge Leq in $\mathrm{dB}(\mathrm{A})$ | Calculated <br> Noise Level <br> Drop-off Rate $=3.0 \mathrm{~dB} / \mathrm{DD}$ |
| Aref | 0 | 81.9 | 67.1 |  |
| A25 | 25 | 106.9 |  | 65.9 |
| A50 | 50 | 131.9 |  | 65.0 |
| A85 | 85 | 166.9 |  | 64.0 |
| A150 | 150 | 231.9 |  | 62.6 |
| A200 | 200 | 281.9 |  | 61.7 |
| A400 | 400 | 481.9 |  | 59.4 |
| A500 | 500 | 581.9 |  | 58.6 |
| Analysis Point | Distance from <br> Drip Edge (ft.) | Distance from <br> Analysis Point <br> (ft.) | Measured Noise Level at Drip Edge Leq in $\mathrm{dB}(\mathrm{A})$ | Calculated Noise Level Drop-off Rate $=4.0 \mathrm{~dB} / \mathrm{DD}$ |
| Aref | 0 | 81.9 | 67.1 |  |
| A25 | 25 | 106.9 |  | 65.4 |
| A50 | 50 | 131.9 |  | 64.0 |
| A85 | 85 | 166.9 |  | 62.5 |
| A200 | 200 | 281.9 |  | 59.0 |
| A400 | 400 | 481.9 |  | 55.6 |
| A500 | 500 | 581.9 |  | 54.3 |
| Analysis Point | Distance from <br> Drip Edge (ft.) | Distance from <br> Analysis Point <br> (ft.) | Measured Noise Level at Drip Edge Leq in $\mathrm{dB}(\mathrm{A})$ | Calculated Noise Level Drop-off Rate $=6.0 \mathrm{~dB} / \mathrm{DD}$ |
| Aref | 0 | 81.9 | 67.1 |  |
| A25 | 25 | 106.9 |  | 65 |
| A50 | 50 | 131.9 |  | 63 |
| A85 | 85 | 166.9 |  | 61 |
| A200 | 200 | 281.9 |  | 56 |
| A400 | 400 | 481.9 |  | 52 |
| A500 | 500 | 581.9 |  | 50 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| West Linn Abernethy Bridge Northbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 85 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 42.5 |
| w: Width of Structure |  |  |  | 140 |
| Mw : Midpoint of structure (w/2) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 70 |
| Dref: Reference distance - from S to Aref |  |  |  | 81.9 |
| Measured Noise Level at Drip Edge, $\mathrm{dB}(\mathrm{A})$ |  |  |  | 67.1 |
| Set-back Calculations: |  |  |  |  |
|  | Distance from Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in $\mathrm{dB}(\mathrm{A})$ | Calculated Noise Level Drop-off Rate $=4.5$ dB/DD |
| Analysis Point <br> Aref <br> A1 | 0 | 81.9 | 67.1 |  |
| A1 | 1 | 82.9 |  | 67.0 |
| A2 | 2 | 83.9 |  | 66.9 |
| A3 | 3 | 84.9 |  | 66.9 |
| A4 | 4 | 85.9 |  | 66.8 |
| A5 | 5 | 86.9 |  | 66.7 |
| A6 | 6 | 87.9 |  | 66.6 |
| A7 | 7 | 88.9 |  | 66.6 |
| A8 | 8 | 89.9 |  | 66.5 |
| A9 | 9 | 90.9 |  | 66.4 |
| A10 | 10 | 91.9 |  | 66.3 |
| A11 | 11 | 92.9 |  | 66.3 |
| A12 | 12 | 93.9 |  | 66.2 |
| A13 | 13 | 94.9 |  | 66.1 |
| A14 | 14 | 95.9 |  | 66.1 |
| A15 | 15 | 96.9 |  | 66.0 |
| A16 | 16 | 97.9 |  | 65.9 |
| A17 | 17 | 98.9 |  | 65.9 |
| A18 | 18 | 99.9 |  | 65.8 |
| A19 | 19 | 100.9 |  | 65.7 |
| A20 | 20 | 101.9 |  | 65.7 |
| A21 | 21 | 102.9 |  | 65.6 |
| A22 | 22 | 103.9 |  | 65.5 |
| A23 | 23 | 104.9 |  | 65.5 |
| A24 | 24 | 105.9 |  | 65.4 |
| A25 | 25 | 106.9 |  | 65.4 |
| A26 | 26 | 107.9 |  | 65.3 |
| A27 | 27 | 108.9 |  | 65.2 |
| A28 | 28 | 109.9 |  | 65.2 |
| A29 | 29 | 110.9 |  | 65.1 |
| A30 | 30 | 111.9 |  | 65.1 |
| A31 | 31 | 112.9 |  | 65.0 |
| A32 | 32 | 113.9 |  | 65.0 |
| A33 | 33 | 114.9 |  | 64.9 |
| A34 | 34 | 115.9 |  | 64.8 |
| A35 | 35 | 116.9 |  | 64.8 |
| A36 | 36 | 117.9 |  | 64.7 |
| A37 | 37 | 118.9 |  | 64.7 |
| A38 | 38 | 119.9 |  | 64.6 |
| A39 | 39 | 120.9 |  | 64.6 |
| A40 | 40 | 121.9 |  | 64.5 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| West Linn Abernethy Bridge Northbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 85 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 42.5 |
| w: Width of Structure |  |  |  | 140 |
| Mw : Midpoint of structure ( $\mathrm{w} / 2$ ) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 70 |
| Dref: Reference distance - from S to Aref |  |  |  | 81.9 |
| Measured Noise Level at Drip Edge, $\mathrm{dB}(\mathrm{A})$ |  |  |  | 67.1 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in dB(A) | Calculated Noise Level Drop-off Rate $=4.5$ dB/DD |
| A41 | 41 | 122.9 |  | 64.5 |
| A42 | 42 | 123.9 |  | 64.4 |
| A43 | 43 | 124.9 |  | 64.4 |
| A44 | 44 | 125.9 |  | 64.3 |
| A45 | 45 | 126.9 |  | 64.2 |
| A46 | 46 | 127.9 |  | 64.2 |
| A47 | 47 | 128.9 |  | 64.1 |
| A48 | 48 | 129.9 |  | 64.1 |
| A49 | 49 | 130.9 |  | 64.0 |
| A50 | 50 | 131.9 |  | 64.0 |
| A51 | 51 | 132.9 |  | 63.9 |
| A52 | 52 | 133.9 |  | 63.9 |
| A53 | 53 | 134.9 |  | 63.8 |
| A54 | 54 | 135.9 |  | 63.8 |
| A55 | 55 | 136.9 |  | 63.8 |
| A56 | 56 | 137.9 |  | 63.7 |
| A57 | 57 | 138.9 |  | 63.7 |
| A58 | 58 | 139.9 |  | 63.6 |
| A59 | 59 | 140.9 |  | 63.6 |
| A60 | 60 | 141.9 |  | 63.5 |
| A61 | 61 | 142.9 |  | 63.5 |
| A62 | 62 | 143.9 |  | 63.4 |
| A63 | 63 | 144.9 |  | 63.4 |
| A64 | 64 | 145.9 |  | 63.3 |
| A65 | 65 | 146.9 |  | 63.3 |
| A66 | 66 | 147.9 |  | 63.2 |
| A67 | 67 | 148.9 |  | 63.2 |
| A68 | 68 | 149.9 |  | 63.2 |
| A69 | 69 | 150.9 |  | 63.1 |
| A70 | 70 | 151.9 |  | 63.1 |
| A71 | 71 | 152.9 |  | 63.0 |
| A72 | 72 | 153.9 |  | 63.0 |
| A73 | 73 | 154.9 |  | 62.9 |
| A74 | 74 | 155.9 |  | 62.9 |
| A75 | 75 | 156.9 |  | 62.9 |
| A76 | 76 | 157.9 |  | 62.8 |
| A77 | 77 | 158.9 |  | 62.8 |
| A78 | 78 | 159.9 |  | 62.7 |
| A79 | 79 | 160.9 |  | 62.7 |
| A80 | 80 | 161.9 |  | 62.7 |
| A81 | 81 | 162.9 |  | 62.6 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| West Linn Abernethy Bridge Northbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 85 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 42.5 |
| w: Width of Structure |  |  |  | 140 |
| Mw : Midpoint of structure ( $\mathrm{w} / 2$ ) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 70 |
| Dref: Reference distance - from S to Aref |  |  |  | 81.9 |
| Measured Noise Level at Drip Edge, $\mathrm{dB}(\mathrm{A})$ |  |  |  | 67.1 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in dB(A) | Calculated Noise Level Drop-off Rate $=4.5$ dB/DD |
| A82 | 82 | 163.9 |  | 62.6 |
| A83 | 83 | 164.9 |  | 62.5 |
| A84 | 84 | 165.9 |  | 62.5 |
| A85 | 85 | 166.9 |  | 62.5 |
| A86 | 86 | 167.9 |  | 62.4 |
| A87 | 87 | 168.9 |  | 62.4 |
| A88 | 88 | 169.9 |  | 62.3 |
| A89 | 89 | 170.9 |  | 62.3 |
| A90 | 90 | 171.9 |  | 62.3 |
| A91 | 91 | 172.9 |  | 62.2 |
| A92 | 92 | 173.9 |  | 62.2 |
| A93 | 93 | 174.9 |  | 62.2 |
| A94 | 94 | 175.9 |  | 62.1 |
| A95 | 95 | 176.9 |  | 62.1 |
| A96 | 96 | 177.9 |  | 62.0 |
| A97 | 97 | 178.9 |  | 62.0 |
| A98 | 98 | 179.9 |  | 62.0 |
| A99 | 99 | 180.9 |  | 61.9 |
| A100 | 100 | 181.9 |  | 61.9 |
| A101 | 101 | 182.9 |  | 61.9 |
| A102 | 102 | 183.9 |  | 61.8 |
| A103 | 103 | 184.9 |  | 61.8 |
| A104 | 104 | 185.9 |  | 61.8 |
| A105 | 105 | 186.9 |  | 61.7 |
| A106 | 106 | 187.9 |  | 61.7 |
| A107 | 107 | 188.9 |  | 61.7 |
| A108 | 108 | 189.9 |  | 61.6 |
| A109 | 109 | 190.9 |  | 61.6 |
| A110 | 110 | 191.9 |  | 61.6 |
| A111 | 111 | 192.9 |  | 61.5 |
| A112 | 112 | 193.9 |  | 61.5 |
| A113 | 113 | 194.9 |  | 61.5 |
| A114 | 114 | 195.9 |  | 61.4 |
| A115 | 115 | 196.9 |  | 61.4 |
| A116 | 116 | 197.9 |  | 61.4 |
| A117 | 117 | 198.9 |  | 61.3 |
| A118 | 118 | 199.9 |  | 61.3 |
| A119 | 119 | 200.9 |  | 61.3 |
| A120 | 120 | 201.9 |  | 61.2 |
| A121 | 121 | 202.9 |  | 61.2 |
| A122 | 122 | 203.9 |  | 61.2 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| West Linn Abernethy Bridge Northbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 85 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 42.5 |
| w: Width of Structure |  |  |  | 140 |
| Mw : Midpoint of structure (w/2) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 70 |
| Dref: Reference distance - from S to Aref |  |  |  | 81.9 |
| Measured Noise Level at Drip Edge, $\mathrm{dB}(\mathrm{A})$ |  |  |  | 67.1 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in dB(A) | Calculated Noise Level Drop-off Rate $=4.5$ dB/DD |
| A123 | 123 | 204.9 |  | 61.1 |
| A124 | 124 | 205.9 |  | 61.1 |
| A125 | 125 | 206.9 |  | 61.1 |
| A126 | 126 | 207.9 |  | 61.0 |
| A127 | 127 | 208.9 |  | 61.0 |
| A128 | 128 | 209.9 |  | 61.0 |
| A129 | 129 | 210.9 |  | 60.9 |
| A130 | 130 | 211.9 |  | 60.9 |
| A131 | 131 | 212.9 |  | 60.9 |
| A132 | 132 | 213.9 |  | 60.8 |
| A133 | 133 | 214.9 |  | 60.8 |
| A134 | 134 | 215.9 |  | 60.8 |
| A135 | 135 | 216.9 |  | 60.8 |
| A136 | 136 | 217.9 |  | 60.7 |
| A137 | 137 | 218.9 |  | 60.7 |
| A138 | 138 | 219.9 |  | 60.7 |
| A139 | 139 | 220.9 |  | 60.6 |
| A140 | 140 | 221.9 |  | 60.6 |
| A141 | 141 | 222.9 |  | 60.6 |
| A142 | 142 | 223.9 |  | 60.5 |
| A143 | 143 | 224.9 |  | 60.5 |
| A144 | 144 | 225.9 |  | 60.5 |
| A145 | 145 | 226.9 |  | 60.5 |
| A146 | 146 | 227.9 |  | 60.4 |
| A147 | 147 | 228.9 |  | 60.4 |
| A148 | 148 | 229.9 |  | 60.4 |
| A149 | 149 | 230.9 |  | 60.3 |
| A150 | 150 | 231.9 |  | 60.3 |
| A151 | 151 | 232.9 |  | 60.3 |
| A152 | 152 | 233.9 |  | 60.3 |
| A153 | 153 | 234.9 |  | 60.2 |
| A154 | 154 | 235.9 |  | 60.2 |
| A155 | 155 | 236.9 |  | 60.2 |
| A156 | 156 | 237.9 |  | 60.2 |
| A157 | 157 | 238.9 |  | 60.1 |
| A158 | 158 | 239.9 |  | 60.1 |
| A159 | 159 | 240.9 |  | 60.1 |
| A160 | 160 | 241.9 |  | 60.0 |
| A161 | 161 | 242.9 |  | 60.0 |
| A162 | 162 | 243.9 |  | 60.0 |
| A163 | 163 | 244.9 |  | 60.0 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| West Linn Abernethy Bridge Northbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 85 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 42.5 |
| w: Width of Structure |  |  |  | 140 |
| Mw : Midpoint of structure ( $\mathrm{w} / 2$ ) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 70 |
| Dref: Reference distance - from S to Aref |  |  |  | 81.9 |
| Measured Noise Level at Drip Edge, $\mathrm{dB}(\mathrm{A})$ |  |  |  | 67.1 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in dB(A) | Calculated Noise Level <br> Drop-off Rate $=4.5$ dB/DD |
| A164 | 164 | 245.9 |  | 59.9 |
| A165 | 165 | 246.9 |  | 59.9 |
| A166 | 166 | 247.9 |  | 59.9 |
| A167 | 167 | 248.9 |  | 59.9 |
| A168 | 168 | 249.9 |  | 59.8 |
| A169 | 169 | 250.9 |  | 59.8 |
| A170 | 170 | 251.9 |  | 59.8 |
| A171 | 171 | 252.9 |  | 59.8 |
| A172 | 172 | 253.9 |  | 59.7 |
| A173 | 173 | 254.9 |  | 59.7 |
| A174 | 174 | 255.9 |  | 59.7 |
| A175 | 175 | 256.9 |  | 59.7 |
| A176 | 176 | 257.9 |  | 59.6 |
| A177 | 177 | 258.9 |  | 59.6 |
| A178 | 178 | 259.9 |  | 59.6 |
| A179 | 179 | 260.9 |  | 59.6 |
| A180 | 180 | 261.9 |  | 59.5 |
| A181 | 181 | 262.9 |  | 59.5 |
| A182 | 182 | 263.9 |  | 59.5 |
| A183 | 183 | 264.9 |  | 59.5 |
| A184 | 184 | 265.9 |  | 59.4 |
| A185 | 185 | 266.9 |  | 59.4 |
| A186 | 186 | 267.9 |  | 59.4 |
| A187 | 187 | 268.9 |  | 59.4 |
| A188 | 188 | 269.9 |  | 59.3 |
| A189 | 189 | 270.9 |  | 59.3 |
| A190 | 190 | 271.9 |  | 59.3 |
| A191 | 191 | 272.9 |  | 59.3 |
| A192 | 192 | 273.9 |  | 59.2 |
| A193 | 193 | 274.9 |  | 59.2 |
| A194 | 194 | 275.9 |  | 59.2 |
| A195 | 195 | 276.9 |  | 59.2 |
| A196 | 196 | 277.9 |  | 59.1 |
| A197 | 197 | 278.9 |  | 59.1 |
| A198 | 198 | 279.9 |  | 59.1 |
| A199 | 199 | 280.9 |  | 59.1 |
| A200 | 200 | 281.9 |  | 59.0 |
| A201 | 201 | 282.9 |  | 59.0 |
| A202 | 202 | 283.9 |  | 59.0 |
| A203 | 203 | 284.9 |  | 59.0 |
| A204 | 204 | 285.9 |  | 59.0 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| West Linn Abernethy Bridge Northbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 85 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 42.5 |
| w: Width of Structure |  |  |  | 140 |
| Mw : Midpoint of structure ( $\mathrm{w} / 2$ ) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 70 |
| Dref: Reference distance - from S to Aref |  |  |  | 81.9 |
| Measured Noise Level at Drip Edge, $\mathrm{dB}(\mathrm{A})$ |  |  |  | 67.1 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in dB(A) | Calculated Noise Level Drop-off Rate $=4.5$ dB/DD |
| A205 | 205 | 286.9 |  | 58.9 |
| A206 | 206 | 287.9 |  | 58.9 |
| A207 | 207 | 288.9 |  | 58.9 |
| A208 | 208 | 289.9 |  | 58.9 |
| A209 | 209 | 290.9 |  | 58.8 |
| A210 | 210 | 291.9 |  | 58.8 |
| A211 | 211 | 292.9 |  | 58.8 |
| A212 | 212 | 293.9 |  | 58.8 |
| A213 | 213 | 294.9 |  | 58.8 |
| A214 | 214 | 295.9 |  | 58.7 |
| A215 | 215 | 296.9 |  | 58.7 |
| A216 | 216 | 297.9 |  | 58.7 |
| A217 | 217 | 298.9 |  | 58.7 |
| A218 | 218 | 299.9 |  | 58.6 |
| A219 | 219 | 300.9 |  | 58.6 |
| A220 | 220 | 301.9 |  | 58.6 |
| A221 | 221 | 302.9 |  | 58.6 |
| A222 | 222 | 303.9 |  | 58.6 |
| A223 | 223 | 304.9 |  | 58.5 |
| A224 | 224 | 305.9 |  | 58.5 |
| A225 | 225 | 306.9 |  | 58.5 |
| A226 | 226 | 307.9 |  | 58.5 |
| A227 | 227 | 308.9 |  | 58.5 |
| A228 | 228 | 309.9 |  | 58.4 |
| A229 | 229 | 310.9 |  | 58.4 |
| A230 | 230 | 311.9 |  | 58.4 |
| A231 | 231 | 312.9 |  | 58.4 |
| A232 | 232 | 313.9 |  | 58.3 |
| A233 | 233 | 314.9 |  | 58.3 |
| A234 | 234 | 315.9 |  | 58.3 |
| A235 | 235 | 316.9 |  | 58.3 |
| A236 | 236 | 317.9 |  | 58.3 |
| A237 | 237 | 318.9 |  | 58.2 |
| A238 | 238 | 319.9 |  | 58.2 |
| A239 | 239 | 320.9 |  | 58.2 |
| A240 | 240 | 321.9 |  | 58.2 |
| A241 | 241 | 322.9 |  | 58.2 |
| A242 | 242 | 323.9 |  | 58.1 |
| A243 | 243 | 324.9 |  | 58.1 |
| A244 | 244 | 325.9 |  | 58.1 |
| A245 | 245 | 326.9 |  | 58.1 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| West Linn Abernethy Bridge Northbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 85 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 42.5 |
| w: Width of Structure |  |  |  | 140 |
| Mw : Midpoint of structure ( $\mathrm{w} / 2$ ) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 70 |
| Dref: Reference distance - from S to Aref |  |  |  | 81.9 |
| Measured Noise Level at Drip Edge, $\mathrm{dB}(\mathrm{A})$ |  |  |  | 67.1 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in dB(A) | Calculated Noise Level Drop-off Rate $=4.5$ dB/DD |
| A246 | 246 | 327.9 |  | 58.1 |
| A247 | 247 | 328.9 |  | 58.0 |
| A248 | 248 | 329.9 |  | 58.0 |
| A249 | 249 | 330.9 |  | 58.0 |
| A250 | 250 | 331.9 |  | 58.0 |
| A251 | 251 | 332.9 |  | 58.0 |
| A252 | 252 | 333.9 |  | 57.9 |
| A253 | 253 | 334.9 |  | 57.9 |
| A254 | 254 | 335.9 |  | 57.9 |
| A255 | 255 | 336.9 |  | 57.9 |
| A256 | 256 | 337.9 |  | 57.9 |
| A257 | 257 | 338.9 |  | 57.8 |
| A258 | 258 | 339.9 |  | 57.8 |
| A259 | 259 | 340.9 |  | 57.8 |
| A260 | 260 | 341.9 |  | 57.8 |
| A261 | 261 | 342.9 |  | 57.8 |
| A262 | 262 | 343.9 |  | 57.8 |
| A263 | 263 | 344.9 |  | 57.7 |
| A264 | 264 | 345.9 |  | 57.7 |
| A265 | 265 | 346.9 |  | 57.7 |
| A266 | 266 | 347.9 |  | 57.7 |
| A267 | 267 | 348.9 |  | 57.7 |
| A268 | 268 | 349.9 |  | 57.6 |
| A269 | 269 | 350.9 |  | 57.6 |
| A270 | 270 | 351.9 |  | 57.6 |
| A271 | 271 | 352.9 |  | 57.6 |
| A272 | 272 | 353.9 |  | 57.6 |
| A273 | 273 | 354.9 |  | 57.5 |
| A274 | 274 | 355.9 |  | 57.5 |
| A275 | 275 | 356.9 |  | 57.5 |
| A276 | 276 | 357.9 |  | 57.5 |
| A277 | 277 | 358.9 |  | 57.5 |
| A278 | 278 | 359.9 |  | 57.5 |
| A279 | 279 | 360.9 |  | 57.4 |
| A280 | 280 | 361.9 |  | 57.4 |
| A281 | 281 | 362.9 |  | 57.4 |
| A282 | 282 | 363.9 |  | 57.4 |
| A283 | 283 | 364.9 |  | 57.4 |
| A284 | 284 | 365.9 |  | 57.3 |
| A285 | 285 | 366.9 |  | 57.3 |
| A286 | 286 | 367.9 |  | 57.3 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| West Linn Abernethy Bridge Northbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 85 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 42.5 |
| w: Width of Structure |  |  |  | 140 |
| Mw : Midpoint of structure ( $\mathrm{w} / 2$ ) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 70 |
| Dref: Reference distance - from S to Aref |  |  |  | 81.9 |
| Measured Noise Level at Drip Edge, $\mathrm{dB}(\mathrm{A})$ |  |  |  | 67.1 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in dB(A) | $\begin{gathered} \text { Calculated Noise Level } \\ \text { Drop-off Rate = } 4.5 \\ \text { dB/DD } \end{gathered}$ |
| A287 | 287 | 368.9 |  | 57.3 |
| A288 | 288 | 369.9 |  | 57.3 |
| A289 | 289 | 370.9 |  | 57.3 |
| A290 | 290 | 371.9 |  | 57.2 |
| A291 | 291 | 372.9 |  | 57.2 |
| A292 | 292 | 373.9 |  | 57.2 |
| A293 | 293 | 374.9 |  | 57.2 |
| A294 | 294 | 375.9 |  | 57.2 |
| A295 | 295 | 376.9 |  | 57.2 |
| A296 | 296 | 377.9 |  | 57.1 |
| A297 | 297 | 378.9 |  | 57.1 |
| A298 | 298 | 379.9 |  | 57.1 |
| A299 | 299 | 380.9 |  | 57.1 |
| A300 | 300 | 381.9 |  | 57.1 |
| A301 | 301 | 382.9 |  | 57.1 |
| A302 | 302 | 383.9 |  | 57.0 |
| A303 | 303 | 384.9 |  | 57.0 |
| A304 | 304 | 385.9 |  | 57.0 |
| A305 | 305 | 386.9 |  | 57.0 |
| A306 | 306 | 387.9 |  | 57.0 |
| A307 | 307 | 388.9 |  | 57.0 |
| A308 | 308 | 389.9 |  | 56.9 |
| A309 | 309 | 390.9 |  | 56.9 |
| A310 | 310 | 391.9 |  | 56.9 |
| A311 | 311 | 392.9 |  | 56.9 |
| A312 | 312 | 393.9 |  | 56.9 |
| A313 | 313 | 394.9 |  | 56.9 |
| A314 | 314 | 395.9 |  | 56.8 |
| A315 | 315 | 396.9 |  | 56.8 |
| A316 | 316 | 397.9 |  | 56.8 |
| A317 | 317 | 398.9 |  | 56.8 |
| A318 | 318 | 399.9 |  | 56.8 |
| A319 | 319 | 400.9 |  | 56.8 |
| A320 | 320 | 401.9 |  | 56.7 |
| A321 | 321 | 402.9 |  | 56.7 |
| A322 | 322 | 403.9 |  | 56.7 |
| A323 | 323 | 404.9 |  | 56.7 |
| A324 | 324 | 405.9 |  | 56.7 |
| A325 | 325 | 406.9 |  | 56.7 |
| A326 | 326 | 407.9 |  | 56.6 |
| A327 | 327 | 408.9 |  | 56.6 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| West Linn Abernethy Bridge Northbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 85 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 42.5 |
| w: Width of Structure |  |  |  | 140 |
| Mw : Midpoint of structure ( $\mathrm{w} / 2$ ) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 70 |
| Dref: Reference distance - from S to Aref |  |  |  | 81.9 |
| Measured Noise Level at Drip Edge, $\mathrm{dB}(\mathrm{A})$ |  |  |  | 67.1 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in dB(A) | $\begin{gathered} \text { Calculated Noise Level } \\ \text { Drop-off Rate = } 4.5 \\ \text { dB/DD } \\ \hline \end{gathered}$ |
| A328 | 328 | 409.9 |  | 56.6 |
| A329 | 329 | 410.9 |  | 56.6 |
| A330 | 330 | 411.9 |  | 56.6 |
| A331 | 331 | 412.9 |  | 56.6 |
| A332 | 332 | 413.9 |  | 56.5 |
| A333 | 333 | 414.9 |  | 56.5 |
| A334 | 334 | 415.9 |  | 56.5 |
| A335 | 335 | 416.9 |  | 56.5 |
| A336 | 336 | 417.9 |  | 56.5 |
| A337 | 337 | 418.9 |  | 56.5 |
| A338 | 338 | 419.9 |  | 56.5 |
| A339 | 339 | 420.9 |  | 56.4 |
| A340 | 340 | 421.9 |  | 56.4 |
| A341 | 341 | 422.9 |  | 56.4 |
| A342 | 342 | 423.9 |  | 56.4 |
| A343 | 343 | 424.9 |  | 56.4 |
| A344 | 344 | 425.9 |  | 56.4 |
| A345 | 345 | 426.9 |  | 56.3 |
| A346 | 346 | 427.9 |  | 56.3 |
| A347 | 347 | 428.9 |  | 56.3 |
| A348 | 348 | 429.9 |  | 56.3 |
| A349 | 349 | 430.9 |  | 56.3 |
| A350 | 350 | 431.9 |  | 56.3 |
| A351 | 351 | 432.9 |  | 56.3 |
| A352 | 352 | 433.9 |  | 56.2 |
| A353 | 353 | 434.9 |  | 56.2 |
| A354 | 354 | 435.9 |  | 56.2 |
| A355 | 355 | 436.9 |  | 56.2 |
| A356 | 356 | 437.9 |  | 56.2 |
| A357 | 357 | 438.9 |  | 56.2 |
| A358 | 358 | 439.9 |  | 56.1 |
| A359 | 359 | 440.9 |  | 56.1 |
| A360 | 360 | 441.9 |  | 56.1 |
| A361 | 361 | 442.9 |  | 56.1 |
| A362 | 362 | 443.9 |  | 56.1 |
| A363 | 363 | 444.9 |  | 56.1 |
| A364 | 364 | 445.9 |  | 56.1 |
| A365 | 365 | 446.9 |  | 56.0 |
| A366 | 366 | 447.9 |  | 56.0 |
| A367 | 367 | 448.9 |  | 56.0 |
| A368 | 368 | 449.9 |  | 56.0 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| West Linn Abernethy Bridge Northbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 85 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 42.5 |
| w: Width of Structure |  |  |  | 140 |
| Mw : Midpoint of structure ( $\mathrm{w} / 2$ ) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 70 |
| Dref: Reference distance - from S to Aref |  |  |  | 81.9 |
| Measured Noise Level at Drip Edge, $\mathrm{dB}(\mathrm{A})$ |  |  |  | 67.1 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in dB(A) | Calculated Noise Level Drop-off Rate $=4.5$ dB/DD |
| A369 | 369 | 450.9 |  | 56.0 |
| A370 | 370 | 451.9 |  | 56.0 |
| A371 | 371 | 452.9 |  | 56.0 |
| A372 | 372 | 453.9 |  | 55.9 |
| A373 | 373 | 454.9 |  | 55.9 |
| A374 | 374 | 455.9 |  | 55.9 |
| A375 | 375 | 456.9 |  | 55.9 |
| A376 | 376 | 457.9 |  | 55.9 |
| A377 | 377 | 458.9 |  | 55.9 |
| A378 | 378 | 459.9 |  | 55.9 |
| A379 | 379 | 460.9 |  | 55.8 |
| A380 | 380 | 461.9 |  | 55.8 |
| A381 | 381 | 462.9 |  | 55.8 |
| A382 | 382 | 463.9 |  | 55.8 |
| A383 | 383 | 464.9 |  | 55.8 |
| A384 | 384 | 465.9 |  | 55.8 |
| A385 | 385 | 466.9 |  | 55.8 |
| A386 | 386 | 467.9 |  | 55.7 |
| A387 | 387 | 468.9 |  | 55.7 |
| A388 | 388 | 469.9 |  | 55.7 |
| A389 | 389 | 470.9 |  | 55.7 |
| A390 | 390 | 471.9 |  | 55.7 |
| A391 | 391 | 472.9 |  | 55.7 |
| A392 | 392 | 473.9 |  | 55.7 |
| A393 | 393 | 474.9 |  | 55.6 |
| A394 | 394 | 475.9 |  | 55.6 |
| A395 | 395 | 476.9 |  | 55.6 |
| A396 | 396 | 477.9 |  | 55.6 |
| A397 | 397 | 478.9 |  | 55.6 |
| A398 | 398 | 479.9 |  | 55.6 |
| A399 | 399 | 480.9 |  | 55.6 |
| A400 | 400 | 481.9 |  | 55.6 |
| A401 | 401 | 482.9 |  | 55.5 |
| A402 | 402 | 483.9 |  | 55.5 |
| A403 | 403 | 484.9 |  | 55.5 |
| A404 | 404 | 485.9 |  | 55.5 |
| A405 | 405 | 486.9 |  | 55.5 |
| A406 | 406 | 487.9 |  | 55.5 |
| A407 | 407 | 488.9 |  | 55.5 |
| A408 | 408 | 489.9 |  | 55.4 |
| A409 | 409 | 490.9 |  | 55.4 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| West Linn Abernethy Bridge Northbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 85 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 42.5 |
| w: Width of Structure |  |  |  | 140 |
| Mw: Midpoint of structure (w/2) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 70 |
| Dref: Reference distance - from S to Aref |  |  |  | 81.9 |
| Measured Noise Level at Drip Edge, $\mathrm{dB}(\mathrm{A})$ |  |  |  | 67.1 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in dB(A) | Calculated Noise Level Drop-off Rate $=4.5$ dB/DD |
| A410 | 410 | 491.9 |  | 55.4 |
| A411 | 411 | 492.9 |  | 55.4 |
| A412 | 412 | 493.9 |  | 55.4 |
| A413 | 413 | 494.9 |  | 55.4 |
| A414 | 414 | 495.9 |  | 55.4 |
| A415 | 415 | 496.9 |  | 55.4 |
| A416 | 416 | 497.9 |  | 55.3 |
| A417 | 417 | 498.9 |  | 55.3 |
| A418 | 418 | 499.9 |  | 55.3 |
| A419 | 419 | 500.9 |  | 55.3 |
| A420 | 420 | 501.9 |  | 55.3 |
| A421 | 421 | 502.9 |  | 55.3 |
| A422 | 422 | 503.9 |  | 55.3 |
| A423 | 423 | 504.9 |  | 55.3 |
| A424 | 424 | 505.9 |  | 55.2 |
| A425 | 425 | 506.9 |  | 55.2 |
| A426 | 426 | 507.9 |  | 55.2 |
| A427 | 427 | 508.9 |  | 55.2 |
| A428 | 428 | 509.9 |  | 55.2 |
| A429 | 429 | 510.9 |  | 55.2 |
| A430 | 430 | 511.9 |  | 55.2 |
| A431 | 431 | 512.9 |  | 55.1 |
| A432 | 432 | 513.9 |  | 55.1 |
| A433 | 433 | 514.9 |  | 55.1 |
| A434 | 434 | 515.9 |  | 55.1 |
| A435 | 435 | 516.9 |  | 55.1 |
| A436 | 436 | 517.9 |  | 55.1 |
| A437 | 437 | 518.9 |  | 55.1 |
| A438 | 438 | 519.9 |  | 55.1 |
| A439 | 439 | 520.9 |  | 55.0 |
| A440 | 440 | 521.9 |  | 55.0 |
| A441 | 441 | 522.9 |  | 55.0 |
| A442 | 442 | 523.9 |  | 55.0 |
| A443 | 443 | 524.9 |  | 55.0 |
| A444 | 444 | 525.9 |  | 55.0 |
| A445 | 445 | 526.9 |  | 55.0 |
| A446 | 446 | 527.9 |  | 55.0 |
| A447 | 447 | 528.9 |  | 54.9 |
| A448 | 448 | 529.9 |  | 54.9 |
| A449 | 449 | 530.9 |  | 54.9 |
| A450 | 450 | 531.9 |  | 54.9 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| West Linn Abernethy Bridge Northbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 85 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 42.5 |
| w: Width of Structure |  |  |  | 140 |
| Mw : Midpoint of structure ( $\mathrm{w} / 2$ ) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 70 |
| Dref: Reference distance - from S to Aref |  |  |  | 81.9 |
| Measured Noise Level at Drip Edge, $\mathrm{dB}(\mathrm{A})$ |  |  |  | 67.1 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in dB(A) | Calculated Noise Level Drop-off Rate $=4.5$ dB/DD |
| A451 | 451 | 532.9 |  | 54.9 |
| A452 | 452 | 533.9 |  | 54.9 |
| A453 | 453 | 534.9 |  | 54.9 |
| A454 | 454 | 535.9 |  | 54.9 |
| A455 | 455 | 536.9 |  | 54.9 |
| A456 | 456 | 537.9 |  | 54.8 |
| A457 | 457 | 538.9 |  | 54.8 |
| A458 | 458 | 539.9 |  | 54.8 |
| A459 | 459 | 540.9 |  | 54.8 |
| A460 | 460 | 541.9 |  | 54.8 |
| A461 | 461 | 542.9 |  | 54.8 |
| A462 | 462 | 543.9 |  | 54.8 |
| A463 | 463 | 544.9 |  | 54.8 |
| A464 | 464 | 545.9 |  | 54.7 |
| A465 | 465 | 546.9 |  | 54.7 |
| A466 | 466 | 547.9 |  | 54.7 |
| A467 | 467 | 548.9 |  | 54.7 |
| A468 | 468 | 549.9 |  | 54.7 |
| A469 | 469 | 550.9 |  | 54.7 |
| A470 | 470 | 551.9 |  | 54.7 |
| A471 | 471 | 552.9 |  | 54.7 |
| A472 | 472 | 553.9 |  | 54.6 |
| A473 | 473 | 554.9 |  | 54.6 |
| A474 | 474 | 555.9 |  | 54.6 |
| A475 | 475 | 556.9 |  | 54.6 |
| A476 | 476 | 557.9 |  | 54.6 |
| A477 | 477 | 558.9 |  | 54.6 |
| A478 | 478 | 559.9 |  | 54.6 |
| A479 | 479 | 560.9 |  | 54.6 |
| A480 | 480 | 561.9 |  | 54.6 |
| A481 | 481 | 562.9 |  | 54.5 |
| A482 | 482 | 563.9 |  | 54.5 |
| A483 | 483 | 564.9 |  | 54.5 |
| A484 | 484 | 565.9 |  | 54.5 |
| A485 | 485 | 566.9 |  | 54.5 |
| A486 | 486 | 567.9 |  | 54.5 |
| A487 | 487 | 568.9 |  | 54.5 |
| A488 | 488 | 569.9 |  | 54.5 |
| A489 | 489 | 570.9 |  | 54.5 |
| A490 | 490 | 571.9 |  | 54.4 |
| A491 | 491 | 572.9 |  | 54.4 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| West Linn Abernethy Bridge Northbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 85 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 42.5 |
| w: Width of Structure |  |  |  | 140 |
| Mw: Midpoint of structure ( $\mathrm{w} / 2$ ) The underside of the deck at this point is the assumed source of structure noise (S) |  |  |  | 70 |
| Dref: Reference distance - from S to Aref |  |  |  | 81.9 |
| Measured Noise Level at Drip Edge, dB (A) |  |  |  | 67.1 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in dB(A) | Calculated Noise Level Drop-off Rate $=4.5$ dB/DD |
| A492 | 492 | 573.9 |  | 54.4 |
| A493 | 493 | 574.9 |  | 54.4 |
| A494 | 494 | 575.9 |  | 54.4 |
| A495 | 495 | 576.9 |  | 54.4 |
| A496 | 496 | 577.9 |  | 54.4 |
| A497 | 497 | 578.9 |  | 54.4 |
| A498 | 498 | 579.9 |  | 54.3 |
| A499 | 499 | 580.9 |  | 54.3 |
| A500 | 500 | 581.9 |  | 54.3 |


| Structure Related Noise Calculation Worksheet |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| K19786: I-205 Widening and Seismic Improvements |  |  |  |  |
| West Linn Abernethy Bridge Northbound Side |  |  |  |  |
| Input Data: |  |  |  |  |
| h: Height of structure, from ground to underside of deck |  |  |  | 85 |
| Aref: Center point between ground and underside of structure (h/2) |  |  |  | 42.5 |
| w: Width of Structure |  |  |  | 140 |
| Mw: Midpoint of structure (w/2) The underside of the deck at this point is the assumed source of structure noise |  |  |  | 70 |
| Dref: Reference distance - from S to Aref |  |  |  | 81.9 |
| Measured Noise Level at Drip Edge, dB(A) |  |  |  | 66.01737413 |
| Set-back Calculations: |  |  |  |  |
| Analysis Point | Distance from <br> Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in $\mathrm{dB}(\mathrm{A})$ | Calculated <br> Noise Level Drop-off Rate $=3.0 \mathrm{~dB} / \mathrm{DD}$ |
| Aref | 0 | 81.9 | 66.01737413 |  |
| A25 | 25 | 106.9 |  | 64.9 |
| A50 | 50 | 131.9 |  | 63.9 |
| A120 | 120 | 201.9 |  | 62.1 |
| A150 | 150 | 231.9 |  | 61.5 |
| A200 | 200 | 281.9 |  | 60.6 |
| A400 | 400 | 481.9 |  | 58.3 |
| A500 | 500 | 581.9 |  | 57.5 |
| Analysis Point | Distance from Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured <br> Noise Level at <br> Drip Edge Leq <br> in $\mathrm{dB}(\mathrm{A})$ | Calculated <br> Noise Level Drop-off Rate $=4.5 \mathrm{~dB} / \mathrm{DD}$ |
| Aref | 0 | 81.9 | 66.01737413 |  |
| A25 | 25 | 106.9 |  | 64.3 |
| A50 | 50 | 131.9 |  | 62.9 |
| A120 | 120 | 201.9 |  | 60.1 |
| A150 | 150 | 231.9 |  | 59.2 |
| A200 | 200 | 281.9 |  | 58.0 |
| A400 | 400 | 481.9 |  | 54.5 |
| A500 | 500 | 581.9 |  | 53.2 |
| Analysis Point | Distance from Drip Edge (ft.) | Distance from Analysis Point (ft.) | Measured Noise Level at Drip Edge Leq in $\mathrm{dB}(\mathrm{A})$ | Calculated <br> Noise Level Drop-off Rate $=6.0 \mathrm{~dB} / \mathrm{DD}$ |
| Aref | 0 | 81.9 | 66.01737413 |  |
| A25 | 25 | 106.9 |  | 64 |
| A50 | 50 | 131.9 |  | 62 |
| A120 | 120 | 201.9 |  | 58 |
| A150 | 150 | 231.9 |  | 57 |
| A200 | 200 | 281.9 |  | 55 |
| A400 | 400 | 481.9 |  | 51 |
| A500 | 500 | 581.9 |  | 49 |

## Appendix B. Calibration Certificates

CALIBRATION LABORATORY


## Calibration Certificate No. 38800

| Instrument: | Sound Level Meter |
| :--- | :--- |
| Model: | 2250 |
| Manufacturer: | Brüel and Kjær |
| Serial number: | 2579777 |
| Tested with: | Microphone $4189 \mathrm{~s} / \mathrm{n} \mathrm{2589635}$ <br>  <br> Type (class): |
| Preamplifier ZCOO32 s/n 7764 |  |
| Customer: | Harris Miller Miller \& Hanson Inc. |
| Tel/Fax: | 781-229-0707 x3119 / 781-229-7939 |


| Date Calibrated:6/28/2017 Cal Due: |  |  |
| :---: | :---: | :---: |
| Status: | Received | Sent |
| In tolerance: | X | X |
| Out of tolerance: |  |  |
| See comments: |  |  |
| Contains non-accredited tests: __Yes X No |  |  |
| Calibration service: __ Basic X Standard |  |  |
| Address: 777 Sou | Bedford S |  |
|  | n, MA 018 |  |

Tested in accordance with the following procedures and standards:
Calibration of Sound Level Meters, Scantek Inc., Rev. 6/26/2015
SLM \& Dosimeters - Acoustical Tests, Scantek Inc., Rev. 7/6/2011
Instrumentation used for calibration: Nor-1504 Norsonic Test System:

| Instrument - Manufacturer | Description | S/N | Cal. Date | Traceability evidence | Cal. Due |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Cal. Lab / Accreditation |  |
| 483B-Norsonic | SME Cal Unit | 31061 | Jul 27, 2016 | Scantek, Inc./ NVLAP | Jul 27, 2017 |
| DS-360-SRS | Function Generator | 88077 | Sep 15, 2016 | ACR Env./ A2LA | Sep 15, 2018 |
| 34401A-Agilent Technologies | Digital Voltmeter | MY47011118 | Sep 15, 2016 | ACR Env./ A2LA | Sep 15, 2017 |
| HM30-Thommen | Meteo Station | 1040170/39633 | Nov 1, 2016 | ACR Env./ A2LA | Nov 1, 2017 |
| PC Program 1019 Norsonic | Calibration software | v.6.1T | Validated <br> Nov 2014 | Scantek, Inc. | - |
| 1251-Norsonic | Calibrator | 30878 | Nov 10, 2016 | Scantek, inc./ NVLAP | Nov 10, 2017 |

Instrumentation and test results are traceable to SI (International System of Units) through standards maintained by NIST (USA) and NPL (UK).

Environmental conditions:

| Temperature $\left({ }^{\circ} \mathrm{C}\right)$ | Barometric pressure ( kPa ) | Relative Humidity $(\%)$ |
| :---: | :---: | :---: |
| 22.7 | 100.58 | 47.4 |


| Calibrated by: | Jpremy Gotwalt | Authorized signatory: | AWilliam D. Gallagher |
| :---: | :---: | :---: | :---: |
| Signature | ky (1) $10 \frac{1}{3 m}$ | Signature | Whationd gallo |
| Date | 6/28/17 | Date | $6 / 28 / 2017$ |

[^3]ISO 17025: 2005, ANSI/NCSL Z540:1994 Part 1 ACCREDITED by NVLAP (an ILAC MRA signatory)

## Calibration Certificate No. 38801

| Instrument: | Microphone |
| :--- | :--- |
| Model: | 4189 |
| Manufacturer: | Brüel \& Kjær |
| Serial number: | $\mathbf{2 5 8 9 6 3 5}$ |
| Composed of: |  |


| Date Calibrated: 6/26/2017 Cal Due: |  |  |
| :---: | :---: | :---: |
| Status: | Received | Sent |
| In tolerance: | X | X |
| Out of tolerance: |  |  |
|  |  |  |
| Contains non-accredited tests: __Yes X No |  |  |
| Address: $\quad 77$ So | Bedford <br> n, MA 01 |  |

Tested in accordance with the following procedures and standards:
Calibration of Measurement Microphones, Scantek, Inc., Rev. 2/25/2015
Instrumentation used for calibration: N-1504 Norsonic Test System:

| Instrument - Manufacturer | Description | S/N | Cal. Date | Traceability evidence | Cal. Due |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Cal. Lab / Accreditation |  |
| 483B-Norsonic | SME Cal Unit | 25747 | Jul 6, 2016 | Scantek, inc./ NVLAP | Jui 6, 2017 |
| DS-360-SRS | Function Generator | 61646 | Aug 12, 2015 | ACR Env. / AzLA | Aug 12, 2017 |
| 34401A-Agilent Technologies | Digital Voltmeter | MY41022043 | Aug 16, 2016 | ACR Env. / A2LA | Aug 16, 2017 |
| DPI 141-Druck | Pressure Indicator | 790/00-04 | Dec 22, 2016 | ACR Env./ A2LA | Dec 22, 2018 |
| HMP233-Vaisala Oyj | Humidity \& Temp. Transmitter | V3820001 | Apr 19, 2017 | ACR Env. A2LA | Apr 19, 2018 |
| PC Program 1017 Norsonic | Calibration software | v.6.1T | $\begin{aligned} & \text { Validated Nov } \\ & 2014 \end{aligned}$ | Scantek, Inc. | - |
| 1253-Norsonic | Calibrator | 28326 | Nov 10, 2016 | Scantek, inc./ NVLAP | Nov 10, 2017 |
| 1203-Norsonic | Preamplifier | 21270 | May 24, 2017 | Scantek, Inc./ NVLAP | May 24, 2018 |
| 4180-Brüel\&Kjær | Microphone | 2246115 | Oct 26, 2015 | NPL-UK / UKAS | Oct 26, 2017 |

Instrumentation and test results are traceable to SI - BIPM through standards maintained by NPL (UK) and NIST (USA)

| Calibrated by: | Lydon Dawkins $/$ Authorized signatory: | William D Gallagher |  |
| :---: | :---: | :---: | :---: |
| Signature | Leqolon | Lauehead | Signature |
| Date | $6 / 26 / 2017$ | Date | $6 / 28 / 2017$ |

Calibration Certificates or Test Reports shall not be reproduced, except in full, without written approval of the laboratory. This Calibration Certificate or Test Reports shall not be used to claim product certification, approval or endorsement by NVLAP, NIST, or any agency of the federal government.
Document stored as: Z:\Calibration Lab\Mic 2017\B\&K4189_2589635_M1.doc

## Calibration Certificate No. 38809

| Instrument: | Acoustical Calibrator | Date Calibrated: 6/26/2017 Cal Due: |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Model: | 4231 | Status: | Received | Sent |
| Manufacturer: | Brüel and Kjær | In tolerance: <br> Out of tolerance: | X | X |
| Serial number: | 2579293 |  |  |  |
| Class (IEC 60942): | 1 | See comments: |  |  |
| Barometer type: <br> Barometer $s / n$ : |  | Contains non-accredited tests: __Yes X No |  |  |
| Customer: <br> Tel/Fax: | Harris Miller Miller \& Hanson Inc. 781-229-0707 x3119 / 781-2297939 | Address: | Bedford St <br> n, MA 018 |  |

Tested in accordance with the following procedures and standards:
Calibration of Acoustical Calibrators, Scantek Inc., Rev. 10/1/2010
Instrumentation used for calibration: Nor-1504 Norsonic Test System:

| Instrument - Manufacturer | Description | S/N | Cal. Date | Traceability evidence | Cal. Due |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Cal. Lab / Accreditation |  |
| 483B-Norsonic | SME Cal Unit | 31052 | Oct 26, 2016 | Scantek, Inc./ NVLAP | Oct 26, 2017 |
| DS-360-SRS | Function Generator | 33584 | Oct 20, 2015 | ACR Env./ A2LA | Oct 20, 2017 |
| 34401A-Agilent Technologies | Digital Voltmeter | US36120731 | Oct 12, 2016 | ACR Env. / A2LA | Oct 12, 2017 |
| HM30-Thommen | Meteo Station | 1040170/39633 | Nov 1, 2016 | ACR Env. ALLA | Nov 1, 2017 |
| 140-Norsonic | Real Time Analyzer | 1406423 | Oct 29, 2016 | Scantek / NVLAP | Oct 29, 2017 |
| PC Program 1018 Norsonic | Calibration software | v.6.1T | $\begin{array}{\|c\|} \hline \text { Validated Nov } \\ 2014 \\ \hline \end{array}$ | Scantek, Inc. | - - |
| 4134-Brüel\&Kjær | Microphone | 173368 | Nov 10, 2016 | Scantek, Inc. / NVLAP | Nov 10, 2017 |
| 1203-Norsonic | Preamplifier | 14059 | Feb 13, 2017 | Scantek, Inc./ NVLAP | Feb 13, 2018 |

Instrumentation and test results are traceable to SI (International System of Units) through standards maintained by NIST (USA) and NPL (UK)

| Calibrated by: | / Lydon/Bawkins/ | Authorized signatory: | William D. Gallagher |
| :---: | :---: | :---: | :---: |
| Signature |  | Signature | Wellew Datioh |
| Date | $6 / 26 / 2017$ | Date | 612812017 |

[^4] ACCREDITED by NVLAP (an ILAC MRA signatory)

# Calibration Certificate No. 38852 

| Instrument: | Sound Level Meter |
| :--- | :--- |
| Model: | 820 |
| Manufacturer: | Larson Davis |
| Serial number: | $\mathbf{1 2 8 6}$ |
| Tested with: | Microphone 40AQ s/n 23040 |
|  | Preamplifier PRM828 s/n 1833 |
| Type (class): | $\mathbf{1}$ |
| Customer: | Harris Miller Miller \& Hanson Inc. |
| Tel/Fax: | $\mathbf{7 8 1 - 2 2 9 - 0 7 0 7 ~ x 3 1 1 9 ~ / ~ 7 8 1 - 2 2 9 - 7 9 3 9 ~}$ |


| Date Calibrated:7/6/2017 Cal Due: |  |  |
| :---: | :---: | :---: |
| Status: | Received | Sent |
| In tolerance: | X | X |
| Out of tolerance: |  |  |
| See comments: |  |  |
| Contains non-accredited tests: __Yes X No |  |  |
| Calibration service:__ Basic X Standard |  |  |
| Address: 77 Sou | Bedford S n, MA 018 |  |

Tested in accordance with the following procedures and standards:
Calibration of Sound Level Meters, Scantek Inc., Rev. 6/26/2015
SLM \& Dosimeters - Acoustical Tests, Scantek Inc., Rev. 7/6/2011
Instrumentation used for calibration: Nor-1504 Norsonic Test System:

| Instrument - Manufacturer | Description | S/N | Cal. Date | Traceability evidence | Cal. Due |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
| 483B-Norsonic | SME Cal Unit | 25747 | Jul 6, 2016 | Scantek, Inc./ NVLAP | Jul 6, 2017 |
| DS-360-SRS | Function Generator | 61646 | Aug 12, 2015 | ACR Env./A2LA | Aug 12, 2017 |
| 34401A-Agilent Technologies | Digital Voltmeter | MY41022043 | Aug 16, 2016 | ACR Env. / A2LA | Aug 16, 2017 |
| DPI 141-Druck | Pressure Indicator | $790 / 00-04$ | Dec 22, 2016 | ACR Env./A2LA | Dec 22, 2018 |
| HMP233-Vaisala Oyj | Humidity \& Temp. <br> Transmitter | V3820001 | Apr 19, 2017 | ACR Env./A2LA | Apr 19, 2018 |
| PC Program 1019 Norsonic | Calibration software | v.6.1T | Validated Nov <br> 2014 | Scantek, Inc. |  |
| 1251-Norsonic | Calibrator | 30878 | Nov 10,2016 | Scantek, Inc./ NVLAP | Nov 10, 2017 |

Instrumentation and test results are traceable to SI (International System of Units) through standards maintained by NIST (USA) and NPL (UK).

Environmental conditions:

| Temperature $\left({ }^{\circ} \mathrm{C}\right)$ | Barometric pressure $(\mathrm{kPa})$ | Relative Humidity $(\%)$ |
| :---: | :---: | :---: |
| 22.3 | 100.52 | 59.5 |


| Calibrated by: | L Lydon Dawkins | Authorized signatory: | Steven E. Marshall |
| :---: | :---: | :---: | :---: |
| Signature | Inden Dauntus | Signature | skum "Mlarstald |
| Date | $7 / 6 / 2017$ | Date | $7 / 7 / 2017$ |

[^5]ISO 17025: 2005, ANSI/NCSL Z540:1994 Part 1 ACCREDITED by NVLAP (an ILAC MRA signatory) 10

## Calibration Certificate No. 38853

| Instrument: | Microphone |
| :--- | :--- |
| Model: | $40 A Q$ |
| Manufacturer: | GRAS |
| Serial number: | 23040 |
| Composed of: |  |
|  |  |
| Customer: | Harris Miller Miller \& Hanson Inc. |
| Tel/Fax: | 781-229-0707 x3119/781-229-7939 |

Date Calibrated: $7 / 5 / 2017$ Cal Due:
Status:

| Received |
| :--- |

In tolerance:
Out of tolerance:
See comments:
Sent
Contains non-accredited tests: __Yes X No

Address: | 77 South Bedford Street, |
| :--- |
| Burlington, MA 01803 | Burlington, MA 01803

Tested in accordance with the following procedures and standards:
Calibration of Measurement Microphones, Scantek, Inc., Rev. 2/25/2015

Instrumentation used for calibration: N-1504 Norsonic Test System:

| Instrument - Manufacturer | Description | S/N | Cal. Date | Traceability evidence | Cal. Due |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Cal. Lab / Accreditation |  |
| 483B-Norsonic | SME Cal Unit | 31052 | Oct 26, 2016 | Scantek, Inc./ NVLAP | Oct 26, 2017 |
| DS-360-SRS | Function Generator | 33584 | Oct 20, 2015 | ACR Env./ A2LA | Oct 20, 2017 |
| 34401A-Agilent Technologies | Digital Voltmeter | US36120731 | Oct 12, 2016 | ACR Env. / A2LA | Oct 12, 2017 |
| HM30-Thommen | Meteo Station | 1040170/39633 | Nov 1, 2016 | ACR Env./ A2LA | Nov 1, 2017 |
| PC Program 1017 Norsonic | Calibration software | v.6.1T | $\begin{aligned} & \text { Validated Nov } \\ & 2014 \end{aligned}$ | Scantek, Inc. | - |
| 1253-Norsonic | Calibrator | 28326 | Nov 10, 2016 | Scantek, Inc./ NVLAP | Nov 10, 2017 |
| 1203-Norsonic | Preamplifier | 14059 | Feb 13, 2017 | Scantek, Inc./ NVLAP | Feb 13, 2018 |
| 4180-Brüel\&Kjær | Microphone | 2246115 | Oct 26, 2015 | NPL-UK / UKAS | Oct 26, 2017 |

Instrumentation and test results are traceable to SI - BIPM through standards maintained by NPL (UK) and NIST (USA)


[^6] ISO 17025: 2005, ANSI/NCSL Z540:1994 Part 1 ACCREDITED by NVLAP (an ILAC MRA signatory)

## Calibration Certificate No. 38854

| Instrument: | Acoustical Calibrator | Date Calibrated: 6/30/2017 Cal Due: |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Model: | CAL250 | Status: | Received | Sent |
| Manufacturer: | Larson Davis | In tolerance: | x | X |
| Serial number: | 2368 | Out of tolerance: |  |  |
| Class (IEC 60942): | 1 L | See comments: | X |  |
| Barometer type: <br> Barometer s/n: |  | Contains non-accredited tests: __Yes X No |  |  |
| Customer: Tel/Fax: | Harris Miller Miller \& Hanson Inc. 781-229-0707 x3119 / 781-2297939 | Address: 77 So | Bedford Str <br> n, MA 0180 |  |

Tested in accordance with the following procedures and standards:
Calibration of Acoustical Calibrators, Scantek Inc., Rev. 10/1/2010
Instrumentation used for calibration: Nor-1504 Norsonic Test System:

| Instrument - Manufacturer | Description | S/N | Cal. Date | Traceability evidence | Cal. Due |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Cal. Lab / Accreditation |  |
| 483B-Norsonic | SME Cal Unit | 31052 | Oct 26, 2016 | Scantek, Inc./ NVLAP | Oct 26, 2017 |
| DS-360-SRS | Function Generator | 33584 | Oct 20, 2015 | ACR Env./ A2LA | Oct 20, 2017 |
| 34401A-Agilent Technologies | Digital Voltmeter | US36120731 | Oct 12, 2016 | ACR Env. / A2LA | Oct 12, 2017 |
| HM30-Thommen | Meteo Station | 1040170/39633 | Nov 1, 2016 | ACR Env./ A2LA | Nov 1, 2017 |
| 140-Norsonic | Real Time Analyzer | 1406423 | Oct 29, 2016 | Scantek / NVLAP | Oct 29, 2017 |
| PC Program 1018 Norsonic | Calibration software | v.6.1T | $\begin{aligned} & \text { Validated Nov } \\ & 2014 \end{aligned}$ | Scantek, Inc. | - |
| 4134-Brüel\&Kjær | Microphone | 173368 | Nov 10, 2016 | Scantek, Inc. / NVLAP | Nov 10, 2017 |
| 1203-Norsonic | Preamplifier | 14059 | Feb 13, 2017 | Scantek, Inc./ NVLAP | Feb 13, 2018 |

Instrumentation and test results are traceable to SI (International System of Units) through standards maintained by NIST (USA) and NPL (UK)

| Calibrated by: | Lydon Dawkins | Authorized signatory: | Steven E. Marshall |
| :---: | :---: | :---: | :---: |
| Signature | Medontlumbeso | Signature | Stamesillarshall |
| Date | $6130 / 2017$ | Date | 7/5/2017 |

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ISO 17025: 2005, ANSI/NCSL Z540:1994 Part 1 ACCREDITED by NVLAP (an ILAC MRA signatory)

## Calibration Certificate No. 40280

| Instrument: | Sound Level Meter |
| :---: | :---: |
| Mode: | 2250 |
| Manufacturer: |  |
| Serial number: | 2579777 |
| Tested with: | Microphone $4189 \mathrm{~s} / \mathrm{n} 2589635$ |
|  | Preamplifier ZC0032 s/n 7764 |
| Type (ctass): | 1 |
| Customer: | Harrls Miller Miller \& Hanson Inc. |
| Tel/Fax: | 781-229-0707 $\times 3119$ / 781-229-7939 |

Date Calibrated:3/14/2018 Cai Due: Status:
In tolerance:
Out of tolerance:
See comments:
Contains non-accredited tests: Yes $X$ No Colibration service: _ Basic X Standard Address: 77 South Bedford Street, Burlington, MA 01803

Tested in accordance with the following procedures and standards:
Calibration of Sound Level Meters, Scantek Inc., Rev. 6/26/2015
SLM \& Dosimeters - Acoustical Tests, Scantek Inc., Rev. 7/5/2011
Instrumentation used for calibration: Nor-1504 Norsonic Test System:

| Instrument - Manufacturer | Description | S/N | Cal. Date | Traceabillty evidence | Cal. Due |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Cal, Lab / Accreditation |  |
| 4838-Norsonic | SME Cal Unit | 31052 | Oct 30, 2017 | Scantek, lric./ NVLAP | Oct 30, 2018 |
| DS-360-SRS | Function Generator | 33584 | Oct 24, 2017 | ACR Eriv./ A2LA | Oct 24, 2019 |
| 34401A-Agilent Technoiogies | Digital Voltmeter | US36120731 | Oct 25, 2017 | ACR Env. / A2LA | Oct 25,2018 |
| HM30-Thommen | Meteo Station | 1040170/39633 | Oct 25, 2017 | ACR Emv./ A2LA | Oet 25, 2018 |
| PC Program 1019 Norsonic | Calibration software | v.6.1T | $\begin{array}{\|c\|} \hline \text { Validated Noy } \\ 2014 \end{array}$ | scantek, inc. | - |
| 1251-Morsonic | Calibrator | 30878 | Nov 10, 2017 | Scantek, Inc./ NVLAP | Now 10, 2018 |

Instrumentation and test results are traceable to SI (International System of Units) through standards maintained by NIST (USA) and NPL (UK).

Environmental conditions:

| Temperature $\left({ }^{\circ} \mathrm{C}\right)$ | Barometric pressure $(\mathrm{kPa})$ | Relative Humidity $(\%)$ |
| :---: | :---: | :---: |
| 23.6 | 99.19 | 38.2 |


| Calibrated by: | ALydon Rawking | Authorized signatory: | Steven E. Marshall |
| :---: | :---: | :---: | :---: |
| Signature | Leforx lowelew | Signature | \%2uncFIosind |
| Date | 3/14/2018 | Date | $3 / 15 / 2018$ |

Calibration Certificates or Test Reports shall not be reproduced, except in full, without written approval of the laboratory.
This Calibration Certificate or Test Reports shall not be used to claim product certification, approval or endorsement by NVLAP, NIST, or any agency of the federal government.
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Page 2 of 2

ISO 17025: 2005, ANSI/NCSL Z540:1994 Part 1 ACCREDITED by NVLAP (an ILAC MRA signatory)

Calibration Certificate No. 40281

| Instrument: | Microphone | Date Calibrated: 3/13/2018 Cal Due: |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Model: | 4189 | Stotus: in toleronce: | Recelved | Sent |
| Monufocturer: | Briuel \& Kjar |  | X | X |
| Serial number: | 2589635 | Out of tolerance: |  |  |
| Composed of: |  | See comments: |  |  |
|  |  | Contains non-acc | ed tests: | No |
| Customer: | Harris Miller Miller \& Hanson Inc. | Address: 77 Sour | Bedford S |  |
| Tel/Fax: | 781-229-0707 x3119/781-229-7939 | Burlin | on, MA 018 |  |

Tested in accordance with the following procedures and standards:
Calibration of Measurement Microphones, Scantek, Inc., Rev. 2/25/2015
Instrumentation used for calibration: N-1504 Norsonic Test \$ystem:

| Instrument - Manufacturer | Description | 5/N | Cal. Date | Traceability evfdence | Cal. Due |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Cal. Lab / Accreditation |  |
| 4838-Norsonic | SME Cal Unit | 31052 | Oct 30, 2017 | Scantek, Inc./ NY/AP | Oct 30, 2018 |
| DS-360-SRS | Function Generator | 33584 | Oct 24, 2017 | ACR Env/ / ALLA | Oet 24, 2019 |
| 34401A-Agilent Technologies | Digital Voltmeter | U536120731 | Oct 25, 2017 | ACR Env. / AZLA | Oct 25, 2018 |
| HM30-Thommen | Meteo Station | 1040170/39633 | Oct 25, 2017 | ACA Env/alda | Oct 25, 2018 |
| PC Program 1017 Norsonic | Calibration software | v.6.1T | Validated Now 2014 | Scantek, Inc. | - |
| 1253-Norsonit | Calibrator | 28326 | Nov 10, 2017 | Scantek, Inc./ NVLAP | Nov 10, 2018 |
| 1203-Norsonic | Preamplifier | 14059 | Feb 12, 2018 | Scantek, Inc/ / NVLAP | Feb 12, 2019 |
|  | Microphone | 2246115 | Oct 24, 2017 | DANAK / DPLA | Oct 24, 2019 |

Instrumentation and test results are traceable to SI - BIPM through standards maintained by NPL (UK) and NIST (USA)

| Calibrated by: | / Lydon Dawkins/ | Authorized signatory: | Steven E. Marshall |
| :---: | :---: | :---: | :---: |
| Signature | Hedon Davehum | Signature | Werem CMmantall |
| Date | $3 / 13 / 2018$ | Date | $3 / 15 / 2018$ |

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Page 1 of 2

## Calibration Certificate No. 40282

instrument:
Model:
Manufacturer:
Serial number:
Class (IEC 60942):
Barometer type:
Barometer $s / n$ :
Customer:
Tel/Fax:

```
Acoustical Calibrator
4231
Britel and Kjær
2579293
1
```

Harris Miller Miller \& Hanson Inc
$781-229-0707 \times 3119 / 781-229$ -
7939 7939

Dote Collbrated: 3/12/2018 Cal Due:

| Status: | Received | Sent |
| :--- | :---: | :---: |
| In tolerance: | X | X |
| Out of toleronce: |  |  |
| See comments: |  |  |
| Contoins non-accredited tests: $\quad$ Yes $\mathbf{X}$ No |  |  |

Address:
有

## 77 South Bedford Street, Burlington, MA 01803

Tested in accordance with the following procedures and standards: Calibration of Acoustical Calibrators, Scantek Inc., Rev. 10/1/2010

Instrumentation used for callbration: Nor-1504 Norsonic Test System:

| Instrument - Manufacturer | Description | S/N | Cal. Date | Traceability evidence | Cal. Due |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Cal, Lab/ Actreditation |  |
| 4838-Norsonic | SME Cal Unit | 31052 | Oct 30, 2017 | Scantek, tnc./ NVLAP | Oct 30, 2018 |
| 05-360-SRS | Function Generator | 33584 | Oct 24, 2017 | ACR ERv./ A2LA | Oct 24, 2019 |
| 34401A-Agilent Technologies | Digital Voltmeter | U536120731 | Oct 25,2017 | ACR Env. / A2LA | Oct 25, 2018 |
| HM30-Thommen | Meteo Station | 1040170/39633 | Oct 25,2017 | ACA Env// A2LA | Oct 25, 2018 |
| 140-Norsonic | Reall Time Analyzer | 1406423 | Oct 31, 2017 | Scantek / NVLAP | Oct 31, 2018 |
| PC Program 1018 Norsonic | Calibration software | v.6.1T | $\begin{gathered} \text { Validated Now } \\ 2014 \end{gathered}$ | Scantek, Inc. |  |
| 4134-Brüel\&Kjör | Microphone | 173368 | Nov 10, 2017 | Scantek, Inc. / WVLAP | Nov 10, 2018 |
| 1203-Norsonic | Preamplifier | 14059 | Feb 12, 2018 | Scantek, Inc./ NVLAP | Feb 12, 2019 |

Instrumentation and test results are traceable to SI (International System of Units) through standards maintained by NIST (USA) and NPL (UK)


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Page 1 of 2

# Scanteh, Inc. CALIBRATION LABORATORY 

ISO 17025: 2005, ANSI/NCSL Z540:1994 Part 1 ACCREDITED by NVLAP (an ILAC MRA signatory)

## Calibration Certificate No. 40291

| Instrument: | Sound Level Meter |
| :---: | :---: |
| Model: | 2250 |
| Monufocturer: | Briuel and Kjzer |
| Serial number: | 2619791 |
| Tested with: | Microphone $4189 \mathrm{~s} / \mathrm{n} 2616506$ |
|  | Preamplifier ZC0032 s/n 11159 |
| Type (class): | 1 |
| Customer: | Harris Miller Miller \& Hanson Inc. |
| Tel/Fax: | 781-229-0707 x3119 / 781-229-7939 |


| Date Callbrated:3/ | 2018 |  |
| :---: | :---: | :---: |
| Status: | Received | Sent |
| In toleronce: | X | $x$ |
| Out of tolerance: |  |  |
| See comments: |  |  |
| Contains non-accre | ted tests: | X N0 |
| Colibrotion service: | Basic X | dard |
| Address: 77 Sou | Bedford S |  |
| Burling | n, MA 018 |  |

Tested in accordance with the following procedures and standards:
Calibration of Sound Level Meters, Scantek Inc., Rev. 6/26/2015
SLM \& Dosimeters - Acoustical Tests, Scantek Inc., Rev. 7/6/2011
Instrumentation used for calibration: Nor-1504 Norsonic Test System:

| Instrument - Manufacturer | Deseription | 5/0 | Cal. Date | Traceabillty evidence | Cal. Dut |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Cal. Lab / Accreditation |  |
| 4838-Norsonic | SME Cal Unit | 31051 | Jull 28, 2017 | Scantek, Inc./ NVLAP | Jul 28, 2018 |
| DS-360-5RS | Function Generator | 88077 | Sep 15, 2016 | ACR Env./ ALLA | Sep 15, 2018 |
| 34401A-Agilent Technologies | Digital Voltmeter | MY47011118 | Sep 20, 2017 | ACR Emv./ A2LA | Sep 20, 2018 |
| HM30-Thommen | Meteo Station | 1040170/39633 | Oct 25, 2017 | ACh Env./ A2LA | Oct 25, 2018 |
| PC Program 1019 Norsonic | Callibration software | v.6.1t | Validated Noy 2014 | Scantek, Inc. | - |
| 1251-Norsonic | Calibrator | 30878 | Nov 10, 2017 | Scantek, Inc./ NVLAP | Nov 10, 2018 |

Instrumentation and test results are traceable to SI (International System of Units) through standards maintained by NIST (USA) and NPL (UK).

Environmental conditions;

| Temperature ( ${ }^{\circ} \mathrm{C}$ ) | Barometric pressure (kPa) | Relative Humidity (\%) |
| :---: | :---: | :---: |
| 22.9 | 99.31 | 38.8 |


| Calibrated by: | Jeremy Gitwalt | Authorized signatory: | Steven E. Marshall |
| :---: | :---: | :---: | :---: |
| Signature |  | $4 / 4$ | Signature |
| Date | $1 / 4 / / 8$ | Date | $3 / 5 / 20 / 8$ |

[^7]
## Scanteh, Inc.

 CALIBRATION LABORATORYISO 17025: 2005, ANSI/NCSL 2540:1994 Part 1 ACCREDITED by NVLAP (an ILAC MRA signatory)


## Calibration Certificate No. 40292

| Instrument: | Microphone |
| :--- | :--- |
| Model: | $\mathbf{4 1 8 9}$ |
| Manufacturer: | Brïel \& Kjeer |
| Serial number: | $\mathbf{2 6 1 6 5 0 6}$ |
| Composed of: |  |
|  |  |
| Customer: | Harris Miller Miller \& Hanson Inc. |
| Tel/Fax: | $\mathbf{7 8 1 - 2 2 9 - 0 7 0 7 \times 3 1 1 9 / 7 8 1 - 2 2 9 - 7 9 3 9 ~}$ |



Tested in accordance with the following procedures and standards: Calibration of Measurement Microphones, Scantek, Inc., Rev. 2/25/2015

Instrumentation used for calibration: N-1504 Norsonic Test System:

| Instrument - Manufacturer | Description | S/N | Cal. Date | Traceability evidence | Cal. Due |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Cal. Lab/Accroditation |  |
| 4838-Norsonic | SME Cal Unit | 31061 | Jull 28, 2017 | Scantek, Inc./ NVLAP | Mul 28, 2018 |
| OS-360-SRS | Function Generator | 88077 | Sep 15, 2016 | ACR Env/ AZLA | Sep 15, 2018 |
| 34401A-Agilent Technologies | Digital Voltmeter | MY47011118 | Sep 20, 2017 | ACR Env/ A2LA | Sep 20, 2018 |
| HM30-Thommen | Meteo Station | 1040170/39633 | Oct 25, 2017 | ACA Env./ AZLA | Oct 25,2018 |
| PC Program 1017 Norsonic | Callbration software | v.6.1T | Validated Now 2014 | Stantek, Int. | - |
| 1253-Norsonic | Calibrator | 28326 | Nov 10, 2017 | Scantek, Inc./ NVLAP | Nov 10, 2018 |
| 1203-Norsonic | Preamplifier | 92268 | Oct 18, 2017 | Scantek, Inc./ NVLAP | Oct 18, 2018 |
| 4180-Brtiel 8 Kjaer | Microphone | 2246115 | Oct 24, 2017 | DANAK/ DPLA | Oct 24, 2019 |

Instrumentation and test results are traceable to $S$ - BIPM through standards maintained by NPL (UK) and NIST (USA)

| Calibrated by: | Jerems Gotwalt | Authorized signatory: | Steven E Marshall |
| :---: | :---: | :---: | :---: |
| Signature | m. 1 人束 | Signature | bwuen EMousiadd |
| Date | $1 / 3 / 12 / 18$ | Date | $3 / 5 / 2018$ |

[^8]
## Calibration Certificate No. 40293

## Instrument:

Model:
Manufacturer:
Serial number:
Class (IEC 60942):
Borometer type:
Barometer $\mathrm{s} / \mathrm{n}$ :
Customer:
Tel/Fax:

Acoustical Calibrator<br>4231<br>Brüel and Kjær<br>2579294<br>1

Harris Miller Miller \& Hanson Inc.
$\mathbf{7 8 1 - 2 2 9 - 0 7 0 7 \times 3 1 1 9 /}$
$\mathbf{7 8 1 - 2 2 9 - 7 9 3 9}$

Date Calibrated: 3/12/2018 Cal Due:

| Stotus: | Recelved | Sent |
| :--- | :---: | :---: |
| in tolerance: | $\mathbf{X}$ | $\mathbf{X}$ |
| Out of tolerance: |  |  |
| See comments: |  |  |
| Contains non-accredited tests: | Ves $X$ No |  |

## 77 South Bedford Street

 Burlington, MA 01803Tested in accordance with the following procedures and standards:
Calibration of Acoustical Calibrators, Scantek Inc., Rev, 10/1/2010
Instrumentation used for calibration: Nor-1504 Norsonic Test System:

| Instrument - Manufacturer | Description | \$/N | Cal. Date | Traceability ev/dence | Cal. Due |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Cal. Lab / Accreditation |  |
| 4838-Norsonic | SME Cal Unit | 31061 | Jul 28, 2017 | Scantek, Inc./ NVLAP | Jul 28, 2018 |
| DS-360-5RS | Function Generator | 88077 | Sep 15,2016 | ACR Env./ AZLA | Sep 15, 2018 |
| 34401A-Agilent Technologles | Digital Voltmeter | MY47011118 | Sep 20, 2017 | ACR Env/ / A2LA | Sep 20, 2018 |
| HM30-Thommen | Meteo Station | 1040170/39633 | Oct 25, 2017 | ACR Env./ A2LA | Oct 25, 2018 |
| 140-Marsonic | Real Time Analyzer | 1403978 | Mar 22, 2017 | Scantek, Inc. / NVLAP | Mar 22, 2018 |
| PC Program 1018 Norsonic | Calibration software | v.6.17 | Validated Nov 2014 | Scantek, Inc. |  |
| 4192-BrūelRKjær | Microphone | 2854675 | Nov 11, 2017 | Stantek, Inc. / NVLAP | Nov 11, 2018 |
| 1203-Norsonic | Preamplifier | 92268 | Oct 18, 2017 | Scantek Inc/ MVLAP | Ott 18, 2018 |

Instrumentation and test results are traceable to SI (International System of Units) through standards maintained by NIST (USA) and NPL (UK)


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Page 1 of 2

CALIBRATION LABORATORY
ISO 17025: 2005, ANSI/NCSL 2540:1994 Part 1 ACCREDITED by NVLAP (an ILAC MRA signatory)

# Calibration Certificate No. 40294 

| Instrument: | Sound Level Meter |
| :--- | :--- |
| Model: | 2250 |
| Manufacturer: | Brüel and Kjeer |
| Serial number: | 2579776 |
| Tested with: | Microphone $\mathbf{4 1 8 9} \mathrm{s/n} \mathbf{2 6 1 6 5 0 7}$ |
|  | Preamplifier 2C0032 s/n 18967 |
| Type (class): | 1 |
| Customer: | Harris Miller Miller \& Hanson Inc. |
| Tel/Fax: | $\mathbf{7 8 1 - 2 2 9 - 0 7 0 7 ~ \times 3 1 1 9 / 7 8 1 - 2 2 9 - 7 9 3 9 ~}$ |

Date Calibrated:3/14/2018 Cal Due: Status:
in tolerance:
Out of tolerance:
See comments:

| Recelved | Sent |
| :---: | :---: |
| X | X |
|  |  |
|  |  |

Contains non-accredited tests: Yes X No Callbration service: $\qquad$ Basic X Standard Address: 77 South Bedford Street Burlington, MA 01803

Tested in accordance with the following procedures and standards:
Calibration of Sound Level Meters, Stantek inc., Rev. 6/26/2015
SLM \& Dosimeters - Acoustical Tests, Scantek Inc., Rev. 7/6/2011
Instrumentation used for calibration: Nor-1504 Norsonic Test System:

| Instrument - Manufacturer | Descriptlon | 5/N | Cal, Date | Traceabillty evidence | Cal. Due |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Cal, Lab / Accreditation |  |
| 4838-Norsonic | SME Cal Unit | 31061 | Jull 28,2017 | Scantek, Inc./ NVLAP | Jul 28, 2018 |
| DS-360-SAS | Function Generator | 88077 | Sep 15, 2016 | ACR Env./ A2LA | Sep 15, 2018 |
| 34401A-Agilent Technologies | Digital Voltmeter | MY47011118 | Sep 20, 2017 | ACR Env./ A2LA | Sep 20, 2018 |
| HM30-Thommen | Meteo Station | 1040170/39633 | Oct 25, 2017 | ACR Env./ A2LA | Oct 25, 2018 |
| PC Program 1019 Morsontc | Calibration software | v.6.1T | Validated Nov 2014 | Scantek, Inc. | - |
| 1251-Norsonic | Calibrator | 30878 | Nov 10, 2017 | Scantek, Inc./ NVLAP | Now 10, 2018 |

Instrumentation and test results are traceable to SI (International System of Units) through standards
maintained by NIST (USA) and NPL (UK).
Environmental conditions:

| Temperature $\left({ }^{\circ} \mathrm{C}\right)$ | Barometric pressure $(\mathrm{kPa})$ | Relative Humidity $(\%)$ |
| :---: | :---: | :---: |
| 23.2 | 99.31 | $\mathbf{3 9 . 1}$ |


| Calibrated by: | Jeremy Gotwalt | Authorized signatory: | Steven E. Marshall |
| :---: | :---: | :---: | :---: |
| Signature | 40\% | Signature |  |
| Date | $1 \mathrm{O} 3 / 14 / 18$ | Date | $3 / 15 / 2018$ |

Calibration Certifitates or Test Reports shall not be reproduced, except in fult, without writen approval of the laboratory.
This Calibration Certificate or Test Reports shall not be used to claim product certification, approval or endorsement by NVLAP, NIST, or any agency of the federal government.
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Page 1 of 2

## Scanteh, Inc. CALIBRATION LABORATORY

 ISO 17025: 2005, ANSI/NCSL Z540:1994 Part 1 ACCREDITED by NVLAP (an ILAC MRA signatory)
# Calibration Certificate No. 40295 

| Instrument: | Microphone |
| :--- | :--- |
| Model: | $\mathbf{4 1 8 9}$ |
| Monufocturer: | Brüel \& Kjaer |
| Seriol number: | $\mathbf{2 6 1 6 5 0 7}$ |
| Composed of: |  |
|  |  |
| Customer: | Harris Miller Miller \& Hanson Inc. |
| Tel/Fox: | $\mathbf{7 8 1 - 2 2 9 - 0 7 0 7 ~ \times 3 1 1 9 / 7 8 1 - 2 2 9 - 7 9 3 9 ~}$ |

Dote Calibrated: $3 / 12 / 2018$ Cal Due:

| Status: |
| :--- |
| In tolerance: |
| Received |
| Out of tolerance: |
| See comments: |

Contoins non-occredited tests: __Yes X No
Address: 77 South Bedford Street Burlington, MA 01803

Tested in accordance with the following procedures and standards:
Calibration of Measurement Microphones, Scantek, Inc., Rev. 2/25/2015
Instrumentation used for calibration: $\mathbf{N - 1 5 0 4}$ Norsonic Test System:

| Instrument - Manufacturer | Description | S/N | Cal. Date | Traceability euldence | Cal. Due |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Cal. Lab/ Accreditation |  |
| 483B-Norsonit | SME Cal Unit | 31061 | Jull 28, 2017 | Stantek, Inc/ / NVLAP | Jul 28, 2018 |
| DS-360-5RS | Function Generator | 88077 | Sep 15, 2016 | ACR Envo/ A2LA | Sep 15, 2018 |
| 74401A-Agilent Technologies | Digital Voltmeter | M 1 47011118 | Sep 20, 2017 | ACR Env./ AzLA | Sep 20, 2018 |
| HM30-Thommen | Meteo Station | 1040170/39633 | Oct 25,2017 | ACR Env./ AZLA | Oet 25, 2018 |
| PC Program 1017 Norsonic | Calibration software | v.6.1T | Validated Now 2014 | Scantek, Inc. | - |
| 1253-Norsonic | Calibrator | 28326 | Nov 10, 2017 | Scantek, Inc./ NVLAP | Nov 10, 2018 |
| 1203-Narsonic | Preamplifier | 92268 | Oct 18, 2017 | Scantek, Inc/ NVLAP | Oct 18, 2018 |
| 4180-Brtielqkjar | Microphone | 2246115 | Oct 24, 2017 | DANAK / DPLA | Oct 24, 2019 |

Instrumentation and test results are traceable to 51 - BIPM through standards maintained by NPL (UK) and NIST (USA)

| Calibrated by: | Jeremy Gotwalt | Authorized signatory: | Steven E Marshall |
| :---: | :---: | :---: | :---: |
| Signature | anteratios | Signature | Samamandial |
| Date | 3/12/18 | Date | $3 / 5 / 2018$ |

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Page 1 of 2

CALIBRATION LABORATORY
ISO 17025: 2005, ANSI/NCSL 2540:1994 Part 1 ACCREDITED by NVLAP (an ILAC MRA signatory)


## Calibration Certificate No. 40296

Instrument:<br>Model:<br>Monufacturer:<br>Serial number:<br>Closs (IEC 60942):<br>Acoustical Calibrator 4231<br>Brüel and Kjar<br>2579295<br>Barometer type:<br>1<br>Barometer s/n:<br>Customer:<br>\section*{Harris Miller Miller \& Hanson Inc. Address:<br><br>781-229-0707 x3119 / 781-229-7939}<br>Status:<br>In tolerance:<br>See comments:<br>Tel/Fax:

Date Calibrated: 3/12/2018 Cal Due:

Out of tolerance:

Contains non-accredited tests: $\qquad$ Yes X No

Tested in accordance with the following procedures and standards:
Calibration of Acoustical Calibrators, Scantek Inc., Rev. 10/1/2010

Instrumentation used for calibration: Nor-1504 Norsonic Test System:

| Instrument - Manufacturer | Description | \$/N | Cal. Date | Traceability evidence | Cal. Due |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Cal. Lab / Accreditation |  |
| 4838-Norsonic | SME Cal Unit | 31061 | Jul 28, 2017 | Scantek, Inc// MVLAP | Jul 28, 2018 |
| DS-360-SRS | Function Generator | 88077 | Sep 15,2016 | ACR Env./A2LA | Sep 15,2018 |
| 34401A-Agilent Technologies | Digital Voltmeter | MY47011118 | 5ep 20, 2017 | ACR Env/ AzLA | Sep 20, 2018 |
| HM330-Thommen | Meteo Station | 1040170/39633 | Oct 25, 2017 | ACR Env./ AZLA | Oct 25, 2018 |
| 140-Norsonic | Real Time Analyzer | 1403978 | Mar 22, 2017 | Scantek, Inc. / NVLAP | Mar 22, 2018 |
| PC Program 1018 Norsonlc | Calitbration software | v.6.1T | Validated Nov 2014 | Scantek, Inc. |  |
| 4192-Brüel\&Kjer | Microphone | 2854675 | Nov 11, 2017 | Scantek, Inc. / NVLAP | Nov 11,2018 |
| 1203-Norsonic | Preamplifier | 92268 | Oct 18, 2017 | Scantek, Inc./ NVLAP | Oet 18, 2018 |

Instrumentation and test results are traceable to $\mathbf{S I}$ (International System of Units) through standards maintained by NIST (USA) and NPL (UK)

| Calibrated by: | Jgremx Gotwalt | Authorized signatory: | Steven E. Marshall |
| :---: | :---: | :---: | :---: |
| Signature | 4A大 | Signature |  |
| Date | $(1) 3 / 12 / 18$ | Date | 9/15/20/8 |

[^9]
## Appendix C. Traffic Data Used in the Noise Analysis

Table C-1. Short-Term 10-minute Traffic Counts

| Measurement Location | Roadway | Vehicle | Counted NB or EB | Counted SB or WB | Hourly Equivale nt NB or EB | Hourly Equivalen t SB or WB | Speed (mph) NB or EB | Speed (mph) SB or WB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ST01 | 1-205 | Autos | 444 | 296 | 2664 | 1776 | 65 | 65 |
|  |  | MT | 18 | 18 | 108 | 108 |  |  |
|  |  | HT | 44 | 52 | 264 | 312 |  |  |
|  |  | Bus | 0 | 0 | 0 | 0 |  |  |
|  |  | Moto | 3 | 0 | 18 | 0 |  |  |
|  | Borland Rd | Autos | 8 | 8 | 48 | 48 | 45 | 45 |
|  |  | MT | 0 | 0 | 0 | 0 |  |  |
|  |  | HT | 0 | 0 | 0 | 0 |  |  |
|  |  | Bus | 0 | 0 | 0 | 0 |  |  |
|  |  | Moto | 0 | 0 | 0 | 0 |  |  |
| ST02 | I-205 | Autos | 516 | 394 | 3096 | 2364 | 65 | 65 |
|  |  | MT | 26 | 24 | 156 | 144 |  |  |
|  |  | HT | 40 | 30 | 240 | 180 |  |  |
|  |  | Bus | 3 | 0 | 18 | 0 |  |  |
|  |  | Moto | 3 | 2 | 18 | 12 |  |  |
|  | Johnson Creek Rd | Autos | 14 | 6 | 84 | 36 | 45 | 45 |
|  |  | MT | 0 | 0 | 0 | 0 |  |  |
|  |  | HT | 0 | 0 | 0 | 0 |  |  |
|  |  | Bus | 0 | 0 | 0 | 0 |  |  |
|  |  | Moto | 0 | 0 | 0 | 0 |  |  |
| ST03 | I-205 | Autos | 332 | 425 | 1992 | 2550 | 65 | 65 |
|  |  | MT | 14 | 15 | 84 | 90 |  |  |
|  |  | HT | 22 | 42 | 132 | 252 |  |  |
|  |  | Bus | 0 | 0 | 0 | 0 |  |  |
|  |  | Moto | 0 | 0 | 0 | 0 |  |  |
| ST04 | I-205 | Autos | 365 | 472 | 2190 | 2832 | 65 | 65 |
|  |  | MT | 16 | 20 | 96 | 120 |  |  |
|  |  | HT | 28 | 30 | 168 | 180 |  |  |
|  |  | Bus | 0 | 0 | 0 | 0 |  |  |
|  |  | Moto | 0 | 0 | 0 | 0 |  |  |
| ST05 | I-205 | Autos | 400 | 462 | 2400 | 2772 | 65 | 65 |
|  |  | MT | 14 | 26 | 84 | 156 |  |  |
|  |  | HT | 40 | 28 | 240 | 168 |  |  |
|  |  | Bus | 0 | 0 | 0 | 0 |  |  |

Table C-1. Short-Term 10-minute Traffic Counts

| Measurement Location | Roadway | Vehicle | $\begin{aligned} & \text { Counted } \\ & \text { NB or } \\ & \text { EB } \end{aligned}$ | $\begin{aligned} & \text { Counted } \\ & \text { SB or } \\ & \text { WB } \end{aligned}$ | Hourly Equivale nt NB or EB | Hourly Equivalen t SB or WB | $\begin{gathered} \hline \text { Speed } \\ (\mathrm{mph}) \\ \mathrm{NB} \text { or } \\ \mathrm{EB} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { Speed } \\ (\mathrm{mph}) \\ \text { SB or } \\ \text { WB } \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Moto | 0 | 0 | 0 | 0 |  |  |
| ST06 | I-205 | Autos | 436 | 455 | 2616 | 2730 | 65 | 65 |
|  |  | MT | 8 | 20 | 48 | 120 |  |  |
|  |  | HT | 28 | 34 | 168 | 204 |  |  |
|  |  | Bus | 0 | 0 | 0 | 0 |  |  |
|  |  | Moto | 0 | 0 | 0 | 0 |  |  |
|  | Blankenship Rd | Autos | 10 | 14 | 60 | 84 | 25 | 25 |
|  |  | MT | 0 | 0 | 0 | 0 |  |  |
|  |  | HT | 0 | 1 | 0 | 6 |  |  |
|  |  | Bus | 0 | 0 | 0 | 0 |  |  |
|  |  | Moto | 0 | 0 | 0 | 0 |  |  |
| ST07 | 1-205 | Autos | 412 | 474 | 2472 | 2844 | 35 | 55 |
|  |  | MT | 15 | 10 | 90 | 60 |  |  |
|  |  | HT | 39 | 23 | 234 | 138 |  |  |
|  |  | Bus | 0 | 0 | 0 | 0 |  |  |
|  |  | Moto | 0 | 0 | 0 | 0 |  |  |
| ST08 | I-205 | Autos | 414 | 430 | 2484 | 2580 | 55 | 30 |
|  |  | MT | 27 | 15 | 162 | 90 |  |  |
|  |  | HT | 41 | 31 | 246 | 186 |  |  |
|  |  | Bus | 0 | 0 | 0 | 0 |  |  |
|  |  | Moto | 0 | 0 | 0 | 0 |  |  |
|  | Willamette Falls Drive | Autos | 39 | 35 | 234 | 210 | 45 | 45 |
|  |  | MT | 0 | 0 | 0 | 0 |  |  |
|  |  | HT | 0 | 0 | 0 | 0 |  |  |
|  |  | Bus | 0 | 0 | 0 | 0 |  |  |
|  |  | Moto | 0 | 0 | 0 | 0 |  |  |
| ST09 | 1-205 | Autos | 248 | 253 | 1488 | 1518 | 55 | 40 |
|  |  | MT | 16 | 20 | 96 | 120 |  |  |
|  |  | HT | 36 | 40 | 216 | 240 |  |  |
|  |  | Bus | 0 | 0 | 0 | 0 |  |  |
|  |  | Moto | 0 | 0 | 0 | 0 |  |  |
| ST10 | I-205 | Autos | 478 | 556 | 2868 | 3336 | 40 | 40 |
|  |  | MT | 31 | 28 | 186 | 168 |  |  |
|  |  | HT | 34 | 36 | 204 | 216 |  |  |
|  |  | Bus | 0 | 0 | 0 | 0 |  |  |
|  |  | Moto | 0 | 0 | 0 | 0 |  |  |
| ST11 | Willamette Falls Drive | Autos | 40 | 59 | 240 | 354 | 40 | 40 |

Table C-1. Short-Term 10-minute Traffic Counts

| Measurement Location | Roadway | Vehicle | $\begin{aligned} & \text { Counted } \\ & \text { NB or } \\ & \text { EB } \end{aligned}$ | $\begin{aligned} & \text { Counted } \\ & \text { SB or } \\ & \text { WB } \end{aligned}$ | Hourly Equivale nt NB or EB | Hourly <br> Equivalen <br> t SB or <br> WB | $\begin{gathered} \hline \text { Speed } \\ (\mathrm{mph}) \\ \text { NB or } \\ \text { EB } \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { Speed } \\ (\mathrm{mph}) \\ \text { SB or } \\ \text { WB } \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MT | 2 | 0 | 12 | 0 |  |  |
|  |  | HT | 1 | 0 | 6 | 0 |  |  |
|  |  | Bus | 2 | 1 | 12 | 6 |  |  |
|  |  | Moto | 0 | 0 | 0 | 0 |  |  |
| ST12 | I-205 | Autos | 444 | 403 | 2664 | 2418 | 50 | 55 |
|  |  | MT | 18 | 26 | 108 | 156 |  |  |
|  |  | HT | 44 | 25 | 264 | 150 |  |  |
|  |  | Bus | 0 | 0 | 0 | 0 |  |  |
|  |  | Moto | 0 | 0 | 0 | 0 |  |  |
|  | I205SB Offramp to OR 43 | Autos |  | 20 | 0 | 121 |  | 25-40 |
|  |  | MT |  | 1 | 0 | 8 |  |  |
|  |  | HT |  | 1 | 0 | 8 |  |  |
|  |  | Bus |  | 0 | 0 | 0 |  |  |
|  |  | Moto |  | 0 | 0 | 0 |  |  |
| ST13 | I-205 | Autos | 450 | 410 | 2700 | 2460 | 55 | 35 |
|  |  | MT | 17 | 23 | 102 | 138 |  |  |
|  |  | HT | 45 | 27 | 270 | 162 |  |  |
|  |  | Bus | 0 | 0 | 0 | 0 |  |  |
|  |  | Moto | 0 | 0 | 0 | 0 |  |  |
|  | 99E | Autos | 216 | 275 | 1296 | 1650 | 30 | 20 |
|  |  | MT | 4 | 9 | 24 | 54 |  |  |
|  |  | HT | 2 | 4 | 12 | 24 |  |  |
|  |  | Bus | 0 | 0 | 0 | 0 |  |  |
|  |  | Moto | 0 | 0 | 0 | 0 |  |  |
|  | Clackamette Drive | Autos | 2 | 5 | 12 | 30 | 20 | 20 |
|  |  | MT | 1 | 0 | 6 | 0 |  |  |
|  |  | HT | 0 | 0 | 0 | 0 |  |  |
|  |  | Bus | 0 | 0 | 0 | 0 |  |  |
|  |  | Moto | 0 | 0 | 0 | 0 |  |  |
| Structure <br> Radiated <br> Noise <br> Measureme <br> nt Oregon <br> City | I-205 | Autos | 312 | 652 | 1248 | 2608 | 55 | 35 |
|  |  | MT | 63 | 46.5 | 252 | 186 |  |  |
|  |  | HT | 31 | 30 | 124 | 120 |  |  |
|  |  | Bus | 0 | 0 | 0 | 0 |  |  |
|  |  | Moto | 0 | 0 | 0 | 0 |  |  |
|  | 99E | Autos | 339 | 324 | 1356 | 1296 | 30 | 20 |
|  |  | MT | 11 | 11 | 44 | 44 |  |  |
|  |  | HT | 12 | 12 | 48 | 48 |  |  |

Table C－1．Short－Term 10－minute Traffic Counts

| Measurement Location | Roadway | Vehicle | $\begin{aligned} & \text { Counted } \\ & \text { NB or } \\ & \text { EB } \end{aligned}$ | $\begin{aligned} & \text { Counted } \\ & \text { SB or } \\ & \text { WB } \end{aligned}$ | Hourly Equivale nt NB or EB | Hourly Equivalen t SB or WB | $\begin{gathered} \hline \begin{array}{c} \text { Speed } \\ \text { (mph) } \\ \text { NB or } \\ \text { EB } \\ \hline \end{array} ⿳ ⺈ ⿴ 囗 十 一 ~ \end{gathered}$ | $\begin{gathered} \hline \text { Speed } \\ (\mathrm{mph}) \\ \text { SB or } \\ \text { WB } \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Bus | 0 | 0 | 0 | 0 |  |  |
|  |  | Moto | 0 | 0 | 0 | 0 |  |  |
| Structure <br> Radiated <br> Noise <br> Measureme <br> nt West <br> Linn 6－13－ <br> 2018 | I－205 | Autos | 925 | 689 | 3700 | 2756 | 55 | 55 |
|  |  | MT | 49 | 34 | 196 | 136 |  |  |
|  |  | HT | 45 | 34 | 180 | 136 |  |  |
|  |  | Bus | 0 | 0 | 0 | 0 |  |  |
|  |  | Moto | 0 | 0 | 0 | 0 |  |  |
|  | $\begin{aligned} & \text { I-205 NB On- } \\ & \text { Ramp } \end{aligned}$ | Autos | 156 | 0 | 624 | 0 | 36 | 0 |
|  |  | MT | 7 | 0 | 28 | 0 |  |  |
|  |  | HT | 0 | 0 | 0 | 0 |  |  |
|  |  | Bus | 0 | 0 | 0 | 0 |  |  |
|  |  | Moto | 0 | 0 | 0 | 0 |  |  |
|  | I－205 SB Off－Ramp | Autos | 0 | 194 | 0 | 776 | 0 | 32 |
|  |  | MT | 0 | 4 | 0 | 16 |  |  |
|  |  | HT | 0 | 1 | 0 | 4 |  |  |
|  |  | Bus | 0 | 0 | 0 | 0 |  |  |
|  |  | Moto | 0 | 0 | 0 | 0 |  |  |
| Structure <br> Radiated <br> Noise <br> Measureme <br> nt West <br> Linn 6－19－ <br> 2018 | I－205 | Autos | 807 | 625 | 3228 | 2500 | 50 | 55 |
|  |  | MT | 38 | 29 | 152 | 116 |  |  |
|  |  | HT | 54 | 52 | 216 | 208 |  |  |
|  |  | Bus | 0 | 0 | 0 | 0 |  |  |
|  |  | Moto | 0 | 0 | 0 | 0 |  |  |
|  | $\begin{array}{\|l} \hline \text { I-205 NB On- } \\ \text { Ramp } \end{array}$ | Autos | 67 | 0 | 268 | 0 | 30 | 0 |
|  |  | MT | 0 | 0 | 0 | 0 |  |  |
|  |  | HT | 0 | 0 | 0 | 0 |  |  |
|  |  | Bus | 0 | 0 | 0 | 0 |  |  |
|  |  | Moto | 0 | 0 | 0 | 0 |  |  |
|  | I－205 SB Off－Ramp | Autos | 0 | 188 | 0 | 752 | 0 | 32 |
|  |  | MT | 0 | 4 | 0 | 16 |  |  |
|  |  | HT | 0 | 2 | 0 | 8 |  |  |
|  |  | Bus | 0 | 0 | 0 | 0 |  |  |
|  |  | Moto | 0 | 0 | 0 | 0 |  |  |

Source：HMMH， 2018

## Notes for the tables that follow:

1. All Vehicles volume from Synchro Network.
2. Assume Autos, Buses, Medium Trucks, Heavy Trucks and Motorcycle percentages calculated using TMC counts during 12-1 p.m. on May 23, 2017.

| Existing 2017 Truck Peak Hour (12:00-1:00 PM) I-205 Mainline |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Direction | Link | Speed, mph | All Vehicles ${ }^{1}$ | Motorcycles ${ }^{2}$ | Autos ${ }^{2}$ | Buses ${ }^{2}$ | Medium <br> Trucks ${ }^{2}$ | Heavy Trucks ${ }^{2}$ |
| Northbound | I-5 to Stafford Exit | Car 65; Truck 55 | 3,025 | 21 | 2,610 | 6 | 119 | 269 |
| Northbound | Stafford Exit to Stafford Entrance | Car 65; Truck 55 | 2,748 | 19 | 2,371 | 5 | 108 | 245 |
| Northbound | Stafford Entrance to 10th St Exit | Car 65; Truck 55 | 3,059 | 21 | 2,639 | 6 | 120 | 272 |
| Northbound | 10th St Exit to 10th St Entrance | 55 | 2,729 | 19 | 2,354 | 5 | 107 | 243 |
| Northbound | 10th St Entrance OR 43 Exit | 55 | 3,133 | 22 | 2,703 | 6 | 123 | 279 |
| Northbound | OR 43 Exit to OR 43 Loop Entrance | 55 | 2,873 | 20 | 2,479 | 6 | 113 | 256 |
| Northbound | OR 43 Loop Entrance to OR 43 Slip Entrance | 55 | 3,382 | 24 | 2,918 | 6 | 133 | 301 |
| Northbound | OR 43 Slip Entrance to OR 99E Exit | 55 | 3,585 | 25 | 3,093 | 7 | 141 | 319 |
| Northbound | OR 99E Exit to OR 99E Entrance | 55 | 3,010 | 21 | 2,597 | 6 | 118 | 268 |
| Northbound | OR 99E Entrance to OR 213 Exit | 55 | 3,957 | 28 | 3,414 | 8 | 155 | 352 |
| Northbound | OR 213 Exit to OR 213 Entrance | 55 | 3,124 | 22 | 2,695 | 6 | 123 | 278 |
| Northbound | OR 213 Entrance to 82nd Dr Exit | 55 | 4,699 | 33 | 4,054 | 9 | 184 | 418 |
| Southbound | 82nd Dr Entrance to OR 213 Exit | 55 | 4,492 | 33 | 3,941 | 3 | 150 | 364 |


| Existing 2017 Truck Peak Hour (12:00-1:00 PM) I-205 Mainline |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Direction | Link | Speed, mph | All Vehicles ${ }^{1}$ | Motorcycles ${ }^{2}$ | Autos ${ }^{2}$ | Buses ${ }^{2}$ | Medium <br> Trucks ${ }^{2}$ | Heavy Trucks ${ }^{2}$ |
| Southbound | OR 213 Exit to OR 213 Entrance | 55 | 2,822 | 21 | 2,476 | 2 | 94 | 229 |
| Southbound | OR 213 Entrance to OR 99E Exit | 55 | 3,516 | 26 | 3,085 | 2 | 118 | 285 |
| Southbound | OR 99E Exit to OR 99E Entrance | 55 | 2,661 | 20 | 2,335 | 2 | 89 | 216 |
| Southbound | OR 99E Entrance to OR 43 Exit | 55 | 3,276 | 24 | 2,874 | 2 | 110 | 266 |
| Southbound | OR 43 Exit to OR 43 Entrance | 55 | 2,582 | 19 | 2,265 | 2 | 86 | 209 |
| Southbound | OR 43 Entrance to 10th St Exit | 55 | 2,837 | 21 | 2,489 | 2 | 95 | 230 |
| Southbound | 10th St Exit to 10th St Entrance | 55 | 2,406 | 18 | 2,111 | 2 | 81 | 195 |
| Southbound | 10th St Entrance to Stafford Exit | Car 65; Truck 55 | 2,729 | 20 | 2,394 | 2 | 91 | 221 |
| Southbound | Stafford Exit to Stafford Entrance | Car 65; Truck 55 | 2,433 | 18 | 2,135 | 2 | 81 | 197 |
| Southbound | Stafford Entrance to l-5 Exit | Car 65; Truck 55 | 2,745 | 20 | 2,408 | 2 | 92 | 223 |

Source: HDR, 2017
Existing 2017 Truck Peak Hour (12:00-1:00 PM) I-205 Ramps

| Direction | Link | Speed, mph | All Vehicles ${ }^{1}$ | Motorcycles ${ }^{2}$ | Autos ${ }^{2}$ | Buses ${ }^{2}$ | Medium <br> Trucks ${ }^{2}$ | Heavy Trucks ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Northbound | I-205 NB Stafford Exit Ramp | 45 | 277 | 2 | 246 | 0 | 16 | 13 |
| Northbound | I-205 NB Stafford Entrance Ramp | Car 65; Truck 55 | 309 | 2 | 281 | 1 | 18 | 7 |

Existing 2017 Truck Peak Hour (12:00-1:00 PM) I-205 Ramps

| Direction | Link | Speed, mph | All Vehicles ${ }^{1}$ | Motorcycles ${ }^{2}$ | Autos ${ }^{2}$ | Buses ${ }^{2}$ | Medium Trucks ${ }^{2}$ | Heavy <br> Trucks ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Northbound | I-205 NB 10th Ave Exit Ramp | 45 | 330 | 1 | 319 | 0 | 7 | 3 |
| Northbound | I-205 NB 10th Ave Entrance Ramp | 55 | 402 | 1 | 379 | 0 | 16 | 6 |
| Northbound | I-205 NB OR 43 Exit Ramp | 35 | 260 | 4 | 247 | 2 | 6 | 1 |
| Northbound | I-205 NB OR 43 Loop Entrance Ramp | 55 | 489 | 1 | 462 | 4 | 13 | 10 |
| Northbound | I-205 NB OR 43 Slip Entrance Ramp | 55 | 203 | 3 | 184 | 1 | 5 | 10 |
| Northbound | I-205 NB OR99 Exit Ramp | 30 | 575 | 3 | 532 | 6 | 20 | 14 |
| Northbound | I-205 NB OR99 Entrance Ramp | 55 | 947 | 9 | 853 | 4 | 41 | 40 |
| Northbound | I-205 NB OR 213 Exit Ramp | 35 | 833 | 4 | 775 | 6 | 31 | 17 |
| Northbound | I-205 NB OR 213 Entrance Ramp | 55 | 1,575 | 10 | 1452 | 7 | 51 | 55 |
| Southbound | I-205 SB OR 213 Exit Ramp | 25 | 1,670 | 10 | 1557 | 5 | 58 | 40 |
| Southbound | I-205 SB OR 213 Entrance Ramp | 55 | 694 | 5 | 649 | 1 | 25 | 14 |
| Southbound | I-205 SB OR99 Exit Ramp | 45 | 855 | 9 | 782 | 3 | 21 | 40 |
| Southbound | I-205 SB OR99 Entrance Ramp | 55 | 615 | 5 | 567 | 6 | 20 | 17 |
| Southbound | I-205 SB OR 43 Exit Ramp | 40 | 694 | 2 | 642 | 6 | 22 | 22 |
| Southbound | I-205 SB OR 43 Entrance Ramp | 55 | 255 | 1 | 243 | 0 | 7 | 4 |
| Southbound | I-205 SB 10th Ave Exit Ramp | 45 | 431 | 1 | 410 | 0 | 14 | 6 |
| Southbound | I-205 SB 10th Ave Entrance Ramp | Car 65; Truck 55 | 320 | 3 | 301 | 3 | 8 | 5 |
| Southbound | I-205 SB Stafford Exit Ramp | 45 | 296 | 5 | 265 | 3 | 15 | 8 |
| Southbound | I-205 SB Stafford Entrance Ramp | Car 65; Truck 55 | 312 | 1 | 290 | 2 | 10 | 9 |

Source: HDR, 2017

| Existing 2017 Truck Peak Hour (12:00-1:00 PM) Side Street |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Road | Direction | Ramp Terminal Intersection Links | Speed, mph |  | Motorcycles 2 | Autos <br> 2 | Buses | Medium Trucks ${ }^{2}$ | Heavy <br> Trucks |
| Stafford Rd | Northbound | South of I-205 NB Ramps | 45 | 345 | 3 | 333 | 0 | 7 | 2 |
|  | Northbound | Between Stafford Ramp Terminals | 45 | 382 | 3 | 348 | 0 | 18 | 13 |
|  | Northbound | North of I-205 SB Ramps | 45 | 502 | 6 | 442 | 1 | 32 | 21 |
|  | Southbound | North of I-205 SB Ramps | 45 | 527 | 5 | 476 | 3 | 29 | 14 |
|  | Southbound | Between Stafford Ramp Terminals | 45 | 405 | 6 | 369 | 3 | 18 | 9 |
|  | Southbound | South of I-205 NB Ramps | 45 | 334 | 6 | 317 | 2 | 5 | 4 |
| 10th Ave | Northbound | South of 8th Ct | 25 | 366 | 3 | 345 | 2 | 11 | 5 |
|  | Northbound | Between 8th Ct and NB Ramp Terminal | 25 | 540 | 3 | 517 | 2 | 13 | 5 |
|  | Northbound | Between 10th Ramp Terminals | 25 | 507 | 2 | 484 | 3 | 16 | 2 |
|  | Northbound | Between Blankenship Rd and SB Ramp Terminal | 25 | 616 | 0 | 590 | 2 | 17 | 7 |
|  | Southbound | Between SB Ramp Terminal and Blankenship | 25 | 628 | 1 | 600 | 2 | 17 | 8 |
|  | Southbound | Between 10th Ramp Terminals | 25 | 630 | 1 | 607 | 0 | 16 | 6 |
|  | Southbound | Between NB Ramp Terminal and 8th Ct | 25 | 588 | 2 | 571 | 0 | 11 | 4 |
|  | Southbound | South of 8th Ct | 25 | 383 | 0 | 371 | 0 | 10 | 2 |
| OR 43 | Northbound | South of Willamette Falls Dr. | 25 | 422 | 3 | 411 | 0 | 2 | 6 |
|  | Northbound | Between Willamette Falls Dr. and I-205 NB Ramps | 35 | 461 | 4 | 436 | 1 | 9 | 11 |
|  | Northbound | Between OR 43 Ramp Terminals | 35 | 369 | 4 | 353 | 1 | 9 | 2 |


| Existing 2017 Truck Peak Hour (12:00-1:00 PM) Side Street |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Road | Direction | Ramp Terminal Intersection Links | Speed, mph |  | Motorcycles <br> 2 | Autos <br> 2 | Buses <br> 2 | Medium Trucks ${ }^{2}$ | Heavy <br> Trucks <br> 2 |
|  | Northbound | North of I-205 SB Ramps | 35 | 806 | 3 | 754 | 6 | 28 | 15 |
|  | Southbound | North of I-205 SB Ramps | 35 | 852 | 1 | 807 | 6 | 25 | 13 |
|  | Southbound | Between I-205 SB Ramp and NB Loop Ramp | 35 | 854 | 1 | 806 | 7 | 22 | 18 |
|  | Southbound | Between I-205 Ramp Terminals | 35 | 345 | 1 | 323 | 3 | 10 | 8 |
|  | Southbound | Between I-205 NB Ramp and Willimatte Falls Dr. | 35 | 494 | 2 | 469 | 4 | 11 | 8 |
|  | Southbound | South of Willamette Falls Dr. | 25 | 435 | 1 | 427 | 0 | 2 | 5 |
| Willamette Falls Dr. | Eastbound | West of W A St | 35 | 274 | 3 | 260 | 2 | 5 | 4 |
|  | Eastbound | Between W A St and Broadway St | 35 | 296 | 3 | 276 | 1 | 8 | 8 |
|  | Eastbound | Between Broadway St and OR 43 | 35 | 307 | 4 | 286 | 1 | 8 | 8 |
|  | Westbound | Between OR 43 and Broadway | 35 | 298 | 3 | 278 | 4 | 8 | 5 |
|  | Westbound | Between Broadway and W A St | 35 | 294 | 3 | 277 | 4 | 5 | 5 |
|  | Westbound | West of W A St | 35 | 313 | 3 | 299 | 4 | 5 | 2 |
| W A St | Northbound | North of Willamette Falls Dr. | 20 | 70 | 0 | 64 | 2 | 0 | 4 |
|  | Southbound | North of Willamette Falls Dr. | 20 | 111 | 0 | 102 | 1 | 3 | 5 |
| Broadway St | Northbound | North of Willamette Falls Dr. | 20 | 17 | 0 | 16 | 0 | 0 | 1 |
|  | Southbound | North of Willamette Falls Dr. | 20 | 15 | 0 | 15 | 0 | 0 | 0 |
| OR 99E | Northbound | South of 14th Ave | 30 | 1,058 | 9 | 958 | 14 | 38 | 39 |
|  | Northbound | Between 14th Ave and I-205 NB Ramps | 30 | 1,515 | 14 | 1,400 | 17 | 41 | 43 |


| Existing 2017 Truck Peak Hour (12:00-1:00 PM) Side Street |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Road | Direction | Ramp Terminal Intersection Links | Speed, mph |  | Motorcycles <br> 2 | Autos <br> 2 | Buses <br> 2 | Medium Trucks ${ }^{2}$ | Heavy Trucks 2 |
|  | Northbound | Between OR99 Ramp Terminals | 30 | 1,357 | 11 | 1,271 | 20 | 30 | 25 |
|  | Northbound | Between I-205 SB Ramps and Dunes Dr. | 30 | 1,532 | 11 | 1,449 | 18 | 30 | 24 |
|  | Northbound | North of Dunes Dr. | 30 | 1,222 | 6 | 1,160 | 18 | 25 | 13 |
|  | Southbound | North of Dunes Dr. | 30 | 1,274 | 9 | 1,200 | 16 | 34 | 15 |
|  | Southbound | Between Dunes Dr. and I-205 SB Ramps | 30 | 1,474 | 8 | 1,388 | 18 | 37 | 23 |
|  | Southbound | Between OR99 Ramp Terminals | 30 | 1,559 | 15 | 1,438 | 17 | 41 | 48 |
|  | Southbound | Between I-205 NB Ramps and 14th Ave | 30 | 1,341 | 12 | 1,236 | 16 | 32 | 45 |
|  | Southbound | South of 14th Ave | 30 | 988 | 9 | 895 | 14 | 25 | 45 |
| OR 213 | Northbound | South of I-205 NB Ramps | 45 | 2,288 | 15 | 2,117 | 10 | 74 | 72 |
|  | Northbound | Between OR 213 Ramp Terminals | 45 | 708 | 5 | 660 | 1 | 28 | 14 |
|  | Northbound | North of I-205 SB Ramps | 45 | 45 | 0 | 41 | 0 | 4 | 0 |
|  | Southbound | North of I-205 NB Ramps | 45 | 49 | 0 | 43 | 0 | 6 | 0 |
|  | Southbound | Between OR 213 Ramp Terminals | 45 | 1,691 | 6 | 1,591 | 3 | 47 | 44 |
|  | Southbound | South of I-205 NB Ramps | 45 | 2,524 | 10 | 2,366 | 9 | 78 | 61 |

HDR, 2017

| Future 2045 No Build Truck Peak Hour (12:00-1:00 PM) I-205 Mainline |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Direction | Link | Speed, mph | All Vehicles ${ }^{1}$ | Motorcycles ${ }^{2}$ | Autos ${ }^{2}$ | Buses ${ }^{2}$ | Medium <br> Trucks ${ }^{2}$ | Heavy <br> Trucks ${ }^{2}$ |
| Northbound | I-5 to Stafford Exit | $\begin{gathered} \text { Car 65; Truck } \\ 55 \end{gathered}$ | 3,542 | 25 | 3,056 | 7 | 139 | 315 |
| Northbound | Stafford Exit to Stafford Entrance | $\begin{gathered} \text { Car 65; Truck } \\ 55 \end{gathered}$ | 3,185 | 22 | 2,748 | 6 | 125 | 284 |
| Northbound | Stafford Entrance to 10th St Exit | $\begin{gathered} \text { Car 65; Truck } \\ 55 \end{gathered}$ | 3,557 | 25 | 3,069 | 7 | 140 | 317 |
| Northbound | 10th St Exit to 10th St Entrance | 55 | 3,178 | 22 | 2,742 | 6 | 125 | 283 |
| Northbound | 10th St Entrance OR 43 Exit | 55 | 3,648 | 26 | 3,147 | 7 | 143 | 325 |
| Northbound | OR 43 Exit to OR 43 Loop Entrance | 55 | 3,364 | 24 | 2,902 | 6 | 132 | 300 |
| Northbound | OR 43 Loop Entrance to OR 43 Slip Entrance | 55 | 3,995 | 28 | 3,447 | 8 | 157 | 356 |
| Northbound | OR 43 Slip Entrance to OR 99E Exit | 55 | 4,255 | 30 | 3,671 | 8 | 167 | 379 |
| Northbound | OR 99E Exit to OR 99E Entrance | 55 | 3,544 | 25 | 3,058 | 7 | 139 | 316 |
| Northbound | OR 99E Entrance to OR 213 Exit | 55 | 4,634 | 33 | 3,998 | 9 | 182 | 413 |
| Northbound | OR 213 Exit to OR 213 Entrance | 55 | 3,595 | 25 | 3,102 | 7 | 141 | 320 |
| Northbound | OR 213 Entrance to 82nd Dr Exit | 55 | 5,372 | 38 | 4,635 | 10 | 211 | 478 |
| Southbound | 82nd Dr Entrance to OR 213 Exit | 55 | 5,128 | 38 | 4,499 | 4 | 172 | 416 |
| Southbound | OR 213 Exit to OR 213 Entrance | 55 | 3,202 | 24 | 2,809 | 2 | 107 | 260 |
| Southbound | OR 213 Entrance to OR 99E Exit | 55 | 4,118 | 30 | 3,613 | 3 | 138 | 334 |
| Southbound | OR 99E Exit to OR 99E Entrance | 55 | 3,152 | 23 | 2,765 | 2 | 106 | 256 |


| Future 2045 No Build Truck Peak Hour (12:00-1:00 PM) I-205 Mainline |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Direction | Link | Speed, mph | All Vehicles ${ }^{1}$ | Motorcycles ${ }^{2}$ | Autos ${ }^{2}$ | Buses ${ }^{2}$ | Medium <br> Trucks ${ }^{2}$ | Heavy Trucks ${ }^{2}$ |
| Southbound | OR 99E Entrance to OR 43 Exit | 55 | 3,953 | 29 | 3,468 | 3 | 132 | 320 |
| Southbound | OR 43 Exit to OR 43 Entrance | 55 | 2,967 | 22 | 2,603 | 2 | 99 | 241 |
| Southbound | OR 43 Entrance to 10th St Exit | 55 | 3,234 | 24 | 2,837 | 2 | 108 | 262 |
| Southbound | 10th St Exit to 10th St Entrance | 55 | 2,593 | 19 | 2,275 | 2 | 87 | 210 |
| Southbound | 10th St Entrance to Stafford Exit | Car 65; Truck 55 | 2,958 | 22 | 2,595 | 2 | 99 | 240 |
| Southbound | Stafford Exit to Stafford Entrance | Car 65; Truck 55 | 2,600 | 19 | 2,281 | 2 | 87 | 211 |
| Southbound | Stafford Entrance to l-5 Exit | Car 65; Truck 55 | 3,025 | 22 | 2,654 | 2 | 101 | 245 |

HDR, 2017
Future 2045 No Build Truck Peak Hour (12:00-1:00 PM) I-205 Ramps

| Direction | Link | Speed, mph | All Vehicles ${ }^{1}$ | Motorcycles ${ }^{2}$ | Autos ${ }^{2}$ | Buses ${ }^{2}$ | Medium Trucks ${ }^{2}$ | Heavy <br> Trucks ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Northbound | I-205 NB Stafford Exit Ramp | 45 | 357 | 3 | 317 | 0 | 21 | 17 |
| Northbound | I-205 NB Stafford Entrance Ramp | Car 65; Truck 55 | 372 | 2 | 338 | 1 | 22 | 8 |
| Northbound | I-205 NB 10th Ave Exit Ramp | 45 | 379 | 1 | 366 | 0 | 8 | 3 |
| Northbound | I-205 NB 10th Ave Entrance Ramp | 55 | 470 | 1 | 443 | 0 | 19 | 7 |
| Northbound | I-205 NB OR 43 Exit Ramp | 35 | 284 | 4 | 270 | 2 | 7 | 1 |

Future 2045 No Build Truck Peak Hour (12:00-1:00 PM) I-205 Ramps

| Direction | Link | Speed, mph | All Vehicles ${ }^{1}$ | Motorcycles ${ }^{2}$ | Autos ${ }^{2}$ | Buses ${ }^{2}$ | Medium Trucks ${ }^{2}$ | Heavy <br> Trucks ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Northbound | I-205 NB OR 43 Loop Entrance Ramp | 55 | 631 | 1 | 596 | 5 | 16 | 13 |
| Northbound | I-205 NB OR 43 Slip Entrance Ramp | 55 | 260 | 4 | 236 | 1 | 6 | 13 |
| Northbound | I-205 NB OR99 Exit Ramp | 30 | 711 | 4 | 658 | 7 | 25 | 17 |
| Northbound | I-205 NB OR99 Entrance Ramp | 55 | 1,090 | 10 | 982 | 5 | 47 | 46 |
| Northbound | I-205 NB OR 213 Exit Ramp | 35 | 1,039 | 5 | 967 | 7 | 39 | 21 |
| Northbound | I-205 NB OR 213 Entrance Ramp | 55 | 1,777 | 11 | 1638 | 8 | 58 | 62 |
| Southbound | I-205 SB OR 213 Exit Ramp | 25 | 1,926 | 12 | 1796 | 6 | 67 | 46 |
| Southbound | I-205 SB OR 213 Entrance Ramp | 55 | 916 | 7 | 857 | 1 | 33 | 18 |
| Southbound | I-205 SB OR99 Exit Ramp | 45 | 966 | 10 | 884 | 3 | 24 | 45 |
| Southbound | I-205 SB OR99 Entrance Ramp | 55 | 801 | 7 | 738 | 8 | 26 | 22 |
| Southbound | I-205 SB OR 43 Exit Ramp | 40 | 986 | 3 | 912 | 9 | 31 | 31 |
| Southbound | I-205 SB OR 43 Entrance Ramp | 55 | 267 | 1 | 254 | 0 | 7 | 4 |
| Southbound | I-205 SB 10th Ave Exit Ramp | 45 | 641 | 1 | 610 | 0 | 21 | 9 |
| Southbound | I-205 SB 10th Ave Entrance Ramp | Car 65; Truck 55 | 365 | 3 | 343 | 3 | 9 | 6 |
| Southbound | I-205 SB Stafford Exit Ramp | 45 | 358 | 6 | 321 | 4 | 18 | 10 |
| Southbound | I-205 SB Stafford Entrance Ramp | Car 65; Truck 55 | 425 | 1 | 395 | 3 | 14 | 12 |

HDR, 2017

Future 2045 No Build Truck Peak Hour (12:00-1:00 PM) Side Street

| Road | Direction | Ramp Terminal Intersection Links | Speed, mph | All Vehicles 1 | Motorcycles <br> 2 | Autos <br> 2 | Buses $2$ | Medium <br> Trucks ${ }^{2}$ | Heavy <br> Trucks <br> 2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Stafford Rd | Northbound | South of I-205 NB Ramps | 45 | 557 | 5 | 538 | 0 | 11 | 3 |
|  | Northbound | Between Stafford Ramp Terminals | 45 | 606 | 5 | 552 | 0 | 29 | 21 |
|  | Northbound | North of I-205 SB Ramps | 45 | 666 | 8 | 586 | 1 | 42 | 28 |
|  | Southbound | North of I-205 SB Ramps | 45 | 756 | 7 | 683 | 4 | 42 | 20 |
|  | Southbound | Between Stafford Ramp Terminals | 45 | 634 | 9 | 578 | 5 | 28 | 14 |
|  | Southbound | South of I-205 NB Ramps | 45 | 570 | 10 | 541 | 3 | 9 | 7 |
| 10th Ave | Northbound | South of 8th Ct | 25 | 421 | 3 | 397 | 2 | 13 | 6 |
|  | Northbound | Between 8th Ct and NB Ramp Terminal | 25 | 609 | 3 | 583 | 2 | 15 | 6 |
|  | Northbound | Between 10th Ramp Terminals | 25 | 590 | 2 | 563 | 3 | 19 | 2 |
|  | Northbound | Between Blankenship Rd and SB Ramp Terminal | 25 | 710 | 0 | 680 | 2 | 20 | 8 |
|  | Southbound | Between SB Ramp Terminal and Blankenship | 25 | 711 | 1 | 679 | 2 | 19 | 9 |
|  | Southbound | Between 10th Ramp Terminals | 25 | 803 | 1 | 774 | 0 | 20 | 8 |
|  | Southbound | Between NB Ramp Terminal and 8th Ct | 25 | 741 | 3 | 720 | 0 | 14 | 5 |
|  | Southbound | South of 8th Ct | 25 | 537 | 0 | 520 | 0 | 14 | 3 |
| OR 43 | Northbound | South of Willamette Falls Dr. | 25 | 572 | 4 | 557 | 0 | 3 | 8 |
|  | Northbound | Between Willamette Falls Dr. and I-205 NB Ramps | 35 | 560 | 5 | 530 | 1 | 11 | 13 |
|  | Northbound | Between OR 43 Ramp Terminals | 35 | 434 | 5 | 415 | 1 | 11 | 2 |
|  | Northbound | North of I-205 SB Ramps | 35 | 1,117 | 4 | 1,045 | 8 | 39 | 21 |

Future 2045 No Build Truck Peak Hour (12:00-1:00 PM) Side Street

| Road | Direction | Ramp Terminal Intersection Links | Speed, mph |  | Motorcycles <br> 2 | Autos <br> 2 | Buses <br> 2 | Medium Trucks ${ }^{2}$ | Heavy <br> Trucks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Southbound | North of I-205 SB Ramps | 35 | 1,127 | 1 | 1,067 | 8 | 33 | 17 |
|  | Southbound | Between I-205 SB Ramps and NB Loop Ramp | 35 | 1,157 | 1 | 1,092 | 9 | 30 | 24 |
|  | Southbound | Between I-205 Ramp Terminals | 35 | 526 | 2 | 492 | 5 | 15 | 12 |
|  | Southbound | Between I-205 NB Ramp and Willimatte Falls Dr. | 35 | 666 | 3 | 632 | 5 | 15 | 11 |
|  | Southbound | South of Willamette Falls Dr. | 25 | 655 | 2 | 643 | 0 | 3 | 8 |
| Willamette Falls Dr. | Eastbound | West of W A St | 35 | 418 | 5 | 397 | 3 | 8 | 6 |
|  | Eastbound | Between W A St and Broadway St | 35 | 468 | 5 | 436 | 2 | 13 | 13 |
|  | Eastbound | Between Broadway St and OR 43 | 35 | 464 | 6 | 432 | 2 | 12 | 12 |
|  | Westbound | Between OR 43 and Broadway | 35 | 454 | 5 | 424 | 6 | 12 | 8 |
|  | Westbound | Between Broadway and W A St | 35 | 507 | 5 | 478 | 7 | 9 | 9 |
|  | Westbound | West of W A St | 35 | 458 | 4 | 438 | 6 | 7 | 3 |
| W A St | Northbound | North of Willamette Falls Dr. | 20 | 191 | 0 | 175 | 5 | 0 | 11 |
|  | Southbound | North of Willamette Falls Dr. | 20 | 192 | 0 | 176 | 2 | 5 | 9 |
| Broadway St | Northbound | North of Willamette Falls Dr. | 20 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | Southbound | North of Willamette Falls Dr. | 20 | 0 | 0 | 0 | 0 | 0 | 0 |
| OR 99E | Northbound | South of 14th Ave | 30 | 1,278 | 11 | 1,157 | 17 | 46 | 47 |
|  | Northbound | Between 14th Ave and I-205 NB Ramps | 30 | 1,932 | 18 | 1,785 | 22 | 52 | 55 |
|  | Northbound | Between OR99 Ramp Terminals | 30 | 1,777 | 14 | 1,664 | 26 | 39 | 33 |

Future 2045 No Build Truck Peak Hour (12:00-1:00 PM) Side Street

| Road | Direction | Ramp Terminal Intersection Links | Speed, mph | All <br> Vehicles <br> 1 | Motorcycles <br> 2 | Autos <br> 2 | Buses <br> 2 | Medium <br> Trucks ${ }^{2}$ | Heavy <br> Trucks <br> 2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Northbound | Between I-205 SB Ramps and Dunes Dr. | 30 | 1,463 | 11 | 1,384 | 17 | 29 | 23 |
|  | Northbound | North of Dunes Dr. | 30 | 1,323 | 6 | 1,256 | 19 | 27 | 14 |
|  | Southbound | North of Dunes Dr. | 30 | 1,357 | 10 | 1,278 | 17 | 36 | 16 |
|  | Southbound | Between Dunes Dr. and I-205 SB Ramps | 30 | 1,804 | 10 | 1,699 | 22 | 45 | 28 |
|  | Southbound | Between OR99 Ramp Terminals | 30 | 1,767 | 17 | 1,630 | 19 | 46 | 54 |
|  | Southbound | Between I-205 NB Ramps and 14th Ave | 30 | 1,507 | 13 | 1,389 | 18 | 36 | 51 |
|  | Southbound | South of 14th Ave | 30 | 1,148 | 10 | 1,040 | 16 | 29 | 52 |
| OR 213 | Northbound | South of I-205 NB Ramps | 45 | 2,920 | 19 | 2,702 | 13 | 94 | 92 |
|  | Northbound | Between OR 213 Ramp Terminals | 45 | 1,143 | 8 | 1,066 | 2 | 45 | 23 |
|  | Northbound | North of I-205 SB Ramps | 45 | 350 | 0 | 319 | 0 | 31 | 0 |
|  | Southbound | North of I-205 NB Ramps | 45 | 139 | 0 | 122 | 0 | 17 | 0 |
|  | Southbound | Between OR 213 Ramp Terminals | 45 | 1,936 | 7 | 1,822 | 3 | 54 | 50 |
|  | Southbound | South of I-205 NB Ramps | 45 | 2,975 | 12 | 2,789 | 11 | 92 | 72 |

HDR, 2017

Future 2045 Build Truck Peak Hour (12:00-1:00 PM) I-205 Mainline

| Direction | Link | Speed, mph | All <br> Vehicles ${ }^{1}$ | Motorcycles <br> 2 | Autos ${ }^{2}$ | Buses ${ }^{2}$ | Medium Trucks ${ }^{2}$ | Heavy Trucks ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Northbound | I-5 to Stafford Exit | $\begin{gathered} \text { Car 65; Truck } \\ 55 \\ \text { Car 65; Truck } \end{gathered}$ | 4,235 | 30 | 3,654 | 8 | 166 | 377 |
| Northbound | Stafford Exit to Stafford Entrance | $\begin{gathered} 55 \\ \text { Car 65; Truck } \end{gathered}$ | 3,958 | 28 | 3,415 | 8 | 155 | 352 |
| Northbound | Stafford Entrance to 10th St Exit | 55 | 4,403 | 31 | 3,799 | 8 | 173 | 392 |
| Northbound | 10th St Exit to 10th St Entrance | 55 | 3,941 | 28 | 3,400 | 8 | 155 | 351 |
| Northbound | 10th St Entrance OR 43 Exit | 55 | 4,424 | 31 | 3,817 | 8 | 174 | 394 |
| Northbound | OR 43 Exit to OR 43 Loop Entrance | 55 | 4,050 | 28 | 3,494 | 8 | 159 | 361 |
| Northbound | OR 43 Loop Entrance to OR 43 Slip Entrance | 55 | 4,645 | 33 | 4,007 | 9 | 182 | 414 |
| Northbound | OR 43 Slip Entrance to OR 99E Exit | 55 | 4,884 | 34 | 4,214 | 9 | 192 | 435 |
| Northbound | OR 99E Exit to OR 99E Entrance | 55 | 4,025 | 28 | 3,473 | 8 | 158 | 358 |
| Northbound | OR 99E Entrance to OR 213 Exit | 55 | 5,096 | 36 | 4,397 | 10 | 200 | 454 |
| Northbound | OR 213 Exit to OR 213 Entrance | 55 | 3,899 | 27 | 3,364 | 7 | 153 | 347 |
| Northbound | OR 213 Entrance to 82nd Dr Exit | 55 | 5,645 | 40 | 4,870 | 11 | 222 | 503 |
| Southbound | 82nd Dr Entrance to OR 213 Exit | 55 | 5,624 | 42 | 4,934 | 4 | 188 | 456 |
| Southbound | OR 213 Exit to OR 213 Entrance | 55 | 3,553 | 26 | 3,117 | 3 | 119 | 288 |
| Southbound | OR 213 Entrance to OR 99E Exit | 55 | 4,522 | 33 | 3,967 | 3 | 151 | 367 |
| Southbound | OR 99E Exit to OR 99E Entrance | 55 | 3,583 | 27 | 3,143 | 3 | 120 | 290 |
| Southbound | OR 99E Entrance to OR 43 Exit | 55 | 4,488 | 33 | 3,937 | 3 | 150 | 364 |
| Southbound | OR 43 Exit to OR 43 Entrance | 55 | 3,664 | 27 | 3,215 | 3 | 123 | 297 |
| Southbound | OR 43 Entrance to 10th St Exit | 55 | 4,072 | 30 | 3,573 | 3 | 136 | 330 |
| Southbound | 10th St Exit to 10th St Entrance | 55 | 3,463 | 26 | 3,038 | 2 | 116 | 281 |

Future 2045 Build Truck Peak Hour (12:00-1:00 PM) I-205 Mainline

| Direction | Link | Speed, mph | All Vehicles ${ }^{1}$ | Motorcycles <br> 2 | Autos ${ }^{2}$ | Buses ${ }^{2}$ | Medium <br> Trucks ${ }^{2}$ | Heavy Trucks ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Southbound | 10th St Entrance to Stafford Exit | Car 65; Truck 55 Car 65; Truck | 3,937 | 29 | 3,454 | 3 | 132 | 319 |
| Southbound | Stafford Exit to Stafford Entrance | $\begin{gathered} 55 \\ \text { Car 65; Truck } \end{gathered}$ | 3,427 | 25 | 3,007 | 2 | 115 | 278 |
| Southbound | Stafford Entrance to l-5 Exit | 55 | 3,757 | 28 | 3,296 | 3 | 126 | 305 |

HDR, 2017

Future 2045 Build Truck Peak Hour (12:00-1:00 PM) I-205 Ramps

| Direction | Link | Speed, mph | All Vehicles ${ }^{1}$ | Motorcycles ${ }^{2}$ | Autos ${ }^{2}$ | Buses ${ }^{2}$ | Medium <br> Trucks ${ }^{2}$ | Heavy <br> Trucks ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Northbound | I-205 NB Stafford Exit Ramp | 45 | 277 | 2 | 246 | 0 | 16 | 13 |
| Northbound | I-205 NB Stafford Entrance Ramp | Car 65; Truck 55 | 445 | 3 | 405 | 1 | 26 | 10 |
| Northbound | I-205 NB 10th Ave Exit Ramp | 45 | 462 | 1 | 447 | 0 | 10 | 4 |
| Northbound | I-205 NB 10th Ave Entrance Ramp | 55 | 483 | 1 | 455 | 0 | 19 | 7 |
| Northbound | I-205 NB OR 43 Exit Ramp | 35 | 374 | 6 | 355 | 3 | 9 | 1 |
| Northbound | I-205 NB OR 43 Loop Entrance Ramp | 55 | 595 | 1 | 562 | 5 | 15 | 13 |
| Northbound | I-205 NB OR 43 Slip Entrance Ramp | 55 | 239 | 4 | 217 | 1 | 6 | 12 |
| Northbound | I-205 NB OR99 Exit Ramp | 30 | 859 | 4 | 795 | 9 | 30 | 21 |
| Northbound | I-205 NB OR99 Entrance Ramp | 55 | 1,071 | 10 | 965 | 5 | 46 | 45 |
| Northbound | I-205 NB OR 213 Exit Ramp | 35 | 1,197 | 6 | 1114 | 9 | 45 | 24 |
| Northbound | I-205 NB OR 213 Entrance Ramp | 55 | 1,746 | 11 | 1610 | 8 | 57 | 61 |
| Southbound | I-205 SB OR 213 Exit Ramp | 25 | 2,071 | 12 | 1931 | 6 | 72 | 50 |
| Southbound | I-205 SB OR 213 Entrance Ramp | 55 | 969 | 7 | 906 | 1 | 35 | 20 |
| Southbound | I-205 SB OR99 Exit Ramp | 45 | 939 | 10 | 859 | 3 | 23 | 44 |
| Southbound | I-205 SB OR99 Entrance Ramp | 55 | 905 | 7 | 834 | 9 | 29 | 25 |
| Southbound | I-205 SB OR 43 Exit Ramp | 40 | 824 | 2 | 762 | 7 | 26 | 26 |

Future 2045 Build Truck Peak Hour (12:00-1:00 PM) I-205 Ramps

| Direction | Link | Speed, mph | All Vehicles ${ }^{1}$ | Motorcycles ${ }^{2}$ | Autos ${ }^{2}$ | Buses ${ }^{2}$ | Medium Trucks ${ }^{2}$ | Heavy <br> Trucks ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Southbound | I-205 SB OR 43 Entrance Ramp | 55 | 408 | 2 | 389 | 0 | 11 | 6 |
| Southbound | I-205 SB 10th Ave Exit Ramp | 45 | 609 | 1 | 579 | 0 | 20 | 8 |
| Southbound | I-205 SB 10th Ave Entrance Ramp | Car 65; Truck 55 | 474 | 4 | 446 | 4 | 12 | 7 |
| Southbound | I-205 SB Stafford Exit Ramp | 45 | 510 | 9 | 457 | 5 | 26 | 14 |
| Southbound | I-205 SB Stafford Entrance Ramp | Car 65; Truck 55 | 330 | 1 | 307 | 2 | 11 | 10 |

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| Road | Direction | Ramp Terminal Intersection Links | Speed <br> , mph | All Vehicles 1 | Motorcycles <br> 2 | Autos ${ }^{2}$ | Buses ${ }^{2}$ | Medium Trucks ${ }^{2}$ | Heavy Trucks ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Stafford Rd | Northbound | South of I-205 NB Ramps | 45 | 590 | 5 | 569 | - | 12 | 3 |
|  | Northbound | Between Stafford Ramp Terminals | 45 | 548 | 4 | 499 | - | 26 | 19 |
|  | Northbound | North of I-205 SB Ramps | 45 | 654 | 8 | 576 | 1 | 42 | 27 |
|  | Southbound | North of I-205 SB Ramps | 45 | 683 | 6 | 617 | 4 | 38 | 18 |
|  | Southbound | Between Stafford Ramp Terminals | 45 | 757 | 11 | 690 | 6 | 34 | 17 |
|  | Southbound | South of I-205 NB Ramps | 45 | 631 | 11 | 599 | 4 | 9 | 8 |
| 10th Ave | Northbound | South of 8th Ct | 25 | 435 | 4 | 410 | 2 | 13 | 6 |
|  | Northbound | Between 8th Ct and NB Ramp Terminal | 25 | 611 | 3 | 585 | 2 | 15 | 6 |
|  | Northbound | Between 10th Ramp Terminals | 25 | 645 | 3 | 616 | 4 | 20 | 3 |

Future 2045 Build Truck Peak Hour (12:00-1:00 PM) Side Street


Future 2045 Build Truck Peak Hour (12:00-1:00 PM) Side Street


Future 2045 Build Truck Peak Hour (12:00-1:00 PM) Side Street

| Road | Direction | Ramp Terminal Intersection Links | Speed <br> , mph | All Vehicles | Motorcycles <br> 2 | Autos ${ }^{2}$ | Buses ${ }^{2}$ | Medium Trucks ${ }^{2}$ | Heavy <br> Trucks ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Southbound | South of 14th Ave | 30 | 1,261 | 11 | 1,142 | 18 | 32 | 57 |
| OR 213 | Northbound | South of I-205 NB Ramps | 45 | 2,935 | 19 | 2,716 | 13 | 95 | 92 |
|  | Northbound | Between OR 213 Ramp Terminals | 45 | 1,189 | 8 | 1,108 | 2 | 47 | 24 |
|  | Northbound | North of I-205 SB Ramps | 45 | 349 | - | 318 | - | 31 | - |
|  | Southbound | North of I-205 NB Ramps | 45 | 147 | - | 129 | - | 18 | - |
|  | Southbound | Between OR 213 Ramp Terminals | 45 | 2,118 | 8 | 1,993 | 4 | 59 | 55 |
|  | Southbound | South of I-205 NB Ramps | 45 | 3,315 | 13 | 3,107 | 12 | 102 | 80 |

HDR, 2017

# Appendix D. Detailed Noise Abatement Analysis Tables 

Detailed Noise Abatement Analysis Acronyms
AFG Acoustical Feasibility Goal
E/C Effectiveness/Cost Metric
I.L. Insertion Loss

NRDG Noise Reduction Design Goal

| I205CW Stafford Road to OR212 Wall 1 |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $10^{\prime}$ | 12' | $14^{\prime}$ | $16^{\prime}$ | $18^{\prime}$ | $20^{\prime}$ | 22' | 24' | Units |
| Average Wtd I.L. (benefited) |  | 5 | 5.4 | 5.9 | 6.4 | 6.9 | 7.2 | 7.5 | dBA |
| Maximum I.L. | 4 | 5 | 6 | 7 | 8 | 9 | 9 | 10 | dBA |
| Benefited/Impacted $\geq$ AFG | 0 | 5 | 10 | 12 | 13 | 13 | 13 | 13 | \# of dwelling units |
| Benefited/Non Impact $\geq$ AFG | 0 | 0 | 1 | 3 | 3 | 4 | 4 | 4 | \# of dwelling units |
| Total Benefited | 0 | 5 | 11 | 15 | 16 | 17 | 17 | 17 | \# of dwelling units |
| Impacted Units $\geq$ NRDG | 0 | 0 | 0 | 3 | 6 | 11 | 11 | 11 | \# of dwelling units |
| Benefited Units $\geq$ NRDG | 0 | 0 | 0 | 3 | 6 | 11 | 12 | 12 | \# of dwelling units |
| Percent of impacts $\geq$ AFG | 0\% | 31\% | 63\% | 75\% | 81\% | 81\% | 81\% | 81\% | \% |
| Percent of benefits $\geq$ NRDG |  | 0\% | 0\% | 20\% | 38\% | 65\% | 71\% | 71\% | \% |
| "Cost-Reasonable" ? |  | No | No | No | No | No | No | No | ---- |
| Surface Area | 15,601 | 18,717 | 21,840 | 24,966 | 28,088 | 31,202 | 34,323 | 37,446 | sq-ft |
| Surface Area/Ben Rec |  | 3,743 | 1,985 | 1,664 | 1,756 | 1,835 | 2,019 | 2,203 | sq-ft / ben rec |
| Barrier Length | 1,560 | 1,560 | 1,560 | 1,560 | 1,560 | 1,560 | 1,560 | 1,560 | $f t$ |
| Min Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Max Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Avg Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Total Barrier Cost | 312,020 | 374,340 | 436,800 | 499,320 | 702,200 | 780,050 | 858,075 | 936,150 | \$ |
| Cost/Ben Rec |  | 74,868 | 39,709 | 33,288 | 43,888 | 45,885 | 50,475 | 55,068 | \$/ben rec |
| Effectiveness/Cost Metric (E/C) | - | - | - | 7.0 | 13.4 | 23.4 | 21.3 | 19.5 | ---- |


| ODOT Acoustical Feasibilty Goal (dBA) | 5 |
| :--- | :---: |
| ODOT Acoustical Feasibilty Goal (\%) | $51 \%$ |
| ODOT Noise Reduction Design Goal (dBA) | 7 |
| ODOT Noise Reduction Design Goal (\%) | $1 \%$ |




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| I205CW Stafford Road to OR213 Wall 2 |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10' | 12' | 14' | 16' | 18' | 20' | 22' | 24' | Units |
| Average Wtd I.L. (benefited) | 5.6 | 6.6 | 7.7 | 7.7 | 8.4 | 8.9 | 9.7 | 10 | dBA |
| Maximum I.L. | 7 | 9 | 10 | 11 | 12 | 13 | 14 | 14 | dBA |
| Benefited/Impacted $\geq$ AFG | 19 | 24 | 26 | 36 | 36 | 36 | 36 | 36 | \# of dwelling units |
| Benefited/Non Impact $\geq$ AFG | 3 | 5 | 8 | 12 | 16 | 18 | 18 | 19 | \# of dwelling units |
| Total Benefited | 22 | 29 | 34 | 48 | 52 | 54 | 54 | 55 | \# of dwelling units |
| Impacted Units $\geq$ NRDG | 3 | 14 | 24 | 24 | 29 | 34 | 35 | 35 | \# of dwelling units |
| Benefited Units $\geq$ NRDG | 3 | 14 | 26 | 29 | 36 | 43 | 47 | 49 | \# of dwelling units |
| Percent of impacts $\geq$ AFG | 46\% | 59\% | 63\% | 88\% | 88\% | 88\% | 88\% | 88\% | \% |
| Percent of benefits $\geq$ NRDG | 14\% | 48\% | 76\% | 60\% | 69\% | 80\% | 87\% | 89\% | \% |
| "Cost-Reasonable" ? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | ---- |
| Surface Area | 20,717 | 24,863 | 29,004 | 33,151 | 37,293 | 41,436 | 45,578 | 49,721 | sq-feet |
| Surface Area/Ben Rec | 942 | 857 | 853 | 691 | 717 | 767 | 844 | 904 | sq-ft / ben rec |
| Barrier Length | 2,070 | 2,070 | 2,070 | 2,070 | 2,070 | 2,070 | 2,070 | 2,070 | ft |
| Min Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Max Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Avg Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Total Barrier Cost | 414,340 | 497,260 | 580,080 | 828,775 | 932,325 | 1,035,900 | 1,139,450 | 1,243,025 | \$ |
| Cost/Ben Rec | 18,834 | 17,147 | 17,061 | 17,266 | 17,929 | 19,183 | 21,101 | 22,600 | \$ / ben rec |
| Effectiveness/Cost Metric (E/C) | 1.9 | 9.7 | 16.7 | 20.7 | 24.1 | 26.4 | 24.7 | 23.0 | ---- |

ODOT Acoustical Feasibilty Goal (dBA)
ODOT Acoustical Feasibilty Goal (\%) ODOT Noise Reduction Design Goal (dBA)
ODOT Noise Reduction Design Goal (\%)

| 5 |
| :---: |
| $51 \%$ |
| 7 |
| $1 \%$ |







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| I205CW Stafford Road to OR213 Wall 3 30' from Fog Line |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10' | 12' | 14' | 16' | 18' | $20^{\prime}$ | 22' | 24' | Units |
| Average Wtd I.L. (benefited) | 5 | 5.3 | 5.9 | 6.2 | 6.7 | 7.1 | 7.3 | 7.7 | dBA |
| Maximum I.L. | 5 | 6 | 7 | 8 | 9 | 10 | 10 | 11 | dBA |
| Benefited/Impacted $\geq$ AFG | 5 | 12 | 16 | 23 | 25 | 28 | 30 | 30 | \# of dwelling units |
| Benefited/Non Impact $\geq$ AFG | 0 | 0 | 2 | 2 | 5 | 7 | 7 | 8 | \# of dwelling units |
| Total Benefited | 5 | 12 | 18 | 25 | 30 | 35 | 37 | 38 | \# of dwelling units |
| Impacted Units $\geq$ NRDG | 0 | 0 | 4 | 10 | 13 | 17 | 21 | 24 | \# of dwelling units |
| Benefited Units $\geq$ NRDG | 0 | 0 | 4 | 10 | 15 | 19 | 23 | 28 | \# of dwelling units |
| Percent of impacts $\geq$ AFG | 12\% | 29\% | 39\% | 56\% | 61\% | 68\% | 73\% | 73\% | \% |
| Percent of benefits $\geq$ NRDG | 0\% | 0\% | 22\% | 40\% | 50\% | 54\% | 62\% | 74\% | \% |
| "Cost-Reasonable" ? | No | No | No | No | No | No | No | No | ---- |
| Surface Area | 21,586 | 25,907 | 30,226 | 34,537 | 38,857 | 43,176 | 47,497 | 51,821 | sq-feet |
| Surface Area/Ben Rec | 4,317 | 2,159 | 1,679 | 1,381 | 1,295 | 1,234 | 1,284 | 1,364 | sq-ft / ben rec |
| Barrier Length | 2,161 | 2,161 | 2,161 | 2,161 | 2,161 | 2,161 | 2,161 | 2,161 | ft |
| Min Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Max Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Avg Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Total Barrier Cost | 431,720 | 518,140 | 604,520 | 1,079,400 | 1,187,425 | 1,079,400 | 1,187,425 | 1,295,525 | \$ |
| Cost/Ben Rec | 86,344 | 43,178 | 33,584 | 43,176 | 39,581 | 30,840 | 32,093 | 34,093 | \$ / ben rec |
| Effectiveness/Cost Metric (E/C) | - | - | 1.4 | 4.3 | 6.0 | 8.2 | 9.7 | 10.5 | ---- |


| ODOT Acoustical Feasibilty Goal (dBA) | 5 |
| :--- | :---: |
| ODOT Acoustical Feasibilty Goal (\%) | $51 \%$ |
| ODOT Noise Reduction Design Goal (dBA) | 7 |
| ODOT Noise Reduction Design Goal (\%) | $1 \%$ |



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Federal Highway
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| I205CW Stafford Road to OR213 Wall 4 |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10' | 12' | 14' | 16' | 18' | 20' | 22' | $24^{\prime}$ | Units |
| Average Wtd I.L. (benefited) | 6.3 | 7.2 | 7.4 | 8 | 8.5 | 8.7 | 9.2 | 9.5 | dBA |
| Maximum I.L. | 10 | 12 | 13 | 14 | 15 | 16 | 17 | 17 | dBA |
| Benefited/Impacted $\geq$ AFG | 32 | 32 | 33 | 34 | 35 | 35 | 35 | 35 | \# of dwelling units |
| Benefited/Non Impact $\geq$ AFG | 14 | 25 | 42 | 48 | 51 | 56 | 57 | 59 | \# of dwelling units |
| Total Benefited | 46 | 57 | 75 | 82 | 86 | 91 | 92 | 94 | \# of dwelling units |
| Impacted Units $\geq$ NRDG | 16 | 29 | 32 | 32 | 32 | 32 | 32 | 32 | \# of dwelling units |
| Benefited Units $\geq$ NRDG | 17 | 34 | 43 | 48 | 62 | 72 | 76 | 78 | \# of dwelling units |
| Percent of impacts $\geq$ AFG | 86\% | 86\% | 89\% | 92\% | 95\% | 95\% | 95\% | 95\% | \% |
| Percent of benefits $\geq$ NRDG | 37\% | 60\% | 57\% | 59\% | 72\% | 79\% | 83\% | 83\% | \% |
| "Cost-Reasonable" ? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | ---- |
| Surface Area | 15,183 | 18,217 | 21,256 | 24,292 | 27,326 | 30,361 | 33,396 | 36,432 | sq-feet |
| Surface Area/Ben Rec | 330 | 320 | 283 | 296 | 318 | 334 | 363 | 388 | sq-ft / ben rec |
| Barrier Length | 1,517 | 1,517 | 1,517 | 1,517 | 1,517 | 1,517 | 1,517 | 1,517 | ft |
| Min Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Max Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Avg Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Total Barrier Cost | 303,660 | 364,340 | 425,120 | 485,840 | 683,150 | 759,025 | 834,900 | 910,800 | \$ |
| Cost/Ben Rec | 6,601 | 6,392 | 5,668 | 5,925 | 7,944 | 8,341 | 9,075 | 9,689 | \$ / ben rec |
| Effectiveness/Cost Metric (E/C) | 35.4 | 66.3 | 82.5 | 78.9 | 73.6 | 70.1 | 64.4 | 60.3 | -- |


| ODOT Acoustical Feasibilty Goal (dBA) | 5 |
| :--- | :---: |
| ODOT Acoustical Feasibilty Goal (\%) | $51 \%$ |
| ODOT Noise Reduction Design Goal (dBA) | 7 |
| ODOT Noise Reduction Design Goal (\%) | $1 \%$ |






_Optimization.Xsx Summary


Basic Noise Barrier Optimization Tool

| I205CW Stafford Road to OR213 Wall 5 |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $10^{\prime}$ | 12' | $14^{\prime}$ | $16^{\prime}$ | 18' | $20^{\prime}$ | $22^{\prime}$ | $24^{\prime}$ | Units |
| Average Wtd I.L. (benefited) Maximum I.L. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\begin{aligned} & \text { dBA } \\ & \text { dBA } \end{aligned}$ |
| Benefited/Impacted $\geq$ AFG | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | \# of dwelling units |
| Benefited/Non Impact $\geq$ AFG | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | \# of dwelling units |
| Total Benefited | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | \# of dwelling units |
| Impacted Units $\geq$ NRDG | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | \# of dwelling units |
| Benefited Units $\geq$ NRDG | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | \# of dwelling units |
| Percent of impacts $\geq$ AFG | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | \% |
| Percent of benefits $\geq$ NRDG |  |  |  |  |  |  |  |  | \% |
| "Cost-Reasonable" ? |  |  |  |  |  |  |  |  | ---- |
| Surface Area | 15,503 | 18,603 | 21,699 | 24,799 | 27,906 | 31,005 | 34,102 | 37,203 | sq-feet |
| Surface Area/Ben Rec |  |  |  |  |  |  |  |  | sq-ft / ben rec |
| Barrier Length | 1,550 | 1,550 | 1,550 | 1,550 | 1,550 | 1,550 | 1,550 | 1,550 | ft |
| Min Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Max Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Avg Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Total Barrier Cost | 310,060 | 372,060 | 433,980 | 619,975 | 697,650 | 775,125 | 852,550 | 930,075 | \$ |
| Cost/Ben Rec |  |  |  |  |  |  |  |  | \$ / ben rec |
| Effectiveness/Cost Metric (E/C) | - | - | - | - | - | - | - | - | ---- |


| ODOT Acoustical Feasibilty Goal (dBA) | 5 |
| :--- | :---: |
| ODOT Acoustical Feasibilty Goal (\%) | $51 \%$ |
| ODOT Noise Reduction Design Goal (dBA) | 7 |
| ODOT Noise Reduction Design Goal (\%) | $1 \%$ |

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| I205CW Stafford Road to OR213 Wall 6a |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10' | 12' | 14' | 16' | 18' | $20^{\prime}$ | 22' | $24^{\prime}$ | Units |
| Average Wtd I.L. (benefited) | 6.2 | 6.6 | 7 | 7.5 | 7.8 | 8.2 | 8.4 | 8.8 | dBA |
| Maximum I.L. | 10 | 11 | 11 | 12 | 13 | 13 | 13 | 14 | dBA |
| Benefited/Impacted $\geq$ AFG | 39 | 43 | 45 | 47 | 48 | 52 | 53 | 53 | \# of dwelling units |
| Benefited/Non Impact $\geq$ AFG | 15 | 24 | 29 | 35 | 37 | 40 | 44 | 48 | \# of dwelling units |
| Total Benefited | 54 | 67 | 74 | 82 | 85 | 92 | 97 | 101 | \# of dwelling units |
| Impacted Units $\geq$ NRDG | 21 | 30 | 39 | 44 | 46 | 48 | 51 | 52 | \# of dwelling units |
| Benefited Units $\geq$ NRDG | 21 | 32 | 44 | 55 | 65 | 74 | 80 | 83 | \# of dwelling units |
| Percent of impacts $\geq$ AFG | 71\% | 78\% | 82\% | 85\% | 87\% | 95\% | 96\% | 96\% | \% |
| Percent of benefits $\geq$ NRDG | 39\% | 48\% | 59\% | 67\% | 76\% | 80\% | 82\% | 82\% | \% |
| "Cost-Reasonable" ? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | ---- |
| Surface Area | 37,066 | 44,469 | 51,887 | 59,294 | 66,707 | 74,119 | 81,538 | 88,958 | sq-feet |
| Surface Area/Ben Rec | 686 | 664 | 701 | 723 | 785 | 806 | 841 | 881 | sq-ft / ben rec |
| Barrier Length | 3,697 | 3,697 | 3,697 | 3,697 | 3,697 | 3,697 | 3,697 | 3,697 | ft |
| Min Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Max Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Avg Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Total Barrier Cost | 741,320 | 889,380 | 1,037,740 | 1,482,350 | 1,667,675 | 1,852,975 | 2,038,450 | 2,223,950 | \$ |
| Cost/Ben Rec | 13,728 | 13,274 | 14,024 | 18,077 | 19,620 | 20,141 | 21,015 | 22,019 | \$ / ben rec |
| Effectiveness/Cost Metric (E/C) | 10.1 | 14.9 | 18.4 | 20.1 | 19.4 | 19.7 | 20.1 | 19.5 | ---- |


| ODOT Acoustical Feasibilty Goal (dBA) | 5 |
| :--- | :---: |
| ODOT Acoustical Feasibilty Goal (\%) | $51 \%$ |
| ODOT Noise Reduction Design Goal (dBA) | 7 |
| ODOT Noise Reduction Design Goal (\%) | $1 \%$ |








a_Optimization.xsx Summary

a_Optimization.xsx Summary

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Basic Noise Barrier Optimization Tool
11/10/2018

| I205CW Stafford Road to OR213 Wall 6b |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10' | 12' | $14^{\prime}$ | 16' | 18' | $20^{\prime}$ | 22' | $24^{\prime}$ | Units |
| Average Wtd I.L. (benefited) | 5.8 | 6.4 | 6.8 | 7.7 | 8.8 | 9.1 | 9.4 | 9.9 | dBA |
| Maximum I.L. | 8 | 9 | 10 | 10 | 11 | 11 | 12 | 12 | dBA |
| Benefited/Impacted $\geq$ AFG | 4 | 7 | 10 | 10 | 10 | 10 | 10 | 10 | \# of dwelling units |
| Benefited/Non Impact $\geq$ AFG | 1 | 1 | 1 | 1 | 1 | 3 | 4 | 4 | \# of dwelling units |
| Total Benefited | 5 | 8 | 11 | 11 | 11 | 13 | 14 | 14 | \# of dwelling units |
| Impacted Units $\geq$ NRDG | 1 | 3 | 5 | 9 | 10 | 10 | 10 | 10 | \# of dwelling units |
| Benefited Units $\geq$ NRDG | 1 | 3 | 5 | 10 | 11 | 11 | 11 | 11 | \# of dwelling units |
| Percent of impacts $\geq$ AFG | 40\% | 70\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | \% |
| Percent of benefits $\geq$ NRDG | 20\% | 38\% | 45\% | 91\% | 100\% | 85\% | 79\% | 79\% | \% |
| "Cost-Reasonable" ? | No | No | No | No | No | No | No | No | ---- |
| Surface Area | 11,636 | 13,960 | 16,294 | 18,619 | 20,953 | 23,268 | 25,603 | 27,927 | sq-feet |
| Surface Area/Ben Rec | 2,327 | 1,745 | 1,481 | 1,693 | 1,905 | 1,790 | 1,829 | 1,995 | sq-ft / ben rec |
| Barrier Length | 1,165 | 1,165 | 1,165 | 1,165 | 1,165 | 1,165 | 1,165 | 1,165 | ft |
| Min Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Max Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Avg Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Total Barrier Cost | 232,720 | 279,200 | 325,880 | 465,475 | 523,825 | 581,700 | 640,075 | 698,175 | \$ |
| Cost/Ben Rec | 46,544 | 34,900 | 29,625 | 42,316 | 47,620 | 44,746 | 45,720 | 49,870 | \$ / ben rec |
| Effectiveness/Cost Metric (E/C) | 4.3 | 17.2 | 33.8 | 53.2 | 52.5 | 55.9 | 54.7 | 50.1 | ---- |


| ODOT Acoustical Feasibilty Goal (dBA) | 5 |
| :--- | :---: |
| ODOT Acoustical Feasibilty Goal (\%) | $51 \%$ |
| ODOT Noise Reduction Design Goal (dBA) | 7 |
| ODOT Noise Reduction Design Goal (\%) | $1 \%$ |




U.S. Department of Transportañon

Federal Highway
Administration
Basic Noise Barrier Optimization Tool

| I205CW Stafford Road to OR213 Wall 7 |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $10^{\prime}$ | 12' | 14 | 16' | 18' | $20^{\prime}$ | 22' | 24' | Units |
| Average Wtd I.L. (benefited) | 6.2 | 6.4 | 6.7 | 7.3 | 8.2 | 8.8 | 8.8 | 9.3 | dBA |
| Maximum I.L. | 9 | 9 | 10 | 10 | 11 | 11 | 12 | 13 | dBA |
| Benefited/Impacted $\geq$ AFG | 6 | 8 | 11 | 12 | 12 | 12 | 12 | 12 | \# of dwelling units |
| Benefited/Non Impact $\geq$ AFG | 0 | 1 | 1 | 1 | 1 | 2 | 4 | 4 | \# of dwelling units |
| Total Benefited | 6 | 9 | 12 | 13 | 13 | 14 | 16 | 16 | \# of dwelling units |
| Impacted Units $\geq$ NRDG | 2 | 4 | 6 | 8 | 10 | 11 | 12 | 12 | \# of dwelling units |
| Benefited Units $\geq$ NRDG | 2 | 4 | 6 | 8 | 10 | 12 | 13 | 13 | \# of dwelling units |
| Percent of impacts $\geq$ AFG | 38\% | 50\% | 69\% | 75\% | 75\% | 75\% | 75\% | 75\% | \% |
| Percent of benefits $\geq$ NRDG | 33\% | 44\% | 50\% | 62\% | 77\% | 86\% | 81\% | 81\% | \% |
| "Cost-Reasonable" ? | No | No | Yes | Yes | No | No | No | No | ---- |
| Surface Area | 9,733 | 11,684 | 13,635 | 15,587 | 17,531 | 19,476 | 21,420 | 23,363 | sq-feet |
| Surface Area/Ben Rec | 1,622 | 1,298 | 1,136 | 1,199 | 1,349 | 1,391 | 1,339 | 1,460 | sq-ft / ben rec |
| Barrier Length | 989 | 989 | 989 | 989 | 989 | 989 | 989 | 989 | ft |
| Min Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Max Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Avg Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Total Barrier Cost | 194,660 | 233,680 | 272,700 | 311,740 | 438,275 | 486,900 | 535,500 | 584,075 | \$ |
| Cost/Ben Rec | 32,443 | 25,964 | 22,725 | 23,980 | 33,713 | 34,779 | 33,469 | 36,505 | \$ / ben rec |
| Effectiveness/Cost Metric (E/C) | 4.8 | 12.0 | 20.6 | 26.1 | 29.0 | 30.9 | 35.0 | 32.1 | -- |

ODOT Acoustical Feasibilty Goal (dBA)
ODOT Acoustical Feasibilty Goal (\%) ODOT Noise Reduction Design Goal (dBA)
ODOT Noise Reduction Design Goal (\%)

| 5 |
| :---: |
| $51 \%$ |
| 7 |
| $1 \%$ |




U.S. Department of Transportañon

Federal Highway
Administration
Basic Noise Barrier Optimization Tool

| I205CW Stafford Road to OR213 Wall 8 |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $10^{\prime}$ | 12' | 14' | 16' | 18' | 20' | 22' | 24' | Units |
| Average Wtd I.L. (benefited) | 6 | 6.9 | 7.1 | 7.8 | 7.4 | 7.4 | 7.4 | 7.6 | dBA |
| Maximum I.L. | 9 | 10 | 10 | 11 | 11 | 12 | 12 | 13 | dBA |
| Benefited/Impacted $\geq$ AFG | 7 | 8 | 10 | 10 | 11 | 12 | 12 | 12 | \# of dwelling units |
| Benefited/Non Impact $\geq$ AFG | 0 | 0 | 0 | 0 | 3 | 4 | 5 | 5 | \# of dwelling units |
| Total Benefited | 7 | 8 | 10 | 10 | 14 | 16 | 17 | 17 | \# of dwelling units |
| Impacted Units $\geq$ NRDG | 2 | 4 | 6 | 7 | 7 | 7 | 7 | 8 | \# of dwelling units |
| Benefited Units $\geq$ NRDG | 2 | 4 | 6 | 7 | 7 | 7 | 7 | 8 | \# of dwelling units |
| Percent of impacts $\geq$ AFG | 28\% | 32\% | 40\% | 40\% | 44\% | 48\% | 48\% | 48\% | \% |
| Percent of benefits $\geq$ NRDG | 29\% | 50\% | 60\% | 70\% | 50\% | 44\% | 41\% | 47\% | \% |
| "Cost-Reasonable" ? | Yes | Yes | Yes | No | Yes | Yes | Yes | Yes | ---- |
| Surface Area | 6,739 | 8,084 | 9,426 | 10,784 | 12,128 | 13,475 | 14,824 | 16,173 | sq-feet |
| Surface Area/Ben Rec | 963 | 1,011 | 943 | 1,078 | 866 | 842 | 872 | 951 | sq-ft / ben rec |
| Barrier Length | 683 | 683 | 683 | 683 | 683 | 683 | 683 | 683 | ft |
| Min Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Max Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Avg Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Total Barrier Cost | 134,780 | 161,680 | 188,520 | 269,600 | 303,200 | 336,875 | 370,600 | 404,325 | \$ |
| Cost/Ben Rec | 19,254 | 20,210 | 18,852 | 26,960 | 21,657 | 21,055 | 21,800 | 23,784 | \$ / ben rec |
| Effectiveness/Cost Metric (E/C) | 3.3 | 6.3 | 10.2 | 10.4 | 12.9 | 13.3 | 12.8 | 13.5 | -- |

ODOT Acoustical Feasibilty Goal (dBA)
ODOT Acoustical Feasibilty Goal (\%) ODOT Noise Reduction Design Goal (dBA)
ODOT Noise Reduction Design Goal (\%)

| 5 |
| :---: |
| $51 \%$ |
| 7 |
| $1 \%$ |




U.S. Department of transportanion

Federal Highway
Administration
Basic Noise Barrier Optimization Tool
8/3/2018

| $\begin{gathered} \hline \text { K19786CW } \\ \text { Wall } 9 \end{gathered}$ |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10' | 12' | 14' | 16' | 18' | 20' | 22' | $24^{\prime}$ | Units |
| Average Wtd I.L. (benefited) | 6.3 | 7.7 | 7 | 7.7 | 8.5 | 8.7 | 9.1 | 9.6 | dBA |
| Maximum I.L. | 7 | 9 | 10 | 11 | 11 | 12 | 12 | 13 | dBA |
| Benefited/Impacted $\geq$ AFG | 3 | 3 | 5 | 6 | 6 | 7 | 8 | 8 | \# of dwelling units |
| Benefited/Non Impact $\geq$ AFG | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | \# of dwelling units |
| Total Benefited | 3 | 3 | 5 | 6 | 6 | 7 | 8 | 8 | \# of dwelling units |
| Impacted Units $\geq$ NRDG | 2 | 2 | 2 | 4 | 6 | 6 | 6 | 7 | \# of dwelling units |
| Benefited Units $\geq$ NRDG | 2 | 2 | 2 | 4 | 6 | 6 | 6 | 7 | \# of dwelling units |
| Percent of impacts $\geq$ AFG | 18\% | 18\% | 29\% | 35\% | 35\% | 41\% | 47\% | 47\% | \% |
| Percent of benefits $\geq$ NRDG | 67\% | 67\% | 40\% | 67\% | 100\% | 86\% | 75\% | 88\% | \% |
| "Cost-Reasonable" ? | No | No | No | No | No | No | No | No | ---- |
| Surface Area | 5,940 | 7,131 | 8,318 | 9,506 | 10,696 | 11,884 | 13,070 | 14,258 | sq-feet |
| Surface Area/Ben Rec | 1,980 | 2,377 | 1,664 | 1,584 | 1,783 | 1,698 | 1,634 | 1,782 | sq-ft / ben rec |
| Barrier Length | 594 | 594 | 594 | 594 | 594 | 594 | 594 | 594 | ft |
| Min Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Max Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Avg Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Total Barrier Cost | 118,800 | 142,620 | 166,360 | 190,120 | 267,400 | 297,100 | 326,750 | 356,450 | \$ |
| Cost/Ben Rec | 39,600 | 47,540 | 33,272 | 31,687 | 44,567 | 42,443 | 40,844 | 44,556 | \$ / ben rec |
| Effectiveness/Cost Metric (E/C) | 3.5 | 2.9 | 4.2 | 8.7 | 11.6 | 12.2 | 12.7 | 13.6 | -- |


| ODOT Acoustical Feasibilty Goal (dBA) | 5 |
| :--- | :---: |
| ODOT Acoustical Feasibilty Goal (\%) | $51 \%$ |
| ODOT Noise Reduction Design Goal (dBA) | 7 |
| ODOT Noise Reduction Design Goal (\%) | $1 \%$ |





Basic Noise Barrier Optimization Tool

| $\begin{gathered} \hline \text { K19786CW } \\ \text { Wall } 10 \end{gathered}$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $9^{\prime}$ | 11' | $13^{\prime}$ | $15^{\prime}$ | 17' | Units |
| Average Wtd I.L. (benefited) |  | 5.0 | 5.3 | 5.3636364 | 5.3333333 | dBA |
| Maximum I.L. | 4.0 | 5.0 | 6.0 | 6.0 | 6.0 | dBA |
| Benefited/Impacted $\geq$ AFG | 0 | 4 | 6 | 7 | 7 | \# of dwelling units |
| Benefited/Non Impact $\geq$ AFG | 0 | 0 | 0 | 4 | 8 | \# of dwelling units |
| Total Benefited | 0 | 4 | 6 | 11 | 15 | \# of dwelling units |
| Impacted Units $\geq$ NRDG | 0 | 0 | 0 | 0 | 0 | \# of dwelling units |
| Benefited Units $\geq$ NRDG | 0 | 0 | 0 | 0 | 0 | \# of dwelling units |
| Percent of impacts $\geq$ AFG | 0\% | 33\% | 50\% | 58\% | 58\% | \% |
| Percent of benefits $\geq$ NRDG |  | 0\% | 0\% | 0\% | 0\% | \% |
| "Cost-Reasonable" ? |  | No | No | No | No | --- |
| Surface Area | 28,255 | 34,773 | 41,285 | 47,805 | 54,323 | sq-feet |
| Surface Area/Ben Rec |  | 8,693 | 6,881 | 4,346 | 3,622 | sq-ft / ben rec |
| Barrier Length | 3,257 | 3,257 | 3,257 | 3,257 | 3,257 | ft |
| Min Height | 9 | 11 | 13 | 15 | 17 | ft |
| Max Height | 9 | 11 | 13 | 15 | 17 | ft |
| Avg Height | 9 | 11 | 13 | 15 | 17 | ft |
| Total Barrier Cost | 565,100 | 695,460 | 825,700 | 956,100 | 1,358,075 | \$ |
| Cost/Ben Rec |  | 173,865 | 137,617 | 86,918 | 90,538 | \$/ben rec |
| Effectiveness/Cost Metric (E/C) |  | - | - | - | - | ---- |


| ODOT Acoustical Feasibilty Goal (dBA) | 5 |
| :--- | :---: |
| ODOT Acoustical Feasibilty Goal (\%) | $51 \%$ |
| ODOT Noise Reduction Design Goal (dBA) | 7 |
| ODOT Noise Reduction Design Goal (\%) | $1 \%$ |




Basic Noise Barrier Optimization Tool

| $\begin{gathered} \hline \text { K19786CW } \\ \text { Wall } 11 \end{gathered}$ |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10' | 12' | 14' | 16' | 18' | 20' | 22' | 24' | Units |
| Average Wtd I.L. (benefited) | 5 | 6 | 7.5 | 7 | 7.7 | 7.3 | 7.5 | 7.5 | dBA |
| Maximum I.L. | 5 | 7 | 9 | 10 | 11 | 11 | 12 | 12 | dBA |
| Benefited/Impacted $\geq$ AFG | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 4 | \# of dwelling units |
| Benefited/Non Impact $\geq$ AFG | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | \# of dwelling units |
| Total Benefited | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 4 | \# of dwelling units |
| Impacted Units $\geq$ NRDG | 0 | 1 | 1 | 1 | 2 | 2 | 2 | 2 | \# of dwelling units |
| Benefited Units $\geq$ NRDG | 0 | 1 | 1 | 1 | 2 | 2 | 2 | 2 | \# of dwelling units |
| Percent of impacts $\geq$ AFG | 20\% | 40\% | 40\% | 60\% | 60\% | 80\% | 80\% | 80\% | \% |
| Percent of benefits $\geq$ NRDG | 0\% | 50\% | 50\% | 33\% | 67\% | 50\% | 50\% | 50\% | \% |
| "Cost-Reasonable" ? | No | No | No | No | No | No | No | No | ---- |
| Surface Area | 11,451 | 13,741 | 16,032 | 18,321 | 20,612 | 22,902 | 25,192 | 27,482 | sq-feet |
| Surface Area/Ben Rec | 11,451 | 6,871 | 8,016 | 6,107 | 6,871 | 5,726 | 6,298 | 6,871 | sq-ft / ben rec |
| Barrier Length | 1,145 | 1,145 | 1,145 | 1,145 | 1,145 | 1,145 | 1,145 | 1,145 | ft |
| Min Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Max Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Avg Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Total Barrier Cost | 229,020 | 274,820 | 320,640 | 458,025 | 515,300 | 572,550 | 629,800 | 687,050 | \$ |
| Cost/Ben Rec | 229,020 | 137,410 | 160,320 | 152,675 | 171,767 | 143,138 | 157,450 | 171,763 | \$ / ben rec |
| Effectiveness/Cost Metric (E/C) | - | 5.8 | 5.0 | 6.5 | 11.6 | 14.0 | 12.7 | 11.6 | -- |


| ODOT Acoustical Feasibilty Goal (dBA) | 5 |
| :--- | :---: |
| ODOT Acoustical Feasibilty Goal (\%) | $51 \%$ |
| ODOT Noise Reduction Design Goal (dBA) | 7 |
| ODOT Noise Reduction Design Goal (\%) | $1 \%$ |





Basic Noise Barrier Optimization Tool
11/15/2018

| $\begin{gathered} \hline \text { K19786CW } \\ \text { Wall } 12 \end{gathered}$ |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $10^{\prime}$ | 12' | 14' | 16' | 18' | $20^{\prime}$ | 22' | $24^{\prime}$ | Units |
| Average Wtd I.L. (benefited) Maximum I.L. | 3 | 5 | 6 7 | 5.5 8 | 5.3 9 | $\begin{gathered} 5.7 \\ 9 \end{gathered}$ | $\begin{gathered} \hline 6 \\ 10 \end{gathered}$ | $\begin{gathered} 6.3 \\ 10 \end{gathered}$ | $\begin{aligned} & \mathrm{dBA} \\ & \mathrm{dBA} \end{aligned}$ |
| Benefited/Impacted $\geq$ AFG | 0 | 0 | 0 | 4 | 23 | 31 | 35 | 38 | \# of dwelling units |
| Benefited/Non Impact $\geq$ AFG | 0 | 1 | 3 | 9 | 23 | 35 | 41 | 43 | \# of dwelling units |
| Total Benefited | 0 | 1 | 3 | 13 | 46 | 66 | 76 | 81 | \# of dwelling units |
| Impacted Units $\geq$ NRDG | 0 | 0 | 0 | 0 | 0 | 6 | 14 | 19 | \# of dwelling units |
| Benefited Units $\geq$ NRDG | 0 | 0 | 1 | 2 | 3 | 11 | 23 | 35 | \# of dwelling units |
| Percent of impacts $\geq$ AFG | 0\% | 0\% | 0\% | 9\% | 53\% | 72\% | 81\% | 88\% | \% |
| Percent of benefits $\geq$ NRDG |  | 0\% | 33\% | 15\% | 7\% | 17\% | 30\% | 43\% | \% |
| "Cost-Reasonable" ? |  | No | No | No | Yes | Yes | Yes | Yes | ---- |
| Surface Area | 13,805 | 16,565 | 19,326 | 22,087 | 24,848 | 27,607 | 30,369 | 33,133 | sq-feet |
| Surface Area/Ben Rec |  | 16,565 | 6,442 | 1,699 | 540 | 418 | 400 | 409 | sq-ft / ben rec |
| Barrier Length | 1,381 | 1,381 | 1,381 | 1,381 | 1,381 | 1,381 | 1,381 | 1,381 | ft |
| Min Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Max Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Avg Height | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | ft |
| Total Barrier Cost | 276,100 | 331,300 | 386,520 | 441,740 | 621,200 | 690,175 | 759,225 | 828,325 | \$ |
| Cost/Ben Rec |  | 331,300 | 128,840 | 33,980 | 13,504 | 10,457 | 9,990 | 10,226 | \$ / ben rec |
| Effectiveness/Cost Metric (E/C) | - | - | - | - | - | 7.8 | 18.9 | 25.1 | ---- |


| ODOT Acoustical Feasibilty Goal (dBA) | 5 |
| :--- | :---: |
| ODOT Acoustical Feasibilty Goal (\%) | $51 \%$ |
| ODOT Noise Reduction Design Goal (dBA) | 7 |
| ODOT Noise Reduction Design Goal (\%) | $1 \%$ |





[^10]







[^0]:    ${ }^{1}$ ODOT Noise Policy (ODOT 2011) calculates barrier costs to the nearest $\$ 10$ increment.

[^1]:    ${ }^{2} 23$ CFR Part 772, as amended 75 FR 39820, July 13, 2010; Effective date July 13, 2011 - "Procedures for Abatement of Highway Traffic Noise and Construction Noise," Federal Highway Administration, U.S. Department of Transportation. http://www.ffwa.dot.gov/environment/noise/regulations and guidance/

    3 "Oregon Department of Transportation Noise Manual," July 13, 2011.
    http://www.oregon.gov/ODOT/GeoEnvironmental/Docs Environmental/Noise-Manual.pdf

[^2]:    ${ }^{4}$ There may have been an accident located further down I 205 out of sight.

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[^10]:    2_Optimization_NewiIS.XIsx Summary

