# Intersection Control Study 

Date: Friday, October 05, 2018
Project: ODOT | K19786 I-205: Stafford Rd to OR213 Corridor Widening and Abernethy Bridge Seismic Retrofit / Widening

To: Tom Hamstra, ODOT - PM
From: Steve Drahota, HDR - PM

| Subject: | Intersection Control Study |
| :--- | :--- |
|  | Conceptual Approval Request for Roundabout |
|  | Oswego Highway No. 3 at I-205 Northbound Exit-Ramp (Hwy No. 3 at MP |
|  | 11.29 \& Hwy No. 64 at MP 1C 8.79) |
|  | Clackamas County |

## 1 Introduction

### 1.1 Purpose and Background

The purpose of this Intersection Control Study (ICS) is to provide documentation required for the Conceptual Design Approval of a roundabout proposed at the intersection of Oswego Highway (Oregon Route (OR) 43) and Interstate (I) 205 northbound exit-ramp as part of the "I-205: Stafford Road to OR213 Project", key\# 19786. An ICS is a formal comparison of intersection control alternatives, in this case, a traffic signal and a roundabout.

The project proposes to widen l-205 by adding a third travel lane in both directions between the Stafford Road and OR99E Interchanges, and adding a northbound auxiliary lane between the OR99E entrance ramp and OR213 exit-ramp. The project also includes widening and seismically retrofitting the Abernethy Bridge. At the OR43 Interchange, in order to conform to the widened Abernethy Bridge and improve the safety and operations of I-205, the existing northbound OR43 to northbound l-205 entrance ramp will be removed. This movement will be redirected to a reconstructed entrance loop, which currently only serves the southbound OR43 to northbound $\mathrm{l}-205$ movement. A roundabout is proposed to be constructed at the northbound ramp terminal. Figure 1 shows the proposed improvements at the OR43 Interchange.

Figure 1. I-205 at OR43 Interchange - Proposed Improvements


### 1.2 Site Location and Study Area

The intersection of OR43 at I-205 northbound exit-ramp is located in the southern section of West Linn. It is currently signalized. The I-205 southbound ramp terminal is located approximately 850 feet to the north. Willamette Falls Drive, a City minor arterial, approaches from the west to create a T intersection with OR43 approximately 270 feet south of the proposed intersection. The Willamette Falls Drive approach is under stop control. The study area also includes the signalized intersection of OR43 and McKillican Street, which is approximately 950 feet north of the I-205 southbound ramp terminal. A map showing the study area is provided in Figure 2.

Figure 2. Study Area - OR43 between McKillican Street and Willamette Falls Drive


## 2 Traffic Data

### 2.1 AADT, Truck Percentage, and Posted Speed

I-205 serves as a major north-south regional transportation facility and the primary route to the East Portland metropolitan area. OR43 functions as the major north-south arterial through West Linn and includes turn lanes at the I-205 southbound and northbound ramp terminals as well as at Willamette Falls Drive and McKillican Street. Table 1 summarizes the roadway characteristics of I-205 and OR43 in the study area.

Table 1. Roadway Characteristics

| Highway | Milepoint | Segment | Number <br> of Lanes | 2016 <br> AADT | Truck <br> Percent- <br> age (\%) | Posted <br> Speed <br> (mph) |
| :---: | :---: | :--- | :---: | :---: | :---: | :---: |
| I-205 | 7.00 | 0.60 mile east of 10th Street Interchange | 4 | 92,600 | 6.3 | 55 |
| I-205 | 9.12 | On Willamette River Bridge (Abernethy <br> Bridge), 0.30 mile northeast of Oswego <br> Highway (OR43) Interchange | 6 | 106,300 | 6.3 | 55 |
| OR43 | 11.07 | 0.10 mile north of I-205 | $2-3$ | 21,500 | 2.7 | 35 |
| OR43 | 11.34 | 0.01 mile north of Willamette Falls Drive | 4 | 14,000 | 2.7 | 35 |
| OR43 | 11.43 | On Willamette River Bridge (Aka Oregon <br> City Arch Bridge) | 2 | 15,600 | 2.7 | 25 |

### 2.2 Crash History

### 2.2.1 OR43 from McKillican Street to Willamette Falls Drive (MP 10.88-11.36)

The reported crashes in the segment of OR43 between McKillican Street and Willamette Falls Drive were analyzed for the 5 -year period from 2012 through 2016. The majority of crashes occurred north of the l-205 southbound ramp terminal (60 percent [46 crashes]). Crashes were concentrated at the signalized intersection of OR43 and McKillican Street (MP 10.92) and the minor street stop-controlled T intersection of OR43 at Holly Street (MP 10.99), which is approximately 350 feet south of McKillican Street.

The crash analysis results are summarized below and Table 2 represents crash trends by severity, year and time of day. A detailed listing of the crash data is provided in Appendix A.

- Total Crashes - 76
- Fatal Crashes - None
- Serious Injury Crashes - One serious injury crash occurred at the I-205 southbound ramp terminal intersection. A southbound through driver disregarded the signal and hit a westbound vehicle turning left from the exit-ramp.
- Crash Typel Cause - The study segment of OR43 has a high percentage of turn movement crashes ( 43 percent [ 33 crashes]). The majority of the turning crashes occurred at intersections with McKillican Street (5 crashes), Holly Street (6 crashes), I-205 southbound exit-ramp ( 5 crashes), and Willamette Falls Drive ( 4 crashes). Many of them were caused by drivers who disregarded signal or failed to yield right-of-way.
- Crash Rate - The computed crash rate is 4.04 crashes per million vehicles miles (mvm), which is higher than the statewide average crash rate of 3.20 crashes per mvm. Potential factors attributed to the crashes include visibility of signals, congestion, and driveways at two gas stations just north of the I-205 southbound ramp terminal generating significant amount of traffic volumes.
- Top 10 percent SPIS - None

Table 2. Crash Data Summary

| OR43 MP 10.88-11.36 |  | Top 3 Most Frequent Collision Types |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Total | Turning | Rear End | Sideswipeopposite |
| Severity |  |  |  |  |
| Number of Fatal Crash | 0 | 0 | 0 | 0 |
| Number of Serious Injury Crash | 1 | 1 | 0 | 0 |
| Number of Moderate Injury Crash | 7 | 3 | 1 | 1 |
| Number of Minor Injury Crash | 32 | 10 | 16 | 2 |
| Number of Property Damage Only Crash | 36 | 19 | 11 | 3 |
| Total | 76 | 33 | 28 | 6 |
| Type and Year |  |  |  |  |
| 2012 | 14 | 5 | 7 | 0 |
| 2013 | 11 | 4 | 3 | 1 |
| 2014 | 15 | 7 | 5 | 1 |
| 2015 | 20 | 9 | 7 | 3 |
| 2016 | 16 | 8 | 6 | 1 |
| Total | 76 | 33 | 28 | 6 |
| Time of Day |  |  |  |  |
| Early Morning (12-7) | 5 | 2 | 1 | 0 |
| Morning Peak (7-9) | 6 | 4 | 1 | 1 |
| Mid-day (9-4) | 45 | 20 | 17 | 4 |
| Afternoon Peak (4-6) | 12 | 6 | 5 | 0 |
| Evening (6-12) | 8 | 1 | 4 | 1 |
| Total | 76 | 33 | 28 | 6 |

### 2.2.2 OR43 at l-205 Northbound Ramp Terminal

Since a roundabout is proposed to replace the existing signal control at the intersection of OR43 and I-205 northbound ramp terminal, an analysis of the crash history at this intersection was performed to determine current crash trends at the intersection.

There were a total of eleven crashes at the l-205 northbound ramp terminal intersection. The most severe injury type was moderate injury, which resulted from a fixed-object collision involving an intoxicated driver who exceeded the speed limit, ran off the l-205 northbound exit-ramp, and hit a tree. Rear-end ( 36 percent [ 4 crashes]) and turning movement ( 36 percent [ 4 crashes]) crashes are the top two most frequent collision types at this intersection. Of the four turning crashes, three were caused by a southbound through vehicle on OR43 that disregarded the traffic signal and hit an l-205 northbound exit-ramp vehicle turning left. No pedestrian or bicycle crashes occurred at this intersection. A detailed listing of the crash data is provided in Appendix B.

### 2.3 2017 Existing Traffic Volumes

Existing weekday AM and PM turning movement counts were collected on OR43 at its intersections with McKillican Street, I-205 southbound ramps, I-205 northbound ramps, and Willamette Falls Drive by ODOT Region 1 Traffic staff in May 2017. The AM and PM peak hours
were determined to occur between 7:30 AM and 8:30 AM and between 4:30 PM and 5:30 PM, respectively. The existing year 2017 AM and PM traffic volumes and lane configurations at the intersections on OR43 are provided in Figure 3.

Figure 3. Existing Year 2017 Traffic Volumes


Traffic analysis of the 2017 existing conditions was performed using Synchro (version 9.2), which is a traffic analysis and signal optimization software that emulates the methodology from the Highway Capacity Manual with SimTraffic serving as its accompanying micro-simulation application. SimTraffic was used to simulate alternatives and provide queue length statistics.

Table 3 provides volume-to-capacity ( $\mathrm{v} / \mathrm{c}$ ) ratio, average control delay, and resulting LOS for the four study intersections. The OR43/McKillican Street intersection operates at LOS C. The two interchange ramp terminal intersections operate with moderately low delay while the stop-controlled movement at the Willamette Falls Drive intersection is operating at LOS F and experiences delay exceeding two minutes for the side street approach. The delay for this intersection is primarily influenced by insufficient gaps in southbound OR43 traffic resulting in substantial delay for both right- and left-turning vehicles from Willamette Falls Drive during peak periods, despite having a two-stage median turn lane. Synchro/SimTraffic analysis worksheets are provided in Appendix C.

Table 3. OR43 Interchange Traffic Operations Analysis Results (2017 Existing)

| Intersection | Peak Hour | Delay (sec/veh) | LOS | VIC |
| :--- | :---: | :---: | :---: | :---: |
| OR43 at McKillican St | AM | 29.0 | C | 0.83 |
|  | PM | 32.9 | C | 0.79 |
| OR43 at I-205 SB Ramp Terminal | AM | 17.9 | B | 0.87 |
|  | PM | 16.9 | B | 0.69 |
| OR43 at I-205 NB Ramp Terminal | AM | 6.0 | A | 0.40 |
|  | PM | 4.7 | A | 0.33 |
|  | AM | $>120$ | F | ** |

**For unsignalized intersections, the delay is reported for the minor street left turn movement under stop control. Intersection v/c ratio is not reported for unsignalized intersections.

### 2.4 Design Year 2045 Traffic Volumes

The Metro Regional Travel Demand Models were used to forecast project future year demands. ODOT provided the Metro travel demand Visum models for existing year 2010 and future year 2040 AM and PM peak period conditions. These models encompass freeways, arterials, local streets, and intersections within the Portland region. The future year regional models integrate planned transportation projects outside of the project study area to generate reliable and realistic future volume forecasts. The future year Metro models were reviewed and adjusted with appropriate capacity and lane configurations for the no-build baseline scenario. Future build scenario models were developed by updating the no-build model with the widened I-205 freeway segment between OR99E and Stafford Road. Lane capacity and number of lanes were updated
per the proposed roadway design. Examination of the updated regional models identified that no local streets were missing in either the no-build or build scenarios.

The Difference (Incremental) Method was used to forecast future volumes as recommended by ODOT. This method is best suited to the study area because the other future demand forecasting method, the Growth Method, tends to severely overestimate growth on lower volume roadways. In the Difference Method, future year demand volumes are determined by adding the existing traffic counts and the differences between existing and future model volumes. Design year 2045 traffic volumes were developed through extrapolation using the differences between the 2010 and 2040 travel demand models. After developing the future year volumes, volumes were balanced to obtain a set of cohesive network volumes.

## 3 Development of Intersection Control Alternatives

Currently, there are two closely spaced I-205 northbound entrance ramps serving OR43, one from OR43 southbound and the other from OR43 northbound. In order to improve freeway safety and operations and accommodate the widened Abernethy Bridge, the I-205 northbound entrance ramp serving OR43 northbound will be removed, and the entrance loop ramp from OR43 southbound will be reconstructed to allow for the left turn movements from OR43 northbound. Two intersection control alternatives were evaluated to accommodate the left turn movements from OR43 northbound to l-205 northbound at the reconstructed northbound ramp terminal. These two alternatives are described below.

### 3.1 Signal Control

The initial intersection control alternative developed during the early conceptual design phase of the project was a traffic signal. Due to the heavy turning movements, dual left turn lanes were considered on OR43 northbound at its intersection with the l-205 northbound ramp terminal. The existing signal would be replaced to allow for the dual northbound left turn lanes on OR43. Due to the proximity of the adjacent intersections, the intersection of OR43 and Willamette Falls Drive was also assumed to be under signal control. The signal alternative also included a revised lane configuration of the l-205 southbound exit-ramp, through restriping, to accommodate the heavy right turn movement onto OR43 northbound in the existing and future traffic conditions. Figure 4 shows a conceptual design layout of this alternative along with the Design Year 2045 AM and PM peak hour volumes.

Figure 4. Signal Control Alternative - Design Year 2045 Traffic Volumes


### 3.2 Roundabout

As the project design was advanced, a roundabout alternative at the I-205 northbound ramp terminal was identified for consideration as a potential alternative to address safety and operational concerns related to the signalized intersection concept. The roundabout lane configurations and geometry were developed and refined through collaboration with ODOT Region and Salem Traffic-Roadway staff during the Design Verification Package (DVP) and Draft Design Acceptance Package (DAP) phases. For this alternative, no modification to the lane configuration or traffic control at the intersection of OR43 and Willamette Falls Drive was assumed. Similar to the signal alternative, the roundabout design option also included a revised lane configuration of the I-205 southbound exit-ramp, through restriping, to accommodate the heavy right turn movement onto OR43 northbound in the existing and future traffic conditions. Figure 5 shows the current conceptual design layout of the roundabout along with the Design Year 2045 AM and PM peak hour volumes.

Figure 5. Roundabout Alternative - Design Year 2045 Build Traffic Volumes


## 4 Intersection Control Evaluation

A traffic capacity analysis was performed to evaluate how each alternative would perform under Design Year 2045 AM and PM peak hour conditions. It should be noted that the existing ramp meter that regulates traffic entering from OR43 southbound will be removed and a new ramp meter will not be installed for the consolidated I-205 northbound entrance ramp under either alternative. This is due to the insufficient ramp meter storage on the realigned entrance ramp to accommodate the high combined traffic demand from OR43 southbound and northbound. Under current conditions the existing ramp meter has been observed to create queuing that extends beyond the entrance loop ramp and onto OR43 southbound. In either design alternative, the queuing related to a ramp metered condition would result in significant queuing into the new intersection, causing safety and operational issues on OR43. In addition to constructing the new third general purpose lane, the project will be extending the northbound auxiliary lane to the combined entrance loop, which will eliminate the existing short merge condition between I-205 and the entrance loop. For these reasons, a ramp meter will not be constructed with this project.

### 4.1 Capacity Analysis

### 4.1.1 Signal Control Alternative

Traffic analysis was performed using Synchro (version 9.2) with SimTraffic serving as its accompanying micro-simulation application used to provide queue length statistics. Table 4 provides the average control delay, resulting Level of Service (LOS), and volume-to-capacity (v/c) ratios for the four study intersections under the Design Year 2045 conditions. At the OR43 and I205 northbound ramp terminal, the v/c ratio of 0.79 in the 2045 PM peak hour would exceed the Highway Design Manual (HDM) mobility standard (v/c ratio) of 0.75 , which would require a design exception. Although the intersection will operate at an acceptable level of service from a traffic capacity perspective, the vehicle queue in the northbound inside left turn lane would well exceed the available storage as shown in Table 5. This implies that the queue of left-turning vehicles would extend through the upstream signalized intersection and impact the operations of OR43 and Willamette Falls Drive. Additionally, the short length of the second receiving lane on the I-205 entrance loop ramp would result in a low lane utilization rate for the dual turn lane, further affecting the capacity of the signal option.

Due to its proximity to the I-205 northbound ramp terminal, the OR43/Willamette Falls Drive intersection would have to operate on closely coordinated signal timing. This intersection also experiences heavy northbound left turn demands from OR43, which would result in significant queue lengths, particularly in the AM peak hour. During these peak operating conditions, the combined queue effect of northbound through and northbound left turns would result in a condition that creates extensive queuing beyond the intersections and continue over the Oregon City Arch Bridge and into downtown Oregon City. The long northbound queue would create conflicts with the driveways along OR43 between Willamette Falls Drive and the west end of the Oregon City Arch Bridge. One of the project goals was to maintain or improve existing operations on impacted connections while accommodating the third lane on I-205. Based on these traffic analysis findings, the signalized intersection alternative fails to meet one of the key project objectives of not degrading existing operations of an impacted facility.

Table 4. OR43 Interchange Traffic Operations Analysis Results (2045 Signal Alternative)

| Intersection | Peak Hour | Delay (sec/veh) | LOS | vIC |
| :--- | :---: | :---: | :---: | :---: |
| OR43 at McKillican St | AM | 34.1 | C | 0.86 |
|  | PM | 65.0 | E | 0.99 |
| OR43 at I-205 SB Ramp Terminal | AM | 31.0 | C | 0.86 |
|  | PM | 18.1 | B | 0.78 |
| OR43 at I-205 NB Ramp Terminal | AM | 16.7 | B | 0.66 |
|  | PM | 21.7 | C | 0.79 |
|  | AM | 27.6 | C | 0.79 |

Table 5. Design Year 2045 Intersection Operations - Signal Control

|  | Delay (sec/veh) | LOS | VIC | $95^{\text {th }}$ Percentile Queue ( ft ) |  | Available Storage (ft) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OR43 at l-205 NB Ramp Terminal |  |  |  | NB inside Left Turn Lane | NB Outside Left Turn Lane | NB inside Left Turn Lane | NB Outside Left Turn Lane |
| 2045 AM Peak Hour | 16.7 | B | 0.66 | 422 | 352 | *75 | *220 |
| 2045 PM Peak Hour | 21.7 | C | 0.79 | 252 | 287 | *75 | *220 |
| OR43 at Willamette Falls Drive | Delay (sec/veh) | LOS | VIC | $95^{\text {th }}$ Percentile Queue ( ft ) |  | Available Storage (ft) |  |
|  |  |  |  | NB Left Turn Lane | NB Thru Lane | NB Left Turn Lane | NB Thru Lane |
| 2045 AM Peak Hour | 27.6 | C | 0.79 | 380 | 779 | 200 | --- |
| 2045 PM Peak Hour | 20.4 | C | 0.71 | 314 | 550 | 200 | --- |

*Physical storage limit before the lane spilled into the adjacent signal at Willamette Falls Drive; total queue extend much further. Red = Queue length longer than available storage length

### 4.1.2 Roundabout Alternative

Sidra (version 7), which is primarily used to analyze roundabouts, was used to evaluate the OR43/l-205 northbound ramp terminal intersection under the Design Year 2045 Roundabout alternative. The Sidra results are based on Highway Capacity Manual 6 $6^{\text {th }}$ Edition output, which incorporates the latest NCHRP research and methodology for analyzing roundabouts in the U.S.

As part of the concept development for a Roundabout alternative, a single lane entrance ramp with no southbound right turn bypass lane concept was evaluated first. As shown in Table 6, this concept would result in an intersection v/c ratio of 0.95 in the 2045 PM peak hour due to the heavy southbound right turn to $\mathrm{I}-205$ northbound movement. This v/c ratio well exceeds the HDM
mobility standard of 0.75 for Build alternatives. A single northbound lane approaching the roundabout with a southbound right turn bypass lane concept was evaluated next. This concept would also result in a high intersection v/c ratio (0.99) in the 2045 AM peak hour due to the heavy northbound through movement, indicating the intersection would operate at capacity. The Sidra lane configuration layout and traffic capacity analysis results for these two concepts are provided in the Appendix D.

Based on evaluation of the two initial concepts, it was concluded that a southbound right turn bypass lane and a 2-lane northbound approach would be needed in order to achieve an acceptable v/c ratio. Consequently, the conceptual design layout shown in Figure 5 emerged and was selected as the preferred roundabout alternative. Table 6 provides the average control delay, resulting Level of Service (LOS), and volume-to-capacity (v/c) ratios for the intersection of OR43 and I-205 northbound ramp terminal under the Design Year 2045 conditions. As shown, the roundabout would operate at LOS A with very low vehicle delay due to the yield control entry. It also has a low v/c ratio in 2045 AM peak hour while the v/c ratio in the 2045 PM peak hour is slightly higher than the Highway Design Manual mobility standard of 0.75 . As shown in Table 7, the $95^{\text {th }}$ percentile vehicle queues in all the approach lanes are relatively short, ranging from two to nine vehicles ( 5 feet to 225 feet), indicating the roundabout operations would not impact the corridor immediately upstream from the roundabout intersection.

Table 6. Design Year 2045 Intersection Operations - Roundabout Alternative Lane Configurations

| Alternative | OR43 at I-205 NB <br> Ramp Terminal | Delay <br> (sec/veh) | LOS | V/C |
| :--- | :---: | :---: | :---: | :---: |
| Single lane entrance ramp with no <br> southbound right turn bypass lane <br> and with 2 northbound approach <br> lanes | 2045 PM Peak Hour | 12.6 | B | 0.95 |
| 2 lane entrance ramp with a <br> southbound right turn bypass lane <br> and a single northbound approach <br> lane | 2045 AM Peak Hour | 12.4 | B | 0.99 |
| Build Alternative - 2 lane entrance <br> ramp with a southbound bypass <br> lane and with 2 northbound <br> approach lanes | 2045 AM Peak Hour | 5.4 | A | 0.49 |
| Build Alternative - 2 lane entrance <br> ramp with a southbound bypass <br> lane and with 2 northbound <br> approach lanes | 2045 PM Peak Hour | 6.7 | A | 0.78 |

Red $=\mathrm{v} / \mathrm{c}$ ratio for roundabout intersection exceeds Highway Design Manual Mobility Standard of 0.75 for Build Alternative.

Table 7. Design Year 2045 Build 95th Percentile Queues at the OR43/I-205 NB Ramp Terminal - Roundabout Alternative

|  | $95^{\text {th }}$ percentile Queue Length (\# of vehicles - feet) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| OR43 at I-205 NB Ramp Terminal | OR43 SB Right Turn Bypass Lane | OR43 SB <br> Through Lane | Shared right/left Turn Lane on l-205 NB exit-ramp | OR43 NB inside Through Lane | OR43 NB outside Through Lane |
| 2045 AM Peak Hour | 0 vehicle | 3 veh. - 75' | 2 veh. - 50' | 3 veh. - 75' | 0 vehicle |
| 2045 PM Peak Hour | 0 vehicle | 9 veh. - $225^{\prime}$ | 2 veh. -50' | 3 veh. - 75' | 0 vehicle |

Synchro/SimTraffic was used to evaluate the operations of the other intersections in the corridor. The analysis results are shown in Table 8 below.

Table 8. OR43 Interchange Traffic Operations Analysis Results (2045) - Roundabout Alternative

| Intersection | Peak Hour | Delay (sec/veh) | LOS | VIC |
| :--- | :---: | :---: | :---: | :---: |
| OR43 at McKillican St | AM | 74.9 | E | 0.94 |
|  | PM | 49.8 | D | 0.98 |
| OR43 at I-205 SB Ramp Terminal | AM | 38.9 | D | 0.85 |
|  | PM | 18.6 | B | 0.77 |
| OR43 at I-205 NB Ramp Terminal | AM | ${ }^{*} 5.4$ | *A | ${ }^{*} 0.49$ |
|  | PM | *6.7 | *A | ${ }^{*} 0.78$ |

*Traffic operational results from Sidra Analysis
**For unsignalized intersections, the delay is reported for the minor street left turn movement under stop control. Intersection v/c ratio is not reported for unsignalized intersections.

In addition to the Synchro/SimTraffic and Sidra analysis for the study area, Vissim was used to evaluate the operations of vehicles exiting the roundabout in the corridor to ensure they would not be interrupted by queues from downstream intersections. Vissim is a widely-used, behavior-based, multi-purpose traffic micro-simulation program that tracks individual vehicle movements and interactions more realistically than typical Highway Capacity Manual methods. An existing condition Vissim model was developed for the study area, following the guidance in the 2011 ODOT Vissim Protocol. The existing conditions model was qualitatively calibrated based on field observations and served as the basis for developing the Design Year 2045 Build Condition model, which has been reviewed and ratified by ODOT Region 1 Traffic staff for use.

The OR43 southbound right turn movement and the OR43 northbound left turn movement to the reconstructed I-205 northbound entrance loop ramp will operate under free flow condition after exiting the roundabout as the entrance ramp will not have a ramp meter that would otherwise require vehicles to stop, interrupting the roundabout operations. The OR43 northbound through vehicles exiting the roundabout would not be interrupted by the downstream signal at the I-205 southbound ramp terminal as the vehicle queue in the northbound approach lanes to the intersection is determined to be 228 feet and 166 feet in the 2045 AM and PM peak hours, respectively. The available storage for the two northbound through lanes is approximately 610 feet for each of the two northbound through lanes at I-205 southbound ramp terminal. A summary of the Vissim analysis results is provided in the Appendix E.

In regards to the OR43 southbound vehicles exiting the roundabout, the Project Team has identified an existing operational deficiency associated with the downstream signalized intersection at the south end of the Oregon City Arch Bridge, which is approximately $1 / 4$ mile south of the OR43/l-205 northbound ramp terminal and 1,200 feet south of the OR43/Willamette Falls Drive intersection. This condition results in recurring backup of southbound traffic that extends across the Oregon City Arch Bridge and occasionally through the OR43/Willamette Falls Drive and I-205 northbound ramp terminal intersection. Based on site observations, this condition is experienced in the PM peak hour. While operational improvements at the Arch Bridge signal are outside the scope of the Project, a preliminary evaluation of the corridor operations was performed to assess the potential impact of recurring queuing into the roundabout. This analysis was conducted using Vissim by creating a "simulated" southbound queue that extended through the roundabout intersection. Because of the low volume of the l-205 northbound exit-ramp and the fact that the competing left turn movements from OR43 northbound take priority over the OR43 southbound entering traffic, the analysis does not show any significant impact by the Oregon City Arch Bridge signal to the roundabout operations.

One of the main reasons as to why the Oregon City Arch Bridge signal causes a long queue in the southbound direction on OR43 is due to the high right-turning traffic volume ( 424 vehicles) from Willamette Falls Drive destined to Oregon City in the PM peak hour. To further understand the make-up of the Willamette Falls Drive and Oregon City Arch Bridge traffic, origin-destination (OD) data was obtained from StreetLight Data to determine the origin of these trips. StreetLight OD data revealed that during the PM peak hour, approximately 200 ( 28.5 percent) of the 701 (277 vph left turn and 424 vph right turn movements) total eastbound approach vehicles accessing the Willamette Falls Drive intersection with OR43 originated from: (i) I-5 north and south, and (ii) Stafford Road north and south of I-205. What this indicates is that (i) some of the I-205 northbound traffic coming from I-5 would rather exit off at the Stafford Road Interchange to access OR43 via Willamette Falls Drive than continue traveling on I-205 mainline and exit off at the OR43 Interchange, and (ii) traffic originated from Stafford Road north and south of I-205 would rather travel on Willamette Falls Drive to access OR43 than enter northbound I-205 at the Stafford Road Interchange and exit off at the OR43 Interchange. This traffic diversion phenomenon, illustrated in Figure 6, is indicative of traffic trying to avoid the severe congestion on I-205 northbound in the 2-lane section between the Stafford Road and OR43 Interchanges in the PM peak period and using Willamette Falls Drive as a by-pass route. Additionally, the StreetLight OD data presented in Figure 7 showed that 71 percent of the Willamette Falls Drive traffic was destined to areas of

Oregon City between OR43 and OR99E and 10\% of the total PM peak period traffic using the Arch Bridge was continuing on to destinations north of the OR99E Interchange area. These conditions were also validated by multiple field observations during congested periods and input received during public outreach events.

Figure 6. Traffic by-passing I-205 NB


Source: StreetLight Data - StreetLight collects massive volume of geospatial information created by mobile phones, GPS devices, connected cars and commercial trucks, fitness trackers, and more.

Figure 7. StreetLight Data for Willamette Falls Drive and OR43


Source: StreetLight Data - StreetLight collects massive volume of geospatial information created by mobile phones, GPS devices, connected cars and commercial trucks, fitness trackers, and more.

To illustrate the congestion on I-205 northbound between the Stafford Road and OR99E Interchanges, traffic speed data for I-205 was obtained from HERE data. The speed data was then aggregated and averaged for weekdays (excluding holidays) in the entire year of 2017. Figure 8 shows the 2017 average weekday speed data for l-205 northbound. As illustrated in the speed contour map, the northbound section between the Stafford Road and OR99E Interchanges experiences 3 hours of congestion in the afternoon between 3:30 PM and 6:30 PM.

Figure 8. I-205 Northbound 2017 Average Weekday Speed Contour


Source: HERE Data - HERE collects billions of GPS data points every day and leverages over 100 different incident sources to provide a robust foundation for traffic services. Information is collected from a variety of devices across the globe including vehicle sensor data, smartphones, PNDs (Provider Network Data System), road sensors, and connected cars.

With the l-205 corridor widening between Stafford Road and OR213, the majority of traffic currently using Willamette Falls Drive to avoid congestion on I-205 is expected to stay on I-205 and exit off the freeway at the OR99E Interchange to access Oregon City instead of exiting off at the Stafford Interchange to head to Willamette Falls Drive. As a result, there would be reduced traffic demand on OR43 southbound across the Oregon City Arch Bridge, alleviating the existing recurring backup of southbound traffic on OR43.

### 4.2 Safety Performance Comparison

The proposed roundabout control would have fewer conflict points and reduce crash severity due to slower vehicle speeds and differing potential collision types as compared to the signal control. The Federal Highway Administration Crash Modification Factor (CMF) clearinghouse and Highway Safety Manual provide a CMF 0.520 for converting a signal controlled intersection to a single lane or multi-lane roundabout (Clearinghouse CMF ID $225^{1}$ ). It can be estimated that, in the future, the intersection of OR43 and I-205 northbound ramp terminal operating under roundabout control would have 48 percent fewer crashes per year. The 48 percent reduction in crashes would apply to 10 out of the 11 crashes cited in Section 2.2.2 that occurred in the fiveyear 2012-2016 period.

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## 5 Preferred Intersection Control Alternative

The roundabout alternative would improve intersection safety in terms of both crash frequency and severity and reduce overall queuing on OR43. It would not create driveway conflicts with queued vehicles on OR43 and degrade existing operations of an impacted facility as the Signal Control Alternative would. The roundabout is consistent with the City of West Linn's long term vision for OR43 as its Transportation System Plan calls for an additional roundabout at the OR43/Willamette Falls Drive intersection. The current design for the roundabout at the I-205 northbound ramp terminal does not preclude any future improvements associated with the City of West Linn Transportation System Plan or the West Linn Water Front Development Plan that is currently in development.

A scale drawing showing the conceptual design of the proposed roundabout with horizontal and vertical geometry and layout elements is provided in Appendix F.

## 6 Accommodation for other modes of Transportation

### 6.1 Freight Mobility

The Project Team has had a number of conversations and discussions with the Freight Mobility Advisory Committee early on in the project development phase. The roundabout concept has been vetted through the Committee and has received acceptance to move forward. The current layout is designed for a WB-67 Interstate truck circulating through the roundabout from all approaches. The Oregon City Arch Bridge has weight and size restrictions and Willamette Falls Drive is not a designated truck route. The Motor Carrier Freight Mobility Map identifies OR43 as a Black and Yellow route, indicating that the route is highly restricted to truck and oversize traffic.

### 6.2 Bicyclist and Pedestrian

There will be significant bike and pedestrian improvements along OR43 within the project limits. ADA ramps will be upgraded at the OR43/I-205 southbound ramp terminal and the OR43/Willamette Falls Drive intersection. A shared-use path will be constructed along the east side of OR43 from the I-205 southbound ramp terminal to Willamette Falls Drive. Way finding signs will be installed to help guide bicyclists and pedestrians to navigate through the corridor. A rectangular rapid flashing beacon is proposed on OR43 at Willamette Falls Drive to enhance pedestrian crossing safety. Bicycles will also be permitted to use the highway shoulders along OR43 and may access through the roundabout.

Due to the dual-lane approaches, crosswalks will not be provided within proposed roundabout. One of the design considerations of the roundabout alternative, however, is that pedestrians at each leg would face the prospect of crossing multiple lanes of traffic to travel across the roundabout. The heavy vehicular movements, particularly from southbound OR43 in addition to the multilane approach and exit conditions involving northbound OR43, would result in conflicts with pedestrian movements. Studies have shown that conflicts between multilane roundabout approaches and crosswalks create a hazard for sight impaired pedestrians as they cannot
effectively determine gaps in traffic. Legally closing the unmarked crosswalks at the roundabout and providing pedestrians a new route will significantly improve safety in the area. Pedestrians within the interchange area will instead use the proposed shared-use path to access safer striped crosswalks at either a signalized intersection or proposed enhanced crossing with a new rectangular rapid flashing beacon. These alternate crossings are within close proximity to the proposed crossing closure and will result in little, if any, out-of-direction travel incurred by closing the crossings. A separate approval request for the crosswalk closure at the proposed roundabout will be submitted to the State Traffic Engineer through the Region Traffic Engineer.

## 7 Conclusion

The roundabout alternative effectively accommodates the safety, capacity and multimodal needs of the proposed intersection. Compared to the signal control alternative, a roundabout satisfied the following key criteria:

- Provide sufficient capacity and better operational performance for the forecasted movements onto the freeway in both AM and PM peak hours
- Minimize project footprint
- Will not worsen operational conditions to adjacent local streets as compared to the existing conditions
- Providing better safety performance (reductions in crash severity, injuries and in all crashes) due to slower vehicle speeds and fewer conflict points.

Other benefits include reduced pollution, lower traffic noise and fuel use through fewer stops and hard accelerations as well as significant life-cycle cost savings due to no signal equipment installation, power or maintenance costs.

## Appendix A Crash Data (2012-2016) for OR43 between McKillican Street and Willamette Falls Drive

Highway 003 MAINLINE, MP 10.88 to 11.36 01/01/2012 to $12 / 31 / 2016$, Both Add and Non-Add mileage

| H | R |  | C |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | D | C | $\bigcirc$ |  |  |  |  |  |  |  |  |  | PEOPLE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| W | W | $\bigcirc$ | N |  |  |  |  |  |  |  |  |  |  | INJ | URY |  | VEH | CLE |  | VEH | cle | 2 |  | VEH | CLE | 3 |  |
| Y | Y | M | N | MLG | MILE | CRASH |  |  |  | RD | OFF | COLL |  |  |  |  |  |  |  |  |  |  |  |  |  |  | ADD |
| \# | \# | P | \# | TYP | POINT | DATE | TIME | LIGHT | SURF | CH | RD | TYPE | K | A | B | C | TYPE | FR | то | TYPE | FR |  | то | TYPE | FR | то | VEH |
| 003 | 1 | MN |  | 0 | 10.88 | 07/10/2012 | 12P | DAY | DRY | 3 | N | REAR | 0 | 0 | 0 | 0 | 01 | NW | SE | 01 | NW |  | SE |  |  |  |  |
| 003 | 1 | MN |  | 0 | 10.90 | 08/29/2015 | 4 P | DAY | WET | 3 | N | REAR | 0 | 0 | 0 | 6 | 01 | SE | NW | 01 | SE |  | NW |  |  |  |  |
| 003 | 1 | MN |  | 0 | 10.91 | 08/07/2014 | 2 P | DAY | DRY | 3 | N | REAR | 0 | 0 | 0 | 1 | 01 | NW | SE | 01 | NW |  | SE |  |  |  |  |
| 003 | 1 | MN |  | 0 | 10.92 | 06/12/2013 | 3P | DAY | DRY | 1 | N | ANGL | 0 | 0 | 0 | 0 | 01 | SW | NE | 01 | NW |  | SE |  |  |  |  |
| 003 | 1 | MN |  | 0 | 10.92 | 09/13/2013 | 5 P | DAY | DRY | 1 | N | TURN | 0 | 0 | 0 | 0 | 01 | NE | SE | 01 | NW |  | NE |  |  |  |  |
| 003 | 1 | MN |  | 0 | 10.92 | 12/09/2013 | 2 P | DAY | WET | 1 | N | REAR | 0 | 0 | 0 | 0 | 01 | SE | NW | 01 | SE |  | NW |  |  |  |  |
| 003 | 1 | MN |  | 0 | 10.92 | 03/20/2015 | 12P | DAY | DRY | 1 | N | REAR | 0 | 0 | 0 | 1 | 01 | SE | NW | 01 | SE |  | NW |  |  |  |  |
| 003 | 1 | MN |  | 0 | 10.92 | 03/21/2015 | 2 P | DAY | DRY | 1 | N | REAR | 0 | 0 | 0 | 1 | 01 | SE | NW | 01 | SE |  | NW |  |  |  |  |
| 003 | 1 | MN |  | 0 | 10.92 | 04/04/2015 | 3P | DAY | DRY | 1 | N | TURN | 0 | 0 | 1 | 0 | 01 | SE | SW |  |  |  |  |  |  |  |  |
| 003 | 1 | MN |  | 0 | 10.92 | 02/07/2016 | 2 P | DAY | DRY | 1 | N | TURN | 0 | 0 | 0 | 0 | 01 | NE | SE | 01 | NW |  | NE |  |  |  |  |
| 003 | 1 | MN |  | 0 | 10.92 | 02/16/2016 | 4A | DLIT | WET | 1 | N | ANGL | 0 | 0 | 0 | 1 | 01 | SW | NE | 01 | NW |  | SE |  |  |  |  |
| 003 | 1 | MN |  | 0 | 10.92 | 08/14/2016 | 1 P | DAY | DRY | 1 | N | TURN | 0 | 0 | 0 | 1 | 01 | NW | SE | 01 | SE |  | SW |  |  |  |  |
| 003 | 1 | MN |  | 0 | 10.92 | 09/23/2016 | 3P | DAY | DRY | 1 | N | REAR | 0 | 0 | 0 | 0 | 01 | SE | NW | 01 | SE |  | NW |  |  |  |  |
| 003 | 1 | MN |  | 0 | 10.92 | 09/25/2016 | 12P | DAY | DRY | 1 | N | TURN | 0 | 0 | 0 | 1 | 01 | SE | NW | 01 | NW |  | NE |  |  |  |  |
| 003 | 1 | MN |  | 0 | 10.94 | 04/04/2012 | 12P | DAY | WET | 3 | N | SS-M | 0 | 0 | 0 | 2 | 01 | SE | NW | 01 | NW |  | SE | 01 | NW | SE |  |
| 003 | 1 | MN |  | 0 | 10.94 | 08/27/2015 | 8A | DAY | DRY | 3 | N | SS-O | 0 | 0 | 0 | 0 | 01 | S | N | 01 | S |  | N |  |  |  |  |
| 003 | 1 | MN |  | 0 | 10.96 | 06/05/2012 | 3 P | DAY | WET | 3 | N | REAR | 0 | 0 | 0 | 4 | 01 | S | N | 01 | S |  | N | 01 | S | N |  |
| 003 | 1 | MN |  | 0 | 10.96 | 09/14/2015 | 2P | DAY | DRY | 3 | N | SS-O | 0 | 0 | 0 | 0 | 05 | SE | NW | 01 | SE |  | NW |  |  |  |  |
| 003 | 1 | MN |  | 0 | 10.97 | 09/16/2012 | 3 P | DAY | DRY | 3 | N | REAR | 0 | 0 | 0 | 0 | 01 | NW | SE | 01 | NW |  | SE |  |  |  |  |
| 003 | 1 | MN |  | 0 | 10.99 | 01/20/2012 | 4 P | DUSK | WET | 1 | N | TURN | 0 | 0 | 0 | 0 | 01 | SE | NW | 01 | NE |  | SE |  |  |  |  |

Highway 003 MAINLINE, MP 10.88 to 11.36 01/01/2012 to $12 / 31 / 2016$, Both Add and Non-Add mileage

| H | R |  | C |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | D | C | $\bigcirc$ |  |  |  |  |  |  |  |  |  |  | PEOPLE |  |  |  |  |  |  |  |  |  |  |  |  |
| W | W | $\bigcirc$ | N |  |  |  |  |  |  |  |  |  |  | INJ | URY |  | VEH | CLE | 1 | VEH | ICLE | 2 | VEH | CLE |  |  |
| Y | Y | M | N | MLG | MILE | CRASH |  |  |  | RD | OFF | COLL |  |  |  |  |  |  |  |  |  |  |  |  |  | ADD |
| \# | \# | P | \# | TYP | POINT | DATE | TIME | LIGHT | SURF | CH | RD | TYPE | K | A | B | C | TYPE | FR | TO | TYPE | FR | TO | TYPE | FR | TO | VEH |
| 303 | 1 | MN |  | 0 | 10.99 | 01/09/2014 | 3 P | DAY | WET | 1 | N | TURN | 0 | 0 | 0 | 1 | 01 | E | SE | 01 | SE | NW |  |  |  |  |
| 003 | 1 | MN |  | 0 | 10.99 | 10/21/2014 | 7A | DLIT | DRY | 1 | N | TURN | 0 | 0 | 0 | 0 | 01 | NE | SE | 01 | NW | SE |  |  |  |  |
| 003 | 1 | MN |  | 0 | 10.99 | 12/04/2014 | 3P | DAY | WET | 1 | N | TURN | 0 | 0 | 0 | 0 | 01 | SE | NW | 01 | NE | SE |  |  |  |  |
| 003 | 1 | MN |  | 0 | 10.99 | 07/06/2015 | 4 P | DAY | DRY | 1 | N | TURN | 0 | 0 | 0 | 0 | 01 | NE | NW | 01 | SE | NW |  |  |  |  |
| 003 | 1 | MN |  | 0 | 10.99 | 09/21/2016 | 6 P | DAY | DRY | 1 | N | REAR | 0 | 0 | 0 | 0 | 01 | NW | SE | 01 | NW | SE |  |  |  |  |
| 003 | 1 | MN |  | 0 | 10.99 | 10/03/2016 | 10A | DAY | DRY | 1 | N | TURN | 0 | 0 | 0 | 0 | 01 | NE | SE | 01 | NW | SE |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.01 | 11/15/2012 | 3P | DAY | DRY | 3 | N | REAR | 0 | 0 | 0 | 1 | 01 | N | S | 01 | N | S |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.03 | 09/02/2015 | 2 P | DAY | DRY | 3 | N | REAR | 0 | 0 | 0 | 1 | 01 | SE | NW | 01 | SE | NW |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.03 | 08/03/2016 | 12P | DAY | DRY | 2 | N | TURN | 0 | 0 | 0 | 0 | 01 | SW | NW | 01 | NW | NE |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.04 | 03/31/2012 | 12P | DAY | DRY | 3 | N | REAR | 0 | 0 | 0 | 1 | 01 | N | S | 01 | N | S | 01 | N | S |  |
| 003 | 1 | MN |  | 0 | 11.04 | 03/11/2013 | 4 P | DAY | DRY | 2 | N | TURN | 0 | 0 | 0 | 0 | 01 | NW | SE | 01 | SW | NW |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.04 | 01/10/2015 | 1 P | DAY | WET | 2 | N | TURN | 0 | 0 | 0 | 0 | 01 | NW | SE | 01 | SW | NW |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.05 | 02/21/2012 | 4 P | DAY | WET | 2 | N | TURN | 0 | 0 | 0 | 0 | 01 | NE | SE | 01 | NW | SE |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.05 | 10/03/2013 | 11A | DAY | DRY | 3 | N | REAR | 0 | 0 | 0 | 0 | 01 | SE | NW | 01 | SE | NW |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.05 | 01/06/2016 | 1 P | DAY | DRY | 2 | N | TURN | 0 | 0 | 1 | 1 | 01 | SE | NW | 01 | NE | SE |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.05 | 03/24/2016 | 8A | DAWN | DRY | 3 | N | REAR | 0 | 0 | 0 | 0 | 01 | NW | SE | 01 | NW | SE |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.05 | 04/14/2016 | 9A | DAY | WET | 2 | N | TURN | 0 | 0 | 1 | 0 | 01 | SE | NW | 01 | NE | SE |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.06 | 04/17/2012 | 3P | DAY | DRY | 1 | N | TURN | 0 | 0 | 0 | 2 | 01 | SW | NW | 01 | NW | SE |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.06 | 05/07/2013 | 3 P | DAY | DRY | 1 | N | TURN | 0 | 0 | 0 | 0 | 01 | NW | SE | 01 | SW | NW |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.06 | 08/07/2015 | 11A | DAY | DRY | 1 | N | TURN | 0 | 0 | 0 | 0 | 01 | NW | SE | 01 | SW | NW |  |  |  |  |

Highway 003 MAINLINE, MP 10.88 to 11.36 01/01/2012 to $12 / 31 / 2016$, Both Add and Non-Add mileage

| H | R |  | C |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | D | C | $\bigcirc$ |  |  |  |  |  |  |  |  |  | PEOPLE |  |  |  |  |  |  |  |  |  |  |  |  |  |
| w | W | $\bigcirc$ | N |  |  |  |  |  |  |  |  |  |  | INJ | URY |  | VEH | ICLE | 1 | VEH | ICLE | 2 | VEH | CLE |  |  |
| Y | Y | M | N | MLG | MILE | CRASH |  |  |  | RD | OFF | COLL |  |  |  |  |  |  |  |  |  |  |  |  |  | ADD |
| \# | \# | P | \# | TYP | POINT | DATE | TIME | LIGHT | SURF | CH | RD | TYPE | K | A | B | C | TYPE | FR | то | TYPE | FR | то | TYPE | FR | то | VEH |
| 303 | 1 | MN |  | 0 | 11.07 | 01/31/2013 | 8A | DAY | WET | 2 | N | TURN | 0 | 0 | 0 | 1 | 01 | SW | NW | 01 | NW | SE |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.10 | 01/26/2012 | 5 P | UNK | UNK | 3 | N | REAR | 0 | 0 | 0 | 0 | 01 | NW | SE | 01 | NW | SE |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.11 | 05/05/2013 | 12P | DAY | DRY | 3 | N | SS-O | 0 | 0 | 0 | 0 | 01 | SE | NW | 99 | SE | NW |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.11 | 07/17/2013 | 9A | DAY | DRY | 3 | N | REAR | 0 | 0 | 0 | 0 | 99 | NW | SE | 01 | NW | SE | 01 | NW | SE |  |
| 003 | 1 | MN |  | 0 | 11.11 | 07/16/2014 | 5P | DAY | DRY | 3 | N | REAR | 0 | 0 | 1 | 0 | 01 | NW | SE | 01 | NW | SE |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.11 | 05/18/2015 | 2 P | DAY | DRY | 3 | N | REAR | 0 | 0 | 0 | 1 | 01 | NW | SE | 01 | NW | SE |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.13 | 11/05/2012 | 9A | DAY | WET | 1 | N | TURN | 0 | 1 | 0 | 0 | 01 | SE | NW | 01 | NE | SE |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.13 | 12/23/2013 | 9 P | DLIT | WET | 1 | N | ANGL | 0 | 0 | 0 | 0 | 01 | NE | SW | 01 | NW | SE |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.13 | 12/25/2014 | 6 P | DLIT | WET | 1 | N | REAR | 0 | 0 | 0 | 2 | 01 | NW | SE | 01 | NW | SE |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.13 | 01/09/2015 | 6A | DLIT | DRY | 1 | N | TURN | 0 | 0 | 0 | 1 | 01 | NW | SE | 01 | SE | SW |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.13 | 04/25/2015 | 2 P | DAY | DRY | 1 | N | SS-O | 0 | 0 | 1 | 0 | 01 | N | S |  |  |  |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.13 | 07/12/2015 | 3 P | DAY | DRY | 1 | N | TURN | 0 | 0 | 0 | 1 | 01 | SE | NW | 01 | E | SE |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.13 | 09/16/2015 | 6A | DAWN | WET | 1 | N | TURN | 0 | 0 | 0 | 1 | 01 | NW | SE | 01 | SE | SW |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.13 | 12/02/2015 | 5 P | DLIT | WET | 1 | N | TURN | 0 | 0 | 0 | 0 | 01 | SE | NW | 01 | NE | SE |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.13 | 01/21/2016 | 5P | DUSK | DRY | 1 | N | REAR | 0 | 0 | 0 | 1 | 01 | NW | SE | 01 | NW | SE |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.14 | 06/06/2012 | 10A | DAY | DRY | 1 | Y | FIX | 0 | 0 | 1 | 0 | 09 | SE | SW |  |  |  |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.14 | 03/25/2014 | 5 P | DAY | WET | 1 | N | ANGL | 0 | 0 | 0 | 0 | 01 | E | W | 01 | N | S |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.16 | 08/25/2013 | 9 P | DARK | UNK | 3 | Y | FIX | 0 | 0 | 0 | 1 | 01 | N | S |  |  |  |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.27 | 04/08/2014 | 10A | DAY | DRY | 3 | N | SS-O | 0 | 0 | 0 | 1 | 01 | SW | NE | 01 | SW | NE |  |  |  |  |
| 003 | 1 | MN |  | 0 | 11.29 | 02/11/2014 | 10A | DAY | WET | 1 | N | TURN | 0 | 0 | 0 | 0 | 01 | NW | NE | 01 | NE | SW |  |  |  |  |

## Highway 003 MAINLINE, MP 10.88 to 11.36 01/01/2012 to $12 / 31 / 2016$, Both Add and Non-Add mileage



## Appendix B Crash Data (2012-2016) for OR43 at I205 NB Exit-Ramp

## OREGON DEPARTMENT OF TRANSPORTATION - TRANSPORTATION DEVELOPMENT DVIISIO

TRANSPORTATION DATA SECTION - CRASH ANALYSIS AND REPORTING UNIT
Highway 064 CONNECTIONS, MP 8.79 to 8 8.79, Botht Add and Non-Add mileage, 010112012 to $12 / 3112016$
Tomerash DE-CODER V5.1.3 PRC REPORT PRINTABLE EQUIVALENT*M


## \#\#CRASH DE-CODER V5.1.3 PRC REPORT PRINTABLE EQUIVALENT****



## Appendix C Synchro/SimTraffic Analysis Worksheets



|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


|  | $\Rightarrow$ |  | 4 | 4 | $\downarrow$ | $\downarrow$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |  |
| Lane Configurations | * | 「 |  | 44 | 个4 |  |  |
| Traffic Volume (vph) | 64 | 187 | 0 | 897 | 339 | 0 |  |
| Future Volume (vph) | 64 | 187 | 0 | 897 | 339 | 0 |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |  |
| Total Lost time (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  |  |
| Lane Util. Factor | 1.00 | 1.00 |  | 0.95 | 0.95 |  |  |
| Frpb, ped/bikes | 1.00 | 0.98 |  | 1.00 | 1.00 |  |  |
| Flpb, ped/bikes | 1.00 | 1.00 |  | 1.00 | 1.00 |  |  |
| Frt | 1.00 | 0.85 |  | 1.00 | 1.00 |  |  |
| Flt Protected | 0.95 | 1.00 |  | 1.00 | 1.00 |  |  |
| Satd. Flow (prot) | 1719 | 1512 |  | 3539 | 3438 |  |  |
| Flt Permitted | 0.95 | 1.00 |  | 1.00 | 1.00 |  |  |
| Satd. Flow (perm) | 1719 | 1512 |  | 3539 | 3438 |  |  |
| Peak-hour factor, PHF | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |  |
| Adj. Flow (vph) | 65 | 191 | 0 | 915 | 346 | 0 |  |
| RTOR Reduction (vph) | 0 | 164 | 0 | 0 | 0 | 0 |  |
| Lane Group Flow (vph) | 65 | 27 | 0 | 915 | 346 | 0 |  |
| Confl. Peds. (\#/hr) |  |  | 1 |  |  | 1 |  |
| Confl. Bikes (\#/hr) |  | 3 |  |  |  | 3 |  |
| Heavy Vehicles (\%) | 5\% | 5\% | 2\% | 2\% | 5\% | 5\% |  |
| Turn Type | Prot | Perm |  | NA | NA |  |  |
| Protected Phases | 8 |  |  | 6 | 2 |  |  |
| Permitted Phases |  | 8 |  |  |  |  |  |
| Actuated Green, G (s) | 5.5 | 5.5 |  | 23.4 | 23.4 |  |  |
| Effective Green, g (s) | 5.5 | 5.5 |  | 23.4 | 23.4 |  |  |
| Actuated g/C Ratio | 0.14 | 0.14 |  | 0.60 | 0.60 |  |  |
| Clearance Time (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  |  |
| Vehicle Extension (s) | 2.3 | 2.3 |  | 4.5 | 4.2 |  |  |
| Lane Grp Cap (vph) | 243 | 213 |  | 2128 | 2068 |  |  |
| v/s Ratio Prot | c0.04 |  |  | c0.26 | 0.10 |  |  |
| v/s Ratio Perm |  | 0.02 |  |  |  |  |  |
| v/c Ratio | 0.27 | 0.13 |  | 0.43 | 0.17 |  |  |
| Uniform Delay, d1 | 14.9 | 14.6 |  | 4.2 | 3.4 |  |  |
| Progression Factor | 1.00 | 1.00 |  | 1.00 | 1.00 |  |  |
| Incremental Delay, d2 | 0.3 | 0.2 |  | 0.2 | 0.1 |  |  |
| Delay (s) | 15.2 | 14.8 |  | 4.4 | 3.5 |  |  |
| Level of Service | B | B |  | A | A |  |  |
| Approach Delay (s) | 14.9 |  |  | 4.4 | 3.5 |  |  |
| Approach LOS | B |  |  | A | A |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 6.0 |  | HCM 2000 | evel of Service | A |
| HCM 2000 Volume to Capacity ratio |  |  | 0.40 |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 38.9 |  | Sum of lost | me (s) | 10.0 |
| Intersection Capacity Utilization |  |  | 38.1\% |  | CU Level of | Service | A |
| Analysis Period (min) |  |  | 15 |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |



Intersection: 3: OR43 \& McKillican

| Movement | EB | EB | WB | WB | SE | SE | NW | NW | B77 | B77 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | TR | L | TR | L | TR | T |  |
| Maximum Queue (ft) | 84 | 147 | 108 | 90 | 31 | 327 | 209 | 568 | 144 | 71 |
| Average Queue (ft) | 27 | 64 | 48 | 23 | 4 | 146 | 58 | 308 | 31 | 18 |
| 95th Queue (ft) | 64 | 117 | 91 | 67 | 20 | 268 | 170 | 580 | 183 | 147 |
| Link Distance (ft) |  | 206 |  | 166 |  | 445 |  | 534 | 322 | 322 |
| Upstream Blk Time (\%) |  | 0 | 0 | 0 |  |  |  | 5 | 2 | 1 |
| Queuing Penalty (veh) |  | 0 | 0 | 0 |  |  |  | 44 | 9 | 3 |
| Storage Bay Dist (ft) | 150 |  | 50 |  | 180 |  | 110 |  |  |  |
| Storage Blk Time (\%) |  | 0 | 17 | 1 |  | 4 | 0 | 23 |  |  |
| Queuing Penalty (veh) |  | 0 | 4 | 1 |  | 0 | 0 | 16 |  |  |

Intersection: 4: I-205 SB On Ramp \& I-205 SB Off Ramp \& OR43

| Movement | WB | WB | NB | NB | NB | SB | SB | B77 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | $<$ | LR | L | T | T | T | TR | T |
| Maximum Queue (ft) | 184 | 279 | 218 | 203 | 124 | 299 | 331 | 23 |
| Average Queue (ft) | 91 | 128 | 101 | 76 | 12 | 100 | 163 | 1 |
| 95th Queue (ft) | 159 | 241 | 180 | 161 | 70 | 226 | 283 | 21 |
| Link Distance (ft) |  | 1110 |  | 288 | 288 | 322 | 322 | 534 |
| Upstream Blk Time (\%) |  |  | 0 | 0 | 0 | 0 | 1 |  |
| Queuing Penalty (veh) |  |  | 0 | 1 | 0 | 0 | 2 |  |
| Storage Bay Dist (ft) | 500 |  | 180 |  |  |  |  |  |
| Storage BIk Time (\%) |  |  | 2 | 1 |  |  |  |  |
| Queuing Penalty (veh) |  |  | 4 | 2 |  |  |  |  |

Intersection: 5: I-205 NB Off Ramp \& OR43

| Movement | EB | EB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | R | T | T | T | T |
| Maximum Queue (ft) | 84 | 113 | 152 | 123 | 123 | 86 |
| Average Queue (ft) | 35 | 52 | 76 | 50 | 38 | 26 |
| 95th Queue (ft) | 71 | 87 | 131 | 102 | 92 | 69 |
| Link Distance (ft) |  | 849 | 205 | 205 | 185 | 185 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |
| Storage Bay Dist (ft) | 225 |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |

Intersection: 6: OR43 \& Willamette Falls Dr

| Movement | EB | EB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | $R$ | L | T | T | R |
| Maximum Queue (ft) | 149 | 137 | 188 | 69 | 10 | 75 |
| Average Queue (ft) | 134 | 62 | 72 | 4 | 0 | 6 |
| 95th Queue (ft) | 143 | 128 | 141 | 78 | 5 | 50 |
| Link Distance (ft) | 128 | 128 |  | 672 | 205 | 205 |
| Upstream Blk Time (\%) | 84 | 1 |  | 0 |  | 0 |
| Queuing Penalty (veh) | 153 | 1 |  | 0 |  | 0 |
| Storage Bay Dist (ft) |  |  | 200 |  |  |  |
| Storage Blk Time (\%) |  |  | 0 |  |  |  |
| Queuing Penalty (veh) |  |  | 3 |  |  |  |


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Intersection: 29: OR43
Movement
Directions Served
Maximum Queue (ft)
Average Queue (ft)
95th Queue (ft)
Link Distance (ft)
Upstream Blk Time (\%)
Queuing Penalty (veh)
Storage Bay Dist (ft)
Storage Blk Time (\%)
Queuing Penalty (veh)

Intersection: 61:

| Movement | NB | NB | SB |
| :--- | ---: | ---: | ---: |
| Directions Served | T | T | TR |
| Maximum Queue (ft) | 28 | 28 | 16 |
| Average Queue (ft) | 2 | 1 | 1 |
| 95th Queue (ft) | 26 | 23 | 9 |
| Link Distance (ft) | 142 | 142 | 288 |
| Upstream Blk Time (\%) | 0 | 0 |  |
| Queuing Penalty (veh) | 0 | 0 |  |
| Storage Bay Dist (ft) |  |  |  |
| Storage Blk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  |  |

## Network Summary

Network wide Queuing Penalty: 421




|  | $\Rightarrow$ |  | 4 | $\uparrow$ | $\dagger$ | $\downarrow$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |  |
| Lane Configurations | * | $\stackrel{\square}{7}$ | * | $\uparrow$ | 4 | 「 |  |
| Traffic Volume (veh/h) | 277 | 424 | 215 | 522 | 456 | 236 |  |
| Future Volume (Veh/h) | 277 | 424 | 215 | 522 | 456 | 236 |  |
| Sign Control | Stop |  |  | Free | Free |  |  |
| Grade | 0\% |  |  | 0\% | 0\% |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |  |
| Hourly flow rate (vph) | 301 | 461 | 234 | 567 | 496 | 257 |  |
| Pedestrians |  |  |  | 3 | 3 |  |  |
| Lane Width (ft) |  |  |  | 12.0 | 12.0 |  |  |
| Walking Speed (ft/s) |  |  |  | 3.5 | 3.5 |  |  |
| Percent Blockage |  |  |  | 0 | 0 |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |
| Median type |  |  |  | None | TWLTL |  |  |
| Median storage veh) |  |  |  |  | 2 |  |  |
| Upstream signal (ft) |  |  |  |  | 275 |  |  |
| pX, platoon unblocked | 0.91 | 0.91 | 0.91 |  |  |  |  |
| vC , conflicting volume | 1534 | 499 | 753 |  |  |  |  |
| vC 1 , stage 1 conf vol | 496 |  |  |  |  |  |  |
| vC 2 , stage 2 conf vol | 1038 |  |  |  |  |  |  |
| vCu , unblocked vol | 1537 | 397 | 677 |  |  |  |  |
| tC, single (s) | 6.4 | 6.2 | 4.1 |  |  |  |  |
| tC, 2 stage (s) | 5.4 |  |  |  |  |  |  |
| tF (s) | 3.5 | 3.3 | 2.2 |  |  |  |  |
| p0 queue free \% | 0 | 22 | 72 |  |  |  |  |
| cM capacity (veh/h) | 228 | 590 | 830 |  |  |  |  |
| Direction, Lane \# | EB 1 | EB 2 | NB 1 | NB 2 | SB 1 | SB 2 |  |
| Volume Total | 301 | 461 | 234 | 567 | 496 | 257 |  |
| Volume Left | 301 | 0 | 234 | 0 | 0 | 0 |  |
| Volume Right | 0 | 461 | 0 | 0 | 0 | 257 |  |
| cSH | 228 | 590 | 830 | 1700 | 1700 | 1700 |  |
| Volume to Capacity | 1.32 | 0.78 | 0.28 | 0.33 | 0.29 | 0.15 |  |
| Queue Length 95th (ft) | 403 | 184 | 29 | 0 | 0 | 0 |  |
| Control Delay (s) | 212.9 | 29.4 | 11.0 | 0.0 | 0.0 | 0.0 |  |
| Lane LOS | F | D | B |  |  |  |  |
| Approach Delay (s) 101 | 101.9 |  | 3.2 |  | 0.0 |  |  |
| Approach LOS F |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Average Delay |  |  | 34.6 |  |  |  |  |
| Intersection Capacity Utilization |  |  | 61.3\% |  | CU Level | Service | B |
| Analysis Period (min) |  |  | 15 |  |  |  |  |

Intersection: 3: OR43 \& McKillican

| Movement | EB | EB | WB | WB | SE | SE | NW | NW | B77 | B77 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | TR | L | TR | L | TR | T |  |
| Maximum Queue (ft) | 200 | 226 | 166 | 185 | 42 | 499 | 210 | 530 | 67 | 35 |
| Average Queue (ft) | 98 | 142 | 158 | 174 | 2 | 389 | 64 | 265 | 5 | 1 |
| 95th Queue (ft) | 187 | 232 | 187 | 227 | 29 | 575 | 172 | 453 | 60 | 35 |
| Link Distance (ft) |  | 206 |  | 166 |  | 445 |  | 534 | 322 | 322 |
| Upstream Blk Time (\%) | 0 | 5 | 45 | 73 |  | 22 |  | 1 | 0 | 0 |
| Queuing Penalty (veh) | 0 | 0 | 0 | 0 |  | 0 |  | 9 | 0 | 0 |
| Storage Bay Dist (ft) | 150 |  | 100 |  | 180 |  | 110 |  |  |  |
| Storage Blk Time (\%) | 8 | 10 | 92 | 2 |  | 36 | 0 | 24 |  |  |
| Queuing Penalty (veh) | 22 | 10 | 78 | 4 |  | 1 | 3 | 20 |  |  |

Intersection: 4: I-205 SB On Ramp \& I-205 SB Off Ramp \& OR43

| Movement | WB | WB | NB | NB | NB | SB | SB | B77 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | $<$ | LR | L | T | T | T | TR | T |
| Maximum Queue (ft) | 254 | 357 | 100 | 103 | 42 | 362 | 396 | 253 |
| Average Queue (ft) | 124 | 160 | 43 | 42 | 3 | 172 | 240 | 19 |
| 95th Queue (ft) | 207 | 295 | 79 | 89 | 23 | 329 | 371 | 145 |
| Link Distance (ft) |  | 1110 |  | 288 | 288 | 322 | 322 | 534 |
| Upstream Blk Time (\%) |  |  |  |  |  | 0 | 2 | 0 |
| Queuing Penalty (veh) |  |  |  |  |  | 3 | 15 | 0 |
| Storage Bay Dist (ft) | 500 |  | 180 |  |  |  |  |  |
| Storage Blk Time (\%) |  | 0 |  |  |  |  |  |  |
| Queuing Penalty (veh) |  | 0 |  |  |  |  |  |  |

Intersection: 5: I-205 NB Off Ramp \& OR43

| Movement | EB | EB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | R | T | T | T | T |
| Maximum Queue (ft) | 56 | 80 | 105 | 130 | 140 | 98 |
| Average Queue (ft) | 14 | 36 | 39 | 60 | 56 | 29 |
| 95th Queue (ft) | 41 | 62 | 82 | 113 | 114 | 72 |
| Link Distance (ft) |  | 849 | 205 | 205 | 185 | 185 |
| Upstream Blk Time (\%) |  |  |  |  | 0 |  |
| Queuing Penalty (veh) |  |  |  | 0 |  |  |
| Storage Bay Dist (ft) | 225 |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  |

Intersection: 6: OR 43 \& Willamette Falls Dr

| Movement | EB | EB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | $R$ | L | T | $R$ |
| Maximum Queue (ft) | 145 | 142 | 112 | 6 | 9 |
| Average Queue (ft) | 135 | 110 | 50 | 0 | 0 |
| 95th Queue (ft) | 143 | 166 | 90 | 6 | 6 |
| Link Distance (ft) | 128 | 128 |  | 205 | 205 |
| Upstream Blk Time (\%) | 74 | 7 |  |  |  |
| Queuing Penalty (veh) | 261 | 24 |  |  |  |
| Storage Bay Dist (ft) |  |  | 200 |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |







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| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


|  | 4 |  | 4 |  |  | $\downarrow$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |  |
| Lane Configurations | ${ }^{1}$ | T | ${ }^{7}$ | 4 | 4 | 「 |  |
| Traffic Volume (vph) | 270 | 246 | 555 | 950 | 457 | 215 |  |
| Future Volume (vph) | 270 | 246 | 555 | 950 | 457 | 215 |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |  |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Frpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.99 |  |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Frt | 1.00 | 0.85 | 1.00 | 1.00 | 1.00 | 0.85 |  |
| Flt Protected | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 |  |
| Satd. Flow (prot) | 1770 | 1583 | 1787 | 1881 | 1827 | 1532 |  |
| Flt Permitted | 0.95 | 1.00 | 0.28 | 1.00 | 1.00 | 1.00 |  |
| Satd. Flow (perm) | 1770 | 1583 | 535 | 1881 | 1827 | 1532 |  |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |  |
| Adj. Flow (vph) | 284 | 259 | 584 | 1000 | 481 | 226 |  |
| RTOR Reduction (vph) | 0 | 210 | 0 | 0 | 0 | 81 |  |
| Lane Group Flow (vph) | 284 | 49 | 584 | 1000 | 481 | 145 |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  | 3 |  |
| Heavy Vehicles (\%) | 2\% | 2\% | 1\% | 1\% | 4\% | 4\% |  |
| Turn Type | Prot | Perm | pm+pt | NA | NA | Perm |  |
| Protected Phases | 8 |  | 1 | 6 | 2 |  |  |
| Permitted Phases |  | 8 | 6 |  |  | 2 |  |
| Actuated Green, G (s) | 21.0 | 21.0 | 81.0 | 81.0 | 44.0 | 44.0 |  |
| Effective Green, g (s) | 21.0 | 21.0 | 81.0 | 81.0 | 44.0 | 44.0 |  |
| Actuated g/C Ratio | 0.19 | 0.19 | 0.74 | 0.74 | 0.40 | 0.40 |  |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  |
| Vehicle Extension (s) | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 |  |
| Lane Grp Cap (vph) | 337 | 302 | 769 | 1385 | 730 | 612 |  |
| v/s Ratio Prot | c0.16 |  | 0.23 | c0.53 | 0.26 |  |  |
| v/s Ratio Perm |  | 0.03 | c0.33 |  |  | 0.09 |  |
| v/c Ratio | 0.84 | 0.16 | 0.76 | 0.72 | 0.66 | 0.24 |  |
| Uniform Delay, d1 | 42.9 | 37.2 | 19.7 | 8.2 | 26.9 | 21.9 |  |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.23 | 1.66 |  |
| Incremental Delay, d2 | 16.9 | 0.2 | 4.1 | 3.3 | 3.9 | 0.8 |  |
| Delay (s) | 59.8 | 37.4 | 23.8 | 11.5 | 37.1 | 37.0 |  |
| Level of Service | E | D | C | B | D | D |  |
| Approach Delay (s) | 49.1 |  |  | 16.0 | 37.1 |  |  |
| Approach LOS | D |  |  | B | D |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 27.6 |  | M 2000 | evel of Service | C |
| HCM 2000 Volume to Capacity ratio |  |  | 0.79 |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 110.0 |  | m of los | ime (s) | 12.0 |
| Intersection Capacity Utilization |  |  | 79.8\% |  | Level | Service | D |
| Analysis Period (min) |  |  | 15 |  |  |  |  |
| C Critical Lane Group |  |  |  |  |  |  |  |


| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{*}$ | 「 | $\cdots$ | 4 | 4 | 「' |
| Traffic Volume (vph) | 120 | 192 | 388 | 833 | 480 | 596 |
| Future Volume (vph) | 120 | 192 | 388 | 833 | 480 | 596 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 0.97 | 1.00 | 1.00 | 1.00 | 1.00 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 0.85 | 1.00 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1719 | 1499 | 3433 | 1863 | 1810 | 1538 |
| Flt Permitted | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1719 | 1499 | 3433 | 1863 | 1810 | 1538 |
| Peak-hour factor, PHF | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Adj. Flow (vph) | 122 | 196 | 396 | 850 | 490 | 608 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 122 | 196 | 396 | 850 | 490 | 608 |
| Confl. Peds. (\#/hr) |  |  | 1 |  |  | 1 |
| Confl. Bikes (\#/hr) |  | 3 |  |  |  | 3 |
| Heavy Vehicles (\%) | 5\% | 5\% | 2\% | 2\% | 5\% | 5\% |
| Turn Type | Prot | Perm | Prot | NA | NA | pt+ov |
| Protected Phases | 8 |  | 1 | 6 | 2 | 28 |
| Permitted Phases |  | 8 |  |  |  |  |
| Actuated Green, G (s) | 22.8 | 22.8 | 22.0 | 79.2 | 53.2 | 80.0 |
| Effective Green, g (s) | 22.8 | 22.8 | 22.0 | 79.2 | 53.2 | 80.0 |
| Actuated g/C Ratio | 0.21 | 0.21 | 0.20 | 0.72 | 0.48 | 0.73 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  |
| Vehicle Extension (s) | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 |  |
| Lane Grp Cap (vph) | 356 | 310 | 686 | 1341 | 875 | 1118 |
| v/s Ratio Prot | 0.07 |  | 0.12 | c0.46 | 0.27 | 0.40 |
| v/s Ratio Perm |  | c0.13 |  |  |  |  |
| v/c Ratio | 0.34 | 0.63 | 0.58 | 0.63 | 0.56 | 0.54 |
| Uniform Delay, d1 | 37.2 | 39.8 | 39.8 | 7.9 | 20.1 | 6.8 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.18 | 0.25 | 0.47 |
| Incremental Delay, d2 | 0.4 | 3.7 | 2.4 | 1.5 | 1.6 | 0.2 |
| Delay (s) | 37.6 | 43.4 | 42.2 | 10.9 | 6.6 | 3.4 |
| Level of Service | D | D | D | B | A | A |
| Approach Delay (s) | 41.2 |  |  | 20.8 | 4.8 |  |
| Approach LOS | D |  |  | C | A |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 16.7 | HCM 2000 Level of Service | B |
| HCM 2000 Volume to Capacity ratio | 0.66 |  | 12.0 |
| Actuated Cycle Length (s) | 110.0 | Sum of lost time (s) | B |
| Intersection Capacity Utilization | $57.2 \%$ | ICU Level of Service |  |
| Analysis Period (min) | 15 |  |  |
| C Critical Lane Group |  |  |  |

Intersection: 5: OR43 \& McKillican

| Movement | EB | EB | WB | WB | SE | SE | NW | NW | B77 | B77 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | TR | L | TR | L | TR | T |  |
| Maximum Queue (ft) | 206 | 226 | 165 | 197 | 182 | 504 | 200 | 601 | 254 | 267 |
| Average Queue (ft) | 64 | 166 | 115 | 81 | 14 | 397 | 57 | 269 | 80 | 68 |
| 95th Queue (ft) | 181 | 263 | 184 | 208 | 98 | 590 | 153 | 549 | 212 | 207 |
| Link Distance (ft) |  | 206 |  | 166 |  | 445 |  | 534 | 322 | 322 |
| Upstream Blk Time (\%) | 0 | 21 | 12 | 16 |  | 37 |  | 3 | 0 | 0 |
| Queuing Penalty (veh) | 0 | 0 | 0 | 0 |  | 0 |  | 30 | 0 | 2 |
| Storage Bay Dist (ft) | 150 |  | 100 |  | 180 |  | 110 |  |  |  |
| Storage Blk Time (\%) | 0 | 32 | 45 | 1 |  | 43 | 2 | 17 |  |  |
| Queuing Penalty (veh) | 0 | 13 | 11 | 1 |  | 3 | 17 | 12 |  |  |

Intersection: 6: I-205 SB On Ramp \& I-205 SB Off Ramp \& OR43

| Movement | WB | WB | NB | NB | NB | SB | SB | B77 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | $<\mathrm{L}$ | R | L | T | T | T | TR | T |
| Maximum Queue (ft) | 363 | 423 | 280 | 772 | 820 | 376 | 406 | 532 |
| Average Queue (ft) | 176 | 128 | 279 | 734 | 751 | 274 | 344 | 259 |
| 95th Queue (ft) | 346 | 325 | 289 | 828 | 992 | 406 | 461 | 655 |
| Link Distance (ft) |  | 1108 |  | 750 | 750 | 322 | 322 | 534 |
| Upstream Blk Time (\%) |  |  |  | 23 | 43 | 5 | 27 | 9 |
| Queuing Penalty (veh) |  |  |  | 111 | 203 | 26 | 152 | 98 |
| Storage Bay Dist (ft) | 540 |  | 180 |  |  |  |  |  |
| Storage Blk Time (\%) | 1 | 0 | 81 | 3 |  |  |  |  |
| Queuing Penalty (veh) | 4 | 0 | 181 | 15 |  |  |  |  |

Intersection: 8: OR43 \& Willamette Falls Dr

| Movement | EB | EB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | R | L | T | T | R |
| Maximum Queue (ft) | 470 | 255 | 300 | 708 | 359 | 213 |
| Average Queue (ft) | 308 | 109 | 282 | 676 | 313 | 133 |
| 95th Queue (ft) | 495 | 211 | 380 | 779 | 382 | 302 |
| Link Distance (ft) | 458 | 458 |  | 666 | 277 |  |
| Upstream Blk Time (\%) | 8 | 0 |  | 63 | 47 |  |
| Queuing Penalty (veh) | 20 | 0 |  | 0 | 313 |  |
| Storage Bay Dist (ft) |  |  | 200 |  |  | 113 |
| Storage Blk Time (\%) |  |  | 12 | 65 | 48 |  | | Queuing Penalty (veh) |
| :--- |

Intersection: 10: Willamette Falls Dr \& W A St

| Movement | EB | EB | WB | WB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LT | T | T | TR | LR |
| Maximum Queue (ft) | 228 | 79 | 21 | 52 | 246 |
| Average Queue (ft) | 74 | 5 | 1 | 2 | 85 |
| 95th Queue (ft) | 178 | 54 | 21 | 28 | 252 |
| Link Distance (ft) | 593 | 593 | 458 | 458 | 585 |
| Upstream Blk Time (\%) |  |  |  |  | 2 |
| Queuing Penalty (veh) |  |  |  |  | 0 |
| Storage Bay Dist (ft) |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |

## Intersection: 22: I-205 NB Off Ramp

| Movement | EB |
| :--- | ---: |
| Directions Served | T |
| Maximum Queue (ft) | 307 |
| Average Queue (ft) | 57 |
| 95th Queue (ft) | 271 |
| Link Distance (ft) | 502 |
| Upstream Blk Time (\%) | 2 |
| Queuing Penalty (veh) | 0 |
| Storage Bay Dist (ft) |  |
| Storage Blk Time (\%) |  |
| Queuing Penalty (veh) |  |

Intersection: 3005: I-205 NB Off Ramp \& OR43

| Movement | EB | EB | NB | NB | NB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | R | L | L | T | T | R |
| Maximum Queue (ft) | 226 | 248 | 356 | 277 | 316 | 786 | 735 |
| Average Queue (ft) | 119 | 127 | 250 | 235 | 276 | 590 | 276 |
| 95th Queue (ft) | 217 | 287 | 422 | 352 | 356 | 949 | 847 |
| Link Distance (ft) | 241 | 241 | 277 | 277 | 277 | 750 | 750 |
| Upstream Blk Time (\%) | 2 | 11 | 17 | 15 | 35 | 20 | 4 |
| Queuing Penalty (veh) | 4 | 17 | 69 | 62 | 142 | 109 | 19 |
| Storage Bay Dist (ft) |  |  |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |
| Network Summary |  |  |  |  |  |  |  |
| Network wide Queuing P | 2209 |  |  |  |  |  |  |


| HDR | Sim Traffic Report <br> Page 2 |
| :--- | ---: |






Intersection: 5: OR43 \& McKillican

| Movement | EB | EB | WB | WB | SE | SE | NW | NW | B77 | B77 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | TR | L | TR | L | TR | T |  |
| Maximum Queue (ft) | 206 | 256 | 166 | 185 | 150 | 498 | 210 | 608 | 329 | 346 |
| Average Queue (ft) | 157 | 226 | 154 | 173 | 9 | 426 | 102 | 440 | 172 | 175 |
| 95th Queue (ft) | 284 | 243 | 184 | 214 | 79 | 616 | 211 | 773 | 359 | 389 |
| Link Distance (ft) |  | 206 |  | 166 |  | 445 |  | 534 | 322 | 322 |
| Upstream Blk Time (\%) | 2 | 87 | 34 | 79 |  | 37 |  | 14 | 1 | 3 |
| Queuing Penalty (veh) | 0 | 0 | 0 | 0 |  | 0 |  | 156 | 5 | 16 |
| Storage Bay Dist (ft) | 150 |  | 100 |  | 180 |  | 110 |  |  |  |
| Storage Blk Time (\%) | 5 | 91 | 88 | 25 |  | 39 | 13 | 23 |  |  |
| Queuing Penalty (veh) | 16 | 99 | 75 | 41 |  | 1 | 140 | 19 |  |  |

Intersection: 6: I-205 SB On Ramp \& I-205 SB Off Ramp \& OR43

| Movement | WB | WB | NB | NB | NB | SB | SB | B77 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | $<\mathrm{L}$ | R | L | T | T | T | TR | T |
| Maximum Queue (ft) | 550 | 854 | 239 | 230 | 188 | 307 | 401 | 543 |
| Average Queue (ft) | 289 | 293 | 125 | 95 | 90 | 148 | 358 | 277 |
| 95th Queue (ft) | 520 | 729 | 221 | 185 | 155 | 255 | 455 | 647 |
| Link Distance (ft) |  | 1108 |  | 736 | 736 | 322 | 322 | 534 |
| Upstream Blk Time (\%) |  | 1 |  |  |  | 0 | 24 | 2 |
| Queuing Penalty (veh) |  | 0 |  |  |  | 1 | 169 | 34 |
| Storage Bay Dist (ft) | 540 |  | 180 |  |  |  |  |  |
| Storage Blk Time (\%) | 1 | 4 | 6 | 0 |  |  |  |  |
| Queuing Penalty (veh) | 11 | 11 | 6 | 0 |  |  |  |  |

Intersection: 8: OR43 \& Willamette Falls Dr

| Movement | EB | EB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | R | L | T | T | R |
| Maximum Queue (ft) | 302 | 390 | 299 | 517 | 286 | 213 |
| Average Queue (ft) | 158 | 197 | 183 | 220 | 249 | 124 |
| 95th Queue (ft) | 261 | 331 | 305 | 458 | 316 | 296 |
| Link Distance (ft) | 458 | 458 |  | 666 | 263 |  |
| Upstream Blk Time (\%) |  | 0 |  | 1 | 10 |  |
| Queuing Penalty (veh) |  | 0 |  | 0 | 89 |  |
| Storage Bay Dist (ft) |  |  | 200 |  |  | 113 |
| Storage Blk Time (\%) |  |  | 13 | 4 | 41 |  | | Queuing Penalty (veh) |
| :--- |

Intersection: 10: Willamette Falls Dr \& W A St

| Movement | EB | EB | WB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | LT | T | TR | LR |
| Maximum Queue (ft) | 115 | 15 | 2 | 511 |
| Average Queue (ft) | 36 | 1 | 0 | 184 |
| 95th Queue (ft) | 88 | 10 | 2 | 425 |
| Link Distance (ft) | 593 | 593 | 458 | 585 |
| Upstream Blk Time (\%) |  |  |  | 2 |
| Queuing Penalty (veh) |  |  |  | 0 |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

## Intersection: 22: I-205 NB Off Ramp

| Movement | EB |
| :--- | ---: |
| Directions Served | T |
| Maximum Queue (ft) | 124 |
| Average Queue (ft) | 17 |
| 95th Queue (ft) | 109 |
| Link Distance (ft) | 502 |
| Upstream Blk Time (\%) |  |
| Queuing Penalty (veh) |  |
| Storage Bay Dist (ft) |  |
| Storage Blk Time (\%) |  |
| Queuing Penalty (veh) |  |

Intersection: 3005: I-205 NB Off Ramp \& OR43

| Movement | EB | EB | NB | NB | NB | SB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | R | L | L | T | T | T | R |
| Maximum Queue (ft) | 150 | 237 | 243 | 272 | 275 | 756 | 772 | 600 |
| Average Queue (ft) | 31 | 140 | 168 | 184 | 112 | 495 | 501 | 352 |
| 95th Queue (ft) | 97 | 241 | 240 | 254 | 246 | 789 | 813 | 717 |
| Link Distance (ft) |  | 228 |  | 263 | 263 | 736 | 736 |  |
| Upstream Blk Time (\%) | 0 | 6 | 0 | 0 | 0 | 3 | 5 |  |
| Queuing Penalty (veh) | 0 | 13 | 0 | 2 | 2 | 23 | 35 |  |
| Storage Bay Dist (ft) | 225 |  | 145 |  |  |  |  | 500 |
| Storage Blk Time (\%) | 0 | 7 | 11 | 22 |  |  | 26 | 1 |
| Queuing Penalty (veh) | 0 | 2 | 29 | 57 |  |  | 220 | 3 |

## Network Summary

Network wide Queuing Penalty: 1475

| HDR | Sim Traffic Report |
| :--- | :--- |




|  | $\rangle$ | $\stackrel{7}{7}$ | 4 | 4 | $\downarrow$ | $\checkmark$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |  |
| Lane Configurations | * | 「 | \% | $\uparrow$ | $\uparrow$ | 「 |  |
| Traffic Volume (veh/h) | 270 | 246 | 555 | 950 | 457 | 215 |  |
| Future Volume (Veh/h) | 270 | 246 | 555 | 950 | 457 | 215 |  |
| Sign Control | Stop |  |  | Free | Free |  |  |
| Grade | 0\% |  |  | 0\% | 0\% |  |  |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |  |
| Hourly flow rate (vph) | 284 | 259 | 584 | 1000 | 481 | 226 |  |
| Pedestrians |  |  |  | 3 | 3 |  |  |
| Lane Width (ft) |  |  |  | 12.0 | 12.0 |  |  |
| Walking Speed (ft/s) |  |  |  | 3.5 | 3.5 |  |  |
| Percent Blockage |  |  |  | 0 | 0 |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |
| Median type |  |  |  | None | None |  |  |
| Median storage veh) |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |
| vC , conflicting volume | 2652 | 484 | 481 |  |  |  |  |
| vC 1 , stage 1 conf vol |  |  |  |  |  |  |  |
| vC 2 , stage 2 conf vol |  |  |  |  |  |  |  |
| vCu , unblocked vol | 2652 | 484 | 481 |  |  |  |  |
| tC , single (s) | 6.4 | 6.2 | 4.1 |  |  |  |  |
| tC, 2 stage (s) |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 3.3 | 2.2 |  |  |  |  |
| p0 queue free \% | 0 | 55 | 46 |  |  |  |  |
| cM capacity (veh/h) | 12 | 581 | 1087 |  |  |  |  |
| Direction, Lane \# | EB 1 | EB 2 | NB 1 | NB 2 | SB 1 | SB 2 |  |
| Volume Total | 284 | 259 | 584 | 1000 | 481 | 226 |  |
| Volume Left | 284 | 0 | 584 | 0 | 0 | 0 |  |
| Volume Right | 0 | 259 | 0 | 0 | 0 | 226 |  |
| cSH | 12 | 581 | 1087 | 1700 | 1700 | 1700 |  |
| Volume to Capacity | 24.32 | 0.45 | 0.54 | 0.59 | 0.28 | 0.13 |  |
| Queue Length 95th (ft) | Err | 57 | 83 | 0 | 0 | 0 |  |
| Control Delay (s) | Err | 16.1 | 12.1 | 0.0 | 0.0 | 0.0 |  |
| Lane LOS | F | C | B |  |  |  |  |
| Approach Delay (s) | 5237.3 |  | 4.5 |  | 0.0 |  |  |
| Approach LOS | F |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Average Delay |  |  | 1006.0 |  |  |  |  |
| Intersection Capacity Utilization |  |  | 79.8\% |  |  |  | D |
| Analysis Period (min) |  |  | 15 | ICU Level of Service |  |  |  |

Intersection: 5: OR43 \& McKillican

| Movement | EB | EB | WB | WB | SE | SE | NW | NW | B77 | B77 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | TR | L | TR | L | TR | T |  |
| Maximum Queue (ft) | 162 | 223 | 157 | 159 | 202 | 503 | 209 | 641 | 320 | 323 |
| Average Queue (ft) | 43 | 135 | 82 | 38 | 12 | 460 | 74 | 514 | 173 | 172 |
| 95th Queue (ft) | 118 | 222 | 145 | 112 | 92 | 528 | 191 | 749 | 376 | 396 |
| Link Distance (ft) |  | 206 |  | 166 |  | 445 |  | 534 | 322 | 322 |
| Upstream Blk Time (\%) | 0 | 3 | 0 | 1 |  | 56 |  | 21 | 1 | 3 |
| Queuing Penalty (veh) | 0 | 0 | 0 | 0 |  | 0 |  | 223 | 7 | 17 |
| Storage Bay Dist (ft) | 150 |  | 100 |  | 180 |  | 110 |  |  |  |
| Storage Blk Time (\%) | 0 | 9 | 10 | 0 |  | 54 | 1 | 33 |  |  |
| Queuing Penalty (veh) | 0 | 4 | 3 | 0 |  | 4 | 9 | 24 |  |  |

Intersection: 6: I-205 SB On Ramp \& I-205 SB Off Ramp \& OR43

| Movement | WB | WB | NB | NB | NB | SB | SB | B77 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | $<\mathrm{L}$ | R | L | T | T | T | TR | T |
| Maximum Queue (ft) | 443 | 635 | 358 | 446 | 365 | 388 | 417 | 546 |
| Average Queue (ft) | 152 | 242 | 246 | 212 | 147 | 306 | 359 | 270 |
| 95th Queue (ft) | 345 | 563 | 368 | 387 | 295 | 404 | 449 | 652 |
| Link Distance (ft) |  | 1108 |  | 669 | 669 | 322 | 322 | 534 |
| Upstream Blk Time (\%) |  | 0 |  | 0 | 0 | 6 | 26 | 3 |
| Queuing Penalty (veh) |  | 0 |  | 0 | 0 | 33 | 145 | 29 |
| Storage Bay Dist (ft) | 540 |  | 270 |  |  |  |  |  |
| Storage Blk Time (\%) |  | 3 | 19 | 8 |  |  |  |  |
| Queuing Penalty (veh) |  | 5 | 42 | 39 |  |  |  |  |

Intersection: 8: OR43 \& Willamette Falls Dr

| Movement | EB | EB | NB | NB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | R | L | T | T |
| Maximum Queue (ft) | 500 | 496 | 289 | 505 | 24 |
| Average Queue (ft) | 466 | 232 | 139 | 30 | 1 |
| 95th Queue (ft) | 482 | 580 | 251 | 235 | 11 |
| Link Distance (ft) | 458 | 458 |  | 666 | 182 |
| Upstream Blk Time (\%) | 92 | 17 |  | 0 |  |
| Queuing Penalty (veh) | 237 | 43 |  | 0 |  |
| Storage Bay Dist (ft) |  |  | 200 |  |  |
| Storage Blk Time (\%) |  |  | 4 | 0 |  |
| Queuing Penalty (veh) |  |  | 38 | 0 |  |

Queuing and Blocking Report
Future Roundabout Build 7:00 to 8:00 AM
Intersection: 10: Willamette Falls Dr \& W A St

| Movement | EB | EB | WB | WB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LT | T | T | TR | LR |
| Maximum Queue (ft) | 638 | 626 | 84 | 95 | 603 |
| Average Queue (ft) | 607 | 607 | 7 | 8 | 582 |
| 95th Queue (ft) | 628 | 624 | 82 | 86 | 626 |
| Link Distance (ft) | 593 | 593 | 458 | 458 | 585 |
| Upstream Blk Time (\%) | 98 | 95 | 0 | 0 | 96 |
| Queuing Penalty (veh) | 0 | 0 | 0 | 0 | 0 |
| Storage Bay Dist (ft) |  |  |  |  |  |

## Intersection: 22: I-205 NB Off Ramp

| Movement | EB |
| :--- | ---: |
| Directions Served | T |
| Maximum Queue (ft) | 18 |
| Average Queue (ft) | 1 |
| 95th Queue (ft) | 13 |
| Link Distance (ft) | 502 |
| Upstream Blk Time (\%) |  |
| Queuing Penalty (veh) |  |
| Storage Bay Dist (ft) |  |
| Storage Blk Time (\%) |  |
| Queuing Penalty (veh) |  |

Intersection: 3005: I-205 NB Off Ramp \& OR43

| Movement | EB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LR | LT | T | T | R |
| Maximum Queue (ft) | 151 | 182 | 191 | 141 | 89 |
| Average Queue (ft) | 61 | 63 | 16 | 32 | 3 |
| 95th Queue (ft) | 117 | 143 | 95 | 102 | 74 |
| Link Distance (ft) | 161 | 182 | 182 | 669 | 669 |
| Upstream Blk Time (\%) | 0 | 0 | 0 |  | 0 |
| Queuing Penalty (veh) | 1 | 1 | 1 | 0 |  |
| Storage Bay Dist (ft) |  |  |  |  |  |
| Storage Bk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |
| Network Summary |  |  |  |  |  |
| Network wide Queuing Penalty: 907 |  |  |  |  |  |


| HDR | SimTraffic Report |
| :--- | ---: |
| Page 2 |  |




|  | $\rangle$ | $\geqslant$ | 4 | 4 | $\downarrow$ | $\checkmark$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |  |
| Lane Configurations | \% | 「 | \% | $\uparrow$ | $\uparrow$ | 「 |  |
| Traffic Volume (veh/h) | 278 | 499 | 320 | 594 | 594 | 265 |  |
| Future Volume (Veh/h) | 278 | 499 | 320 | 594 | 594 | 265 |  |
| Sign Control | Stop |  |  | Free | Free |  |  |
| Grade | 0\% |  |  | 0\% | 0\% |  |  |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |  |
| Hourly flow rate (vph) | 293 | 525 | 337 | 625 | 625 | 279 |  |
| Pedestrians |  |  |  | 3 | 3 |  |  |
| Lane Width (ft) |  |  |  | 12.0 | 12.0 |  |  |
| Walking Speed (ft/s) |  |  |  | 3.5 | 3.5 |  |  |
| Percent Blockage |  |  |  | 0 | 0 |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |
| Median type |  |  |  | None | None |  |  |
| Median storage veh) |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |
| vC , conflicting volume | 1927 | 628 | 625 |  |  |  |  |
| vC 1 , stage 1 conf vol |  |  |  |  |  |  |  |
| vC 2 , stage 2 conf vol |  |  |  |  |  |  |  |
| vCu , unblocked vol | 1927 | 628 | 625 |  |  |  |  |
| tC , single (s) | 6.4 | 6.2 | 4.1 |  |  |  |  |
| tC, 2 stage (s) |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 3.3 | 2.2 |  |  |  |  |
| p0 queue free \% | 0 | 0 | 65 |  |  |  |  |
| cM capacity (veh/h) | 47 | 481 | 956 |  |  |  |  |
| Direction, Lane \# | EB 1 | EB 2 | NB 1 | NB 2 | SB 1 | SB 2 |  |
| Volume Total | 293 | 525 | 337 | 625 | 625 | 279 |  |
| Volume Left | 293 | 0 | 337 | 0 | 0 | 0 |  |
| Volume Right | 0 | 525 | 0 | 0 | 0 | 279 |  |
| cSH | 47 | 481 | 956 | 1700 | 1700 | 1700 |  |
| Volume to Capacity | 6.20 | 1.09 | 0.35 | 0.37 | 0.37 | 0.16 |  |
| Queue Length 95th (ft) | Err | 425 | 40 | 0 | 0 | 0 |  |
| Control Delay (s) | Err | 96.7 | 10.8 | 0.0 | 0.0 | 0.0 |  |
| Lane LOS | F | F | B |  |  |  |  |
| Approach Delay (s) | 3643.6 |  | 3.8 |  | 0.0 |  |  |
| Approach LOS | F |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Average Delay |  |  | 1111.8 |  |  |  |  |
| Intersection Capacity Utilization |  |  | 74.4\% | ICU Level of Service |  |  | D |
| Analysis Period (min) |  |  | 15 |  |  |  |  |

Intersection: 5: OR43 \& McKillican

| Movement | EB | EB | WB | WB | SE | SE | NW | NW | B77 | B77 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | TR | L | TR | L | TR | T |  |
| Maximum Queue (ft) | 206 | 249 | 166 | 185 | 72 | 500 | 209 | 611 | 310 | 335 |
| Average Queue (ft) | 157 | 226 | 155 | 172 | 5 | 400 | 95 | 418 | 117 | 109 |
| 95th Queue (ft) | 290 | 240 | 181 | 218 | 52 | 628 | 196 | 744 | 283 | 297 |
| Link Distance (ft) |  | 206 |  | 166 |  | 445 |  | 534 | 322 | 322 |
| Upstream Blk Time (\%) | 2 | 86 | 33 | 79 |  | 20 |  | 10 | 0 | 1 |
| Queuing Penalty (veh) | 0 | 0 | 0 | 0 |  | 0 |  | 115 | 0 | 4 |
| Storage Bay Dist (ft) | 150 |  | 100 |  | 180 |  | 110 |  |  |  |
| Storage Blk Time (\%) | 4 | 89 | 87 | 25 |  | 27 | 11 | 22 |  |  |
| Queuing Penalty (veh) | 12 | 97 | 74 | 41 |  | 1 | 112 | 18 |  |  |

Intersection: 6: I-205 SB On Ramp \& I-205 SB Off Ramp \& OR43

| Movement | WB | WB | NB | NB | NB | SB | SB | B77 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | $<\mathrm{L}$ | R | L | T | T | T | TR | T |
| Maximum Queue (ft) | 433 | 475 | 184 | 161 | 169 | 352 | 392 | 185 |
| Average Queue (ft) | 226 | 181 | 92 | 74 | 79 | 221 | 262 | 14 |
| 95th Queue (ft) | 407 | 433 | 162 | 131 | 135 | 365 | 386 | 109 |
| Link Distance (ft) |  | 1108 |  | 669 | 669 | 322 | 322 | 534 |
| Upstream Blk Time (\%) |  | 0 |  |  |  | 1 | 2 |  |
| Queuing Penalty (veh) |  | 0 |  |  |  | 5 | 14 |  |
| Storage Bay Dist (ft) | 540 |  | 180 |  |  |  |  |  |
| Storage Blk Time (\%) | 0 | 1 | 1 | 0 |  |  |  |  |
| Queuing Penalty (veh) | 1 | 2 | 1 | 0 |  |  |  |  |

Intersection: 8: OR43 \& Willamette Falls Dr

| Movement | EB | EB | NB | NB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | R | L | T | T |
| Maximum Queue (ft) | 493 | 509 | 207 | 40 | 39 |
| Average Queue (ft) | 467 | 370 | 89 | 1 | 3 |
| 95th Queue (ft) | 482 | 647 | 159 | 30 | 19 |
| Link Distance (ft) | 458 | 458 |  | 666 | 182 |
| Upstream Blk Time (\%) | 85 | 31 |  |  |  |
| Queuing Penalty (veh) | 332 | 121 |  |  |  |
| Storage Bay Dist (ft) |  |  | 200 |  |  |
| Storage Blk Time (\%) |  |  | 1 | 0 |  |
| Queuing Penalty (veh) |  |  | 4 | 0 |  |

Intersection: 10: Willamette Falls Dr \& W A St

| Movement | EB | EB | WB | WB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LT | T | T | TR | LR |
| Maximum Queue (ft) | 641 | 649 | 68 | 99 | 613 |
| Average Queue (ft) | 595 | 593 | 4 | 5 | 587 |
| 95th Queue (ft) | 719 | 739 | 45 | 55 | 659 |
| Link Distance (ft) | 593 | 593 | 458 | 458 | 585 |
| Upstream Blk Time (\%) | 88 | 86 |  |  | 97 |
| Queuing Penalty (veh) | 0 | 0 |  |  | 0 |
| Storage Bay Dist (ft) |  |  |  |  |  |

## Intersection: 22: I-205 NB Off Ramp

## Movement

Directions Served
Maximum Queue ( ft )
Average Queue (ft)
95th Queue ( ft )
Link Distance (ft)
Upstream Blk Time (\%)
Queuing Penalty (veh)
Storage Bay Dist (ft)
Storage Blk Time (\%)
Queuing Penalty (veh)
Intersection: 3005: I-205 NB Off Ramp \& OR43

| Movement | EB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LR | LT | T | T | R |
| Maximum Queue (ft) | 83 | 165 | 56 | 214 | 8 |
| Average Queue (ft) | 36 | 37 | 2 | 51 | 0 |
| 95th Queue (ft) | 76 | 112 | 35 | 142 | 6 |
| Link Distance (ft) | 161 | 182 | 182 | 669 | 669 |
| Upstream Blk Time (\%) |  | 0 | 0 |  |  |
| Queuing Penalty (veh) |  | 0 | 0 |  |  |
| Storage Bay Dist (ft) |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |

Network Summary
Network wide Queuing Penalty: 954

| HDR | SimTraffic Report |
| :--- | ---: |
| Page 2 |  |

## Appendix D Sidra Roundabout Analysis Worksheets

## SITE LAYOUT

Site: 101 [1 lane onramp 2045 PM (adopted)]
New Site
Roundabout


SIDRA INTERSECTION 7.0 | Copyright © 2000-2017 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: HDR | Created: Friday, August 10, 2018 11:25:30 AM
Project: c:lpwworkinglwest01\d0683504\Sidra Roundabout_OR43_exitramp_20180718.sip7

## MOVEMENT SUMMARY

## Site: 101 [1 lane onramp 2045 PM (adopted)]

New Site
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | f Queue <br> Distance <br> ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
|  |  |  |  |  |  |  |  |  |  |  |  |
| 8 | T1 | 709 | 2.0 | 0.783 | 10.1 | LOS A | 8.1 | 206.7 | 0.90 | 1.12 | 30.7 |
| 18 | R2 | 857 | 2.0 | 0.946 | 20.7 | LOS D | 18.4 | 468.4 | 1.00 | 1.56 | 24.7 |
| Appro |  | 1566 | 2.0 | 0.946 | 15.9 | LOS B | 18.4 | 468.4 | 0.96 | 1.36 | 27.2 |
| NorthWest: I-205 Exit Ramp to OR43 |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 31 | 0.0 | 0.273 | 14.0 | LOS A | 1.2 | 29.8 | 0.66 | 0.82 | 35.2 |
| 16 | R2 | 166 | 0.0 | 0.273 | 7.6 | LOS A | 1.2 | 29.8 | 0.66 | 0.82 | 34.6 |
| Appro |  | 197 | 0.0 | 0.273 | 8.5 | LOS A | 1.2 | 29.8 | 0.66 | 0.82 | 34.7 |
| SouthWest: OR43 |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 540 | 3.0 | 0.382 | 10.2 | LOS A | 2.2 | 57.1 | 0.15 | 0.61 | 35.0 |
| 4 | T1 | 350 | 3.0 | 0.182 | 3.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.34 | 38.3 |
| Approach |  | 890 | 3.0 | 0.382 | 7.7 | LOS A | 2.2 | 57.1 | 0.09 | 0.51 | 36.0 |
| All Ve | cles | 2653 | 2.2 | 0.946 | 12.6 | LOS B | 18.4 | 468.4 | 0.64 | 1.04 | 30.6 |

Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
Intersection and Approach LOS values are based on average delay for all movements ( $\mathrm{v} / \mathrm{c}$ not used).
Roundabout Capacity Model: US HCM 6.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## SITE LAYOUT

## G Site: 101

[2 lane onramp 2045 AM NB 1 lane test]
New Site
Roundabout


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Organisation: HDR | Created: Monday, August 13, 2018 8:56:14 AM
Project: c:\pwworkinglwest01\d0683504\Sidra Roundabout_OR43_exitramp_20180718.sip7

## MOVEMENT SUMMARY

## Gite: 101 [2 lane onramp 2045 AM NB 1 lane test]

New Site
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Mov } \\ \text { ID } \end{gathered}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \end{gathered}$ | $\begin{aligned} & \text { Deg. } \\ & \text { Satn } \\ & \text { v/c } \end{aligned}$ | Average Delay sec | Level of Service | 95\% Back Vehicles veh | f Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| NorthEast: OR43 |  |  |  |  |  |  |  |  |  |  |  |
| 8 | T1 | 490 | 5.0 | 0.488 | 4.8 | LOS A | 2.7 | 71.0 | 0.61 | 0.53 | 32.6 |
| 18 | R2 | 608 | 5.0 | 0.381 | 2.5 | LOS A | 0.0 | 0.0 | 0.00 | 0.34 | 33.6 |
| Appro |  | 1098 | 5.0 | 0.488 | 3.6 | LOS A | 2.7 | 71.0 | 0.27 | 0.42 | 33.1 |
| NorthWest: I-205 Exit Ramp to OR43 |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 122 | 5.0 | 0.379 | 13.0 | LOS A | 1.8 | 47.2 | 0.63 | 0.81 | 34.4 |
| 16 | R2 | 196 | 5.0 | 0.379 | 6.6 | LOS A | 1.8 | 47.2 | 0.63 | 0.81 | 34.3 |
| Appro |  | 318 | 5.0 | 0.379 | 9.1 | LOS A | 1.8 | 47.2 | 0.63 | 0.81 | 34.3 |
| SouthWest: OR43 |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 396 | 2.0 | 0.991 | 25.3 | LOS E | 44.2 | 1122.9 | 1.00 | 0.91 | 30.4 |
| 4 | T1 | 850 | 2.0 | 0.991 | 18.9 | LOS E | 44.2 | 1122.9 | 1.00 | 0.91 | 28.1 |
| Approach |  | 1246 | 2.0 | 0.991 | 21.0 | LOS C | 44.2 | 1122.9 | 1.00 | 0.91 | 28.9 |
| All Vehicles |  | 2662 | 3.6 | 0.991 | 12.4 | LOS B | 44.2 | 1122.9 | 0.66 | 0.70 | 31.1 |

Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
Intersection and Approach LOS values are based on average delay for all movements (v/c not used).
Roundabout Capacity Model: US HCM 6.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## SITE LAYOUT

Site: 101 [2 lane onramp 2045 AM (adopted)]
New Site
Roundabout


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Organisation: HDR | Created: Friday, August 10, 2018 11:46:24 AM
Project: c:\pwworkinglwest01\d0683504\Sidra Roundabout_OR43_exitramp_20180718.sip7

## MOVEMENT SUMMARY

## Site: 101 [2 lane onramp 2045 AM (adopted)]

New Site
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \end{gathered}$ | $\begin{aligned} & \text { Deg. } \\ & \text { Satn } \\ & \text { v/c } \end{aligned}$ | Average Delay sec | Level of Service | 95\% Back Vehicles $\qquad$ | f Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| NorthEast: OR43 |  |  |  |  |  |  |  |  |  |  |  |
| 8 | T1 | 490 | 5.0 | 0.488 | 4.8 | LOS A | 2.7 | 71.0 | 0.61 | 0.53 | 32.6 |
| 18 | R2 | 608 | 5.0 | 0.381 | 2.5 | LOS A | 0.0 | 0.0 | 0.00 | 0.34 | 33.6 |
| Appro |  | 1098 | 5.0 | 0.488 | 3.6 | LOS A | 2.7 | 71.0 | 0.27 | 0.42 | 33.1 |
| NorthWest: I-205 Exit Ramp to OR43 |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 122 | 5.0 | 0.379 | 13.0 | LOS A | 1.8 | 47.2 | 0.63 | 0.81 | 34.4 |
| 16 | R2 | 196 | 5.0 | 0.379 | 6.6 | LOS A | 1.8 | 47.2 | 0.63 | 0.81 | 34.3 |
| Approach |  | 318 | 5.0 | 0.379 | 9.1 | LOS A | 1.8 | 47.2 | 0.63 | 0.81 | 34.3 |
| SouthWest: OR43 |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2T1 | 396 | 2.0 | 0.384 | 10.7 | LOS A | 2.2 | 54.8 | 0.34 | 0.60 | 35.3 |
| 4 |  | 850 | 2.0 | 0.384 | 3.8 | LOS A | 2.2 | 54.8 | 0.04 | 0.38 | 37.7 |
| Approach |  | 1246 | 2.0 | 0.384 | 6.0 | LOS A | 2.2 | 54.8 | 0.14 | 0.45 | 36.8 |
| All Vehicles |  | 2662 | 3.6 | 0.488 | 5.4 | LOS A | 2.7 | 71.0 | 0.25 | 0.48 | 35.0 |

Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
Intersection and Approach LOS values are based on average delay for all movements ( $\mathrm{v} / \mathrm{c}$ not used).
Roundabout Capacity Model: US HCM 6.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## SITE LAYOUT

Gite: 101 [2 lane onramp 2045 PM (adopted)]
New Site
Roundabout


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Organisation: HDR | Created: Friday, August 10, 2018 11:25:05 AM
Project: c:lpwworkinglwest01\d0683504\Sidra Roundabout_OR43_exitramp_20180718.sip7

## MOVEMENT SUMMARY

## Site: 101 [2 lane onramp 2045 PM (adopted)]

New Site
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | f Queue <br> Distance <br> ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
|  |  |  |  |  |  |  |  |  |  |  |  |
| 8 | T1 | 709 | 2.0 | 0.783 | 10.1 | LOS A | 8.1 | 206.7 | 0.90 | 1.12 | 30.7 |
| 18 | R2 | 857 | 2.0 | 0.522 | 2.5 | LOS A | 0.0 | 0.0 | 0.00 | 0.34 | 33.6 |
| Appro |  | 1566 | 2.0 | 0.783 | 6.0 | LOS A | 8.1 | 206.7 | 0.41 | 0.69 | 32.2 |
| NorthWest: I-205 Exit Ramp to OR43 |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 31 | 0.0 | 0.273 | 14.0 | LOS A | 1.2 | 29.8 | 0.66 | 0.82 | 35.2 |
| 16 | R2 | 166 | 0.0 | 0.273 | 7.6 | LOS A | 1.2 | 29.8 | 0.66 | 0.82 | 34.6 |
| Appro |  | 197 | 0.0 | 0.273 | 8.5 | LOS A | 1.2 | 29.8 | 0.66 | 0.82 | 34.7 |
| SouthWest: OR43 |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 540 | 3.0 | 0.382 | 10.2 | LOS A | 2.2 | 57.1 | 0.15 | 0.61 | 35.0 |
| 4 | T1 | 350 | 3.0 | 0.182 | 3.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.34 | 38.3 |
| Approach |  | 890 | 3.0 | 0.382 | 7.7 | LOS A | 2.2 | 57.1 | 0.09 | 0.51 | 36.0 |
| All Ve | cles | 2653 | 2.2 | 0.783 | 6.7 | LOS A | 8.1 | 206.7 | 0.32 | 0.64 | 33.8 |

Site Level of Service (LOS) Method: Delay \& Degree of Saturation (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
Intersection and Approach LOS values are based on average delay for all movements ( $\mathrm{v} / \mathrm{c}$ not used).
Roundabout Capacity Model: US HCM 6.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## Appendix E Vissim Analysis Worksheets



* $=$ for EB left turn stop-controlled movement

* $=$ for EB left turn stop-controlled movement


## Appendix F Conceptual Design of the Proposed Roundabout



(1) See sht. CO6B, note XX Wor d extg. structure
(For drg. nos., see sht. $X X$ )
(2) structure no. $x x x x x$

Sta. " $X X$ " $~$
nXX
Const $X X X X$ to sta. " $X X$ " $X X X+X X . X$, , $L$. Const. retaining wall
(For drg. nos., see sht. $X X$ )
(3) Const. conc. curb
(See drg. no. RD700)
(4) Const. type "X" conc. island
(See drg. nos. RD705 \& RD710)
(5) Const. P.C. conc. sidewalk (See drg. no. RD725)
(6) Const. perpendicular sidewalk ramp Install truncated domes
(For letails see shts. BCXX-BCXX) (For details see shts., $B C X-B C X X$
(See drg. nos. RD755 \& RD760)
(7) Const. mountable conc. curb
(8) Sta. "XX" $x X X+X X, X$, LL. Const. Sign cantile ver
(For drg. nos. see sht. $X x$ )

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1050 SW TTH AVENUE SUI


1-205: PARK PLACE INTCHGE TO
205: PARK PLACE INTCHGE.
WEST LINN INTCHGE SEC.
EAST PORTLAND FREEWA

| Designer. Jason Rahm <br> Drafter: Landon Fisher | $\begin{array}{l}\text { Reviever. John Woff } \\ \text { Checker: Brendan LeBlanc }\end{array}$ |  |
| :--- | :--- | :---: |
| GENERAL CONSTRUCTION NOTES | SHEETNO. |  |


Rotation: $247.8868^{\circ}$ Scale: $1 "=10$






[^0]:    ${ }^{1}$ http://www.cmfclearinghouse.org/cmfpdf.cfm?facid=225

